

**TWO-STAGE LOW NOISE ADVANCED TECHNOLOGY FAN  
I. AERODYNAMIC, STRUCTURAL, AND ACOUSTIC DESIGN**

**30 September 1974**

**by**

**H. E. Messenger, J. T. Ruschak  
and T. G. Sofrin**

**Pratt & Whitney Aircraft Division  
United Aircraft Corporation**

**Prepared for**

**National Aeronautics and Space Administration**

**NASA Lewis Research Center  
Contract NAS3-16811**

1. Report No. NASA CR-134662		2. Government Accession No.		3. Recipient's Catalog No.	
4. Title and Subtitle Two-Stage Low Noise Advanced Technology Fan I. Aerodynamic, Structural, and Acoustic Design				5. Report Date 30 September 1974	
				6. Performing Organization Code	
7. Author(s) H. E. Messenger, J. T. Ruschak and T. G. Sofrin				8. Performing Organization Report No. PWA-5069	
9. Performing Organization Name and Address Pratt & Whitney Aircraft Division United Aircraft Corporation East Hartford, Connecticut 06108				10. Work Unit No.	
				11. Contract or Grant No. NAS3-16811	
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Washington, D. C. 20546				13. Type of Report and Period Covered Contractor Report	
				14. Sponsoring Agency Code	
15. Supplementary Notes Design Report – Project Manager, W. L. Beede, Fluid System Components Division. Technical Advisor, M. F. Heidmann, V/STOL and Noise Division. NASA – Lewis Research Center, Cleveland, Ohio 44135					
16. Abstract  A two-stage fan was designed to reduce noise as much as 20 dB below current requirements. The first-stage rotor has a design tip speed of 365.8 m/sec (1200 ft/sec) and a hub/tip ratio of 0.4. The fan was designed to deliver a pressure ratio of 1.9 with an adiabatic efficiency of 85.3 percent at a specific inlet corrected flow of 209.2 kg/sec/m <sup>2</sup> (42.85 lbm/sec/ft <sup>2</sup> ). Noise reduction devices include acoustically treated casing walls, a flowpath exit acoustic splitter, a translating centerbody sonic inlet device, widely spaced blade rows, and the proper ratio of blades and vanes. Other features include multiple-circular-arc rotor airfoils, resettable stators, split outer casings, and capability to go to close blade-row spacing.					
17. Key Words (Suggested by Author(s)) Quiet Fan                      Acoustic Design Two-Stage Fan                Acoustic Treatments Aerodynamic Design        Sonic Inlet Structural Design				18. Distribution Statement  Unclassified - Unlimited	
19. Security Classif. (of this report) Unclassified		20. Security Classif. (of this page) Unclassified		21. No. of Pages 170	
22. Price*					

\* For sale by the National Technical Information Service, Springfield, Virginia 22151

## TABLE OF CONTENTS

	Page
SUMMARY	1
INTRODUCTION	1
AERODYNAMIC-ACOUSTIC CONSIDERATIONS	2
FLOWPATH AND VELOCITY VECTOR DIAGRAM DESIGN	3
Design Iterations	3
Losses	4
Flow Blockages	4
Air Angles and Velocities	5
Flowpath Spacings	5
Loadings	6
Exit Duct Aerodynamic Design	7
AIRFOIL DESIGN	8
Rotors	8
Airfoil Series	8
Partspan Shrouds	8
Chords, Thicknesses, and Numbers of Blades	8
Incidence and Deviation Angles	9
Channel Areas	10
Rotor Geometry	10
Stators	10
Airfoil Series	10
Chords and Thicknesses	10
Incidence and Deviation Angles	11
Channel Areas	11
Stator Geometry	12
INLET AERODYNAMIC DESIGN	12
Objectives and Techniques	12
Sonic Inlet Geometry	13
Inlet Cowling and Centerbody	13
Sonic Inlet Lip Shapes	13
Inlet Mach Number Distribution, Boundary Layer Characteristics, and Estimated Pressure Recoveries	13

## TABLE OF CONTENTS (Cont'd)

	Page
STRUCTURAL AND VIBRATION ANALYSIS	14
Rotors	15
Blade and Disk Vibration	15
Rotor Blade Stresses	15
Rotor Blade Flutter	16
Partspan Shrouds	17
Disk and Attachment Stresses	18
Stators	18
Stator Vibration	18
Stator Stresses	19
Stator Flutter	19
Interstage Seals	19
Sonic Inlet Support Struts	19
Critical Speeds and Forced Response	19
Baseline Standard Inlet Cowling Configuration	20
Sonic Inlet Configuration	20
ACOUSTIC DESIGN	21
Sonic Inlet, Acoustic Considerations	21
Flowpath and Blade Geometry	21
Rig Spectra Predictions	22
Treatment Attenuation Targets	23
Acoustic Treatment Selection	23
Inlet	23
Interstage and Aft Fan Duct	24
Predicted Attenuation – Interstage and Aft Treatment	25
Competing Noise Sources	25
APPENDIXES	
A. Symbols and Definitions	89
B. Aerodynamic Summaries	95
C. Airfoil Geometry on Design Conical Surfaces	105
D. Airfoil Coordinates on Manufacturing Surfaces	109
E. Two-Ring Acoustic Inlet Aerodynamic and Acoustic Design	157
REFERENCES	161
DISTRIBUTION LIST	163

## LIST OF FIGURES

Figure	Title	Page
1	Rotor and Stator Total Loss Spanwise Profiles	26
2	Rotor Adiabatic Efficiency Spanwise Profiles	27
3	Rotor Inlet and Exit Relative Air Angles Spanwise Profiles	28
4	Rotor Meridional Velocity Spanwise Profiles	29
5	Stator Meridional Velocity Spanwise Profiles	29
6	Inlet and Exit Mach Number Spanwise Profiles for Rotors	30
7	Inlet and Exit Mach Number Spanwise Profiles for Stators	30
8	Fan Flowpaths	31
9	Schematic of the Quiet Two-Stage Fan	32
10	Rotor Diffusion Factor Spanwise Profiles	33
11	Stator Diffusion Factor Spanwise Profiles	33
12	Total Pressure Ratio Spanwise Profiles	34
13	Stator Inlet and Exit Absolute Air Angle Spanwise Profiles	34
14	Fan Exit Duct and Acoustic Splitter Flowpath	35
15	Multiple-Circular-Arc Airfoil Definitions	36
16	Rotor Airfoil Thickness Spanwise Profiles	37
17	Rotor Chordwise Location of Airfoil Maximum Thickness Spanwise Profiles	37
18	Rotor Chord Spanwise Profiles	38
19	Rotor Inlet and Exit Metal Angle Spanwise Profiles	39
20	Rotor Incidence Angle Spanwise Profiles	40

## LIST OF FIGURES (Cont'd)

Figure	Title	Page
21	Rotor Deviation Angle Spanwise Profiles	41
22	Minimum Rotor Channel Area Ratio Spanwise Profiles	42
23	Rotor Front Camber Angle and Chord-Camber Parameter Spanwise Profiles	43
24	Rotor Channel Area Ratios Versus Axial Distance	44/45
25	Meridional View and Polar Representation of Blade Mean-Camber-Line	46
26	Airfoil Coordinate Definition for Manufacturing Sections	46
27	Stator Chord Spanwise Profiles	47
28	Stator Chordwise Location of Maximum Thickness Spanwise Profiles	48
29	Stator Airfoil Thickness Spanwise Profiles	48
30	Stator Incidence Angles Spanwise Profiles	49
31	Stator Deviation Angles Spanwise Profiles	50
32	Stator Inlet and Exit Metal Angles Spanwise Profiles	51
33	Ratios of Channel-Throat-Area to Captured-Area Versus Span for Stators	52
34	Stator 1 Front Camber Angle and Chord-Camber Parameter Spanwise Profiles	53
35	Stator 1 Channel Area Ratios Versus Axial Distance	54
36	Baseline Standard and Sonic Geometries	55
37	Baseline Standard Inlet Outer Wall Mach Number and Shape Factor Distributions	56
38	Sonic Inlet Throat Mach Number Spanwise Profile – Approach Configuration	57

## LIST OF FIGURES (Cont'd)

Figure	Title	Page
39	Mach Number Distributions Along Inlet Walls – Approach Configuration	57
40	Mach Number Distributions Along Inlet Walls – Cruise Configuration	58
41	Mach Number Distributions Along Inlet Walls – Takeoff Configuration	59
42	Boundary Layer Shape Factor Distributions Along Inlet Walls – Cruise Configuration	60
43	Boundary Layer Shape Factor Distributions Along Inlet Walls – Approach Configuration	61
44	Boundary Layer Shape Factor Distributions Along Inlet Walls- Takeoff Configuration	62
45	Rotor 1 Campbell Diagram	63
46	Rotor 2 Campbell Diagram	64
47	Rotor 1 Tip Mode Campbell Diagram	65
48	Rotor 2 Tip Mode Campbell Diagram	66
49	Rotor 1 Goodman Diagram	67
50	Rotor 2 Goodman Diagram	67
51	Schematic of Rotor Partspan Shrouds	68
52	Stator 1 Campbell Diagram	69
53	Stator 2 Campbell Diagram	70
54	Rotor Sideplate Seal Resonance	71
55	Stator Seal Resonance	71
56	Sonic Inlet Support Struts, Campbell Diagram	72
57	Spring-Mass Model for Critical Speed Analysis - Standard Inlet	73
58	Spring-Mass Model for Critical Speed Analysis - Sonic Inlet	74
59	Critical Speed Mode Shapes	75/76

## LIST OF FIGURES (Cont'd)

Figure	Title	Page
60	Schematic of Sonic Inlet Configuration	77
61	Effect of Rotor - Stator Spacing on Blade-Passing Frequency Noise Level	78
62	Fan Aft One-Third Octave Spectra – Untreated	79
63	Fan Aft Noise Attenuation Targets	80
64	Inlet Estimated Attenuation Due to Wall Treatment – Approach	81
65	Summary of Acoustic Treatment	82
66	Treatment Attenuation – Fan Discharge Ducts	83
67	Tuning Curves	84
68	Analytically Predicted Attenuation of Aft Fan Noise at Takeoff	85
69	Predicted Jet and Treated Fan Noise Levels – Approach	86
70	Predicted Jet and Treated Fan Noise Levels – Takeoff	87
71	Two-Ring Acoustic Inlet Design Schematic	158
72	Two-Ring Acoustic Inlet Predicted Attenuation	159

## LIST OF TABLES

Table	Title	Page
I	General Aerodynamic Design Parameters	3
II	Design Performance	4
III	Flow Blockages (% of Annulus Area) at Blade Edge Axial Location	5
IV	Predicted Blade Aerodynamic Diffusion Factors at Stall	7
V	Flow Blockages Assumed for Exit Duct Design	7
VI	Rotor Blading Parameters	9
VII	Stator Blading Parameters	11
VIII	Baseline and Sonic Inlet Total Pressure Recoveries	14
IX	Summary of Rotor Steady Stresses – 105% Design Speed	16
X	Rotor First Coupled Mode Flutter Parameters	17
XI	Partspan Shroud Parameters	17
XII	Rotor Disk and Attachment Stresses – 105% Design Speed	18
XIII	Analytically Predicted Fan Aft PNL at 45.7 Meter (105 Foot) Radius	25
XIV	Identification of Aerodynamic Summary Table Headings	95
XV	Identification of Spans and Diameters for Blade Element Data	96
XVI	Aerodynamic Summary – Rotor 1	97/98
XVII	Aerodynamic Summary – Stator 1	99/100
XVIII	Aerodynamic Summary – Rotor 2	101/102
XIX	Aerodynamic Summary – Stator 2	103/104
XX	Airfoil Geometry on Design Conical Surfaces – Rotor 1	105
XXI	Airfoil Geometry on Design Conical Surfaces – Stator 1	106
XXII	Airfoil Geometry on Design Conical Surfaces – Rotor 2	107

## LIST OF TABLES (Cont'd)

Table	Title	Page
XXIII	Airfoil Geometry on Design Conical Surfaces – Stator 2	108
XXIV	Airfoil Coordinates on Manufacturing Surfaces – Rotor 1	109/123
XXV	Airfoil Coordinates on Manufacturing Surfaces – Stator 1	124/133
XXVI	Airfoil Coordinates on Manufacturing Surfaces – Rotor 2	134/147
XXVII	Airfoil Coordinates on Manufacturing Surfaces – Stator 2	148/156
XXVIII	Two-Ring Acoustic Inlet Treatment Parameters	157

# TWO-STAGE, LOW NOISE ADVANCED TECHNOLOGY FAN

## I. AERODYNAMIC, STRUCTURAL, AND ACOUSTIC DESIGN

H. E. Messenger, J. T. Ruschak and T. G. Sofrin

### SUMMARY

Advanced, long-range, commercial transport aircraft will require a major reduction in engine noise without compromising requirements for high efficiency and adequate stall margin. To achieve a reduction of noise 20 dB below current requirements and to attain efficiency levels, stall margin, flow, and pressure ratio typical of an advanced fan, a two-stage, low tip-speed fan was selected as optimum for the flight Mach number range of 0.85 to 0.90.

Design features to reduce noise include use of low tip speeds and moderate blade aerodynamic loadings, proper relationship of the number of blades and vanes, axial spacings between blade rows of two aerodynamic chord lengths, acoustically treated casing walls, a flowpath exit acoustic splitter, and a translating centerbody sonic-inlet device.

The aerodynamic design was governed by the approximate parameters specified in the contract and applicable test data. Successful NASA-sponsored research fans tested by P&WA<sup>TM</sup> were used to establish criteria for good efficiency and stall margin. Important fan design parameters include a pressure ratio of 1.90 with a fan adiabatic efficiency of 85.3 percent, a first-stage rotor tip speed of 365.8 m/sec (1200 ft/sec), and a specific flow at the first-stage rotor inlet of 209 kg/sec/m<sup>2</sup> (42.85 lbm/sec/ft<sup>2</sup>). Other features of the design include a fan flowpath with a constant outer diameter of 0.836 m (32.90 in.), constant diameter hub sections between blades and vanes to facilitate use of axial spacers for alternate test configurations, multiple-circular-arc rotor airfoils, stators with resettable stagger angle capability, and split outer casings to accommodate on-stand configuration changes.

Structural and vibration analyses included calculation of blade-disk frequencies and their resonances with rig excitations, blade and vane steady-state stresses and flutter parameters, rig critical speeds, and rotor forced response to unbalance. Predicted stresses due to centrifugal, gas bending, and untwist forces are well within the capabilities of the materials selected. To avoid resonances and flutter, first-stage and second-stage rotor blades have a partspan shroud at 66.5 and 60 percent span from the hub, respectively. All blades and vanes were predicted to be free of flutter.

### INTRODUCTION

A fan research program is being conducted by P&WA for NASA-Lewis Research Center under Contract NAS3-16811. The objective of the program is to develop fan technology for application in turbofan engines for an advanced, long-range commercial transport with a cruise Mach number of 0.85 to 0.9. These future engines will be required to meet stringent noise reduction goals with minimum performance penalties. To achieve these goals, fans included in such engines must, during their design phase, incorporate features both to minimize the generation of noise and to obtain the maximum suppression of the noise generated.

An earlier NASA-Lewis study had been conducted for Advanced -Technology-Transport (ATT) application to determine the optimum fan configuration and performance parameters for a cruise Mach number of 0.85 to 0.9 and the stringent noise reduction goal of 20 dB below current requirements (FAR 36). The study showed that the optimum configuration was a low tip-speed, two-stage fan with a low hub/tip ratio [ref. 1]. The optimum pressure ratio was 1.9 and the tip speed was 365.8 m/sec (1200 ft/sec). Under current program, Contract NAS3-16811, this optimum fan is to be designed, constructed, and tested.

Several features that have the potential for minimizing noise were incorporated in this two-stage fan. These features include substantial axial spacing between blades and vanes, proper relationship of the number of blades and vanes, extensive use of acoustic treatment in casing walls and in a flowpath exit acoustic splitter, and a sonic inlet device using a translating centerbody.

Aerodynamic conditions for the fan are within the range of data obtained on two earlier, successful NASA-Lewis sponsored research fans tested by P&WA: 1) a 304.8 m/sec (1000 ft/sec) tip-speed, low-noise, single-stage fan [ref. 2] and 2) a two-stage, 442.0 m/sec (1450 ft/sec) tip-speed fan [ref. 3]. The information obtained from these two previous programs provide a solid foundation for performance predictions and for selection of blade and vane sections for the current design.

This report presents details of the aerodynamic, structural, and acoustic design of the current two-stage fan. Special terms, abbreviations, and symbols used in this report are defined in Appendix A.

## AERODYNAMIC-ACOUSTIC CONSIDERATIONS

Both general design parameters and detailed elements of the fan design were significantly affected by the need to incorporate low noise features. A low tip-speed of 365.8 m/sec (1200 ft/sec) and moderate blade loadings were selected for low noise. As a result, two stages were required to obtain the design pressure ratio. A rather high fan-flow/unit-annulus-area of  $209.2 \text{ kg/sec/m}^2$  ( $42.85 \text{ lbm/sec/ft}^2$ ) was chosen consistent with low engine frontal area and minimum diffusion from sonic inlet throat to fan inlet. The numbers of blades and vanes were chosen to restrict propagation of interaction tone noise at blade-passing frequency and yet maintain the desired solidities. These aerodynamic-acoustic considerations imposed a blade number relationship of  $s = 2r + 6$ , where  $s$  is the number of stator vanes in a given stage and  $r$  the number of upstream rotor blades. To reduce blade-passing tone noise, axial spacings between blade and vane rows were set such that at all spanwise positions the leading edge of each blade row is a minimum of two aerodynamic chords downstream of the trailing edge of the upstream blade. Constant diameter casing wall sections are provided between blade rows to permit tests with alternate spacings and to facilitate incorporation of wall acoustic treatments. Fan exit ducting was designed to include a removable acoustically treated flow splitter as well as wall treatments. A two-ring, acoustic inlet was initially selected to aid in suppression of forward radiated noise; however, this effort was discontinued in favor of a translating centerbody sonic inlet device. Acoustic treatments were also included in the inlet casing walls.

## FLOWPATH AND VELOCITY VECTOR DIAGRAM DESIGN

General aerodynamic design parameters (Table I) for the two-stage low noise fan were chosen to conform with contract requirements, to provide similarity with advanced-technology NASA fan-stages of proven high performance, and to permit the use of existing hardware and test facilities. Because this fan is for application in an engine with a rather high bypass ratio, representative aerodynamic and acoustic data can be obtained without splitting the duct and core flow at the fan exit.

TABLE I  
GENERAL AERODYNAMIC DESIGN PARAMETERS

	CONTRACT WORK STATEMENT	DESIGN
Overall Total Pressure Ratio	1.8-2.0	1.90
Overall Adiabatic Efficiency (%)	-	85.3
Parameters at Inlet to First Rotor:		
Tip Diameter - meters (inches)	0.762 (30) (min.)	0.836 (32.90)
Tip Speed - m/sec (ft/sec)	335.3-396.2 (1100-1300)	365.8 (1200)
Hub/Tip Ratio	0.4 (approx)	0.4
Specific Flow - kg/sec/m <sup>2</sup> (lbm/sec/ft <sup>2</sup> )	-	209.2 (42.85)
Corrected Flow - kg/sec (lbm/sec)	-	96.39 (212.5)
Corrected Speed (rpm)	-	8367

## DESIGN ITERATIONS

The flowpath and velocity vectors used to design the rotor and stator blade elements of the fan were determined from a series of iterations. The iterations were started using a reasonable flowpath shape and general design parameters consistent with requirements for a high bypass ratio turbofan engine, together with estimated efficiency profiles and flow blockages. Velocity vectors and flow conditions were then calculated by a computation system that provides an axisymmetric, compressible flow solution of continuity, energy, and radial equilibrium equations, with curvature, enthalpy, and entropy gradient terms included in the equilibrium equation [Appendix A of ref. 4]. To control velocities and loadings and to maximize predicted stall margin, a series of streamline analysis program runs was used to adjust flowpath shape, blade solidities, and spanwise total pressure slopes. Losses were reestimated using correlations of loss versus Mach number and loading for each significant

aerodynamic change. Stall margin was estimated by using the flowfield calculation to predict blade loading increases as the fan is back-pressured and by using loading limits established from test data as criteria for stall. The final set of design velocity vectors, together with assumed solidities and numbers of blades, was then used in the design of rotor and stator blade elements. Stress and vibration analyses were performed concurrently with the aerodynamic design to insure that the aerodynamic design would be compatible with mechanical design criteria. In subsequent flowpath and velocity vector iterations, calculation stations were revised to conform to actual leading and trailing edge locations of each blade and vane row and to retain desired axial spacings between blade rows. Performance parameters at the design point are summarized in Table II.

TABLE II  
DESIGN PERFORMANCE

	PRESSURE RATIO		ADIABATIC EFFICIENCY	
	Local (per blade row)	Cumulative	Local (per blade row)	Cumulative
<b>Blade Row</b>				
Rotor 1	1.485	1.485	89.5%	89.5%
Stator 1	0.984	1.461		85.6%
Rotor 2	1.317	1.924	90.9%	87.3%
Stator 2	0.987	1.898		85.3%
<b>Stage</b>				
First	1.461		85.6%	
Second	1.298		86.1%	

## LOSSES

Design values of rotor loss (Figure 1, lower set of curves) were estimated using a correlation of total loss versus inlet relative Mach number and loading based on fan rotor test data. No additional losses were added in the partspan shroud regions. Design stator losses (Figure 1, upper set of curves) were based on data correlated as loss parameter versus diffusion factor and percent span. A comparison of the final estimated values of rotor and stator design losses with data<sup>†</sup> from tests of the 304.8 m/sec (1000 ft/sec) single-stage [ref. 5] and the 442.0 m/sec (1450 ft/sec) two-stage [ref. 3] NASA fans is also shown in Figure 1. The corresponding spanwise profiles of rotor adiabatic efficiency are given in Figure 2.

## FLOW BLOCKAGES

Flow blockages were included in the aerodynamic design to account for boundary layer growth on casing walls and to account for the presence of a partspan shroud on each rotor. Blockages due to casing boundary layers at the fan inlet were calculated from analytical predictions of displacement thicknesses. Wall boundary layer growth through the blade rows was estimated from test data from the 442.0 m/sec (1450 ft/sec) fan which achieved its design flow rate [ref. 3]. In addition, to account for the presence of the rotor partspan

<sup>†</sup> Unless otherwise indicated, all data shown in comparisons are for test points at design speed on an operating line passing through the design point of the referenced fan.

shrouds, a blockage equal to the percent of annulus area occupied by each shroud was applied at the exit of the rotors, and approximately one-fourth of this amount was used at the inlet of each rotor. In calculating the design velocity vectors and flow conditions, the total blockages listed in Table III were applied equally to all stream tubes at each of the indicated axial locations.

**TABLE III**  
**FLOW BLOCKAGES (% OF ANNULUS AREA)**  
**AT BLADE EDGE AXIAL LOCATIONS**

LOCATION	TOTAL BLOCKAGE
R1 L. E.	2.6
R1 T. E.	4.9
S1 L. E.	3.1
S1 T. E.	3.3
R2 L. E.	3.7
R2 T. E.	6.1
S2 L. E.	4.3
S2 T. E.	4.6

### **AIR ANGLES AND VELOCITIES**

The fan was designed with a constant tip diameter to allow all the flowpath convergence to be taken at the root of the flowpath, which tends to minimize critical root-loadings and the large past-axial turnings inherent in a low speed, low hub/tip ratio fan rotor. As shown in spanwise profiles of flow angle (Figure 3), the first-stage rotor is designed to turn the flow approximately 30 degrees past axial at the root, about 10 degrees less than the rotor design value of the 304.8 m/sec (1000 ft/sec) fan [ref. 6].

Fan exit flow (aft fan-duct) is axial, as specified by contract, and the annulus area is set to provide an average exit Mach number of about 0.40, a practical value for effective noise treatment and for low losses from struts and ducting downstream of the fan. Flowpath convergence and curvature of the inner casing walls between the inlet spinner and fan exit were used to control velocity profiles and blade aerodynamic loadings (diffusion factors). Resulting profiles of meridional velocity and Mach number at leading and trailing edges of blade rows are shown in Figures 4 through 7.

### **FLOWPATH SPACINGS**

Two flowpath configurations are shown in Figure 8. The lower configuration is the basic test configuration, and the upper configuration is an alternate configuration with more

closely spaced blade rows. To reduce noise associated with blade-vane wake interactions, the axial spacings between adjacent blade rows of the basic flowpath (wide blade-spacing, lower configuration) were set such that at all spanwise positions the leading edge of each blade row is a minimum of two aerodynamic chords downstream of the trailing edge of the upstream blade row. Constant radius hub sections were specified between blade rows to facilitate the use of spacers for increasing or decreasing axial lengths between blade rows for alternate test configurations. The alternate configuration, the upper configuration in Figure 8, has axial spacings between successive blade rows of 1, 1, and 2 aerodynamic chords and an overall length approximately 0.17 m (6.5 in.) less than that of the basic configuration. Streamline analysis calculations indicate that velocity vectors for the two configurations are substantially the same and, hence, no significant differences in aerodynamic performance are predicted.

A schematic showing the mechanical layout of the rig is presented in Figure 9.

## LOADINGS

Spanwise profiles of design diffusion factors for the current fan are compared in Figures 10 and 11 with the diffusion factors that had been obtained from tests of the two previous research fans. The Figures show that the average loadings of the current fan are lower than those of the 304.8 m/sec (1000 ft/sec) single-stage fan [ref. 5] and the 442.0 m/sec (1450 ft/sec) two-stage fan [ref. 3] at test points where each was operating with a practical stall margin and high efficiency. Considerable effort was devoted to balancing the design loadings among blade rows to achieve maximum predicted stall margin. Parameters which were varied in these attempts include hub casing contours, average total pressure ratios and spanwise total pressure slopes of each rotor, and first-stage stator exit air angles. Stall margin was estimated by using the flowfield calculation to predict blade loading increases as the fan is back-pressured and using loading limits established from test data as criteria for surge. The fan stall margin obtained with this method, which in previous applications has given good agreement with test values, is about 18 percent. The predicted fan stall was set by the second-stage stator hub which reached diffusion factor levels of 0.65, considered the loading limit for stators.

The resulting higher loadings and design pressure ratios of the first-stage relative to second-stage, as shown in Figures 10, 11 and 12, reflect a provision for an anticipated, more rapid increase of second-stage blade loadings with an increase in fan back-pressure. Radial profiles of total pressure were sloped negatively (i.e., higher pressure near the hub than near the tip) to obtain high velocities on the hub wall to reduce critical loadings. Also, as part of the attempt to achieve a desirable loading balance, flow angles were set at 7.5 degrees at the exit of the first-stage stator (Figure 13).

The predicted loadings for the four blade-rows at the estimated stall point are presented in Table IV below.

**TABLE IV**  
**PREDICTED BLADE AERODYNAMIC DIFFUSION FACTORS AT STALL**

	HUB (5% Flow)	MEAN (50% Flow)	TIP (90% Flow)
Rotor 1	0.55	0.55	0.51
Stator 1	0.62	0.46	0.45
Rotor 2	0.61	0.47	0.42
Stator 2	0.65	0.47	0.50

Tabulations of aerodynamic parameters at rotor and stator leading and trailing edges are provided in Appendix B (Tables XVI to XIX).

### EXIT DUCT AERODYNAMIC DESIGN

The exit ducting and acoustic splitter contours for the fan were selected: 1) to provide conical casing surfaces convenient for incorporation of acoustic treatment, 2) to control Mach numbers for low losses and low noise, and 3) to allow use of existing rig hardware. Blockages were included in the flowfield calculation in order to account for boundary layer growth along the four flow-surfaces of the exit duct, and annulus areas were gradually increased along the duct to compensate for boundary layer growth to hold a Mach number of about 0.4 throughout the duct at the design point. The boundary layer parameters were estimated from limited test-data on flow over a perforated plate which is qualitatively similar to the acoustic treatments of the present design. Annulus blockages were set somewhat higher than are probably required, which should provide ability to operate at lower than design back pressure without choking of the flow in aft portions of the duct. Exit duct blockage values are listed in Table V. Use of these parameters and of an existing inner support structure resulted in the nearly parallel sloped duct casing walls and splitter contours as shown in Figure 14.

**TABLE V**  
**FLOW BLOCKAGES ASSUMED FOR EXIT DUCT DESIGN (% OF ANNULUS AREA)**

AXIAL LOCATION FROM ROTOR 1 ROOT L.E. REFERENCE PLANE		TOTAL BLOCKAGE
(Meter)	(inch)	(%)
1.0363	40.8	5.6
1.0668	42.0	6.0
1.3208	52.0	7.3
1.5748	62.0	8.9
1.8288	72.0	10.5
2.0930	82.4	12.2
2.3368	92.0	12.2

Splitter geometry was determined from acoustic treatment dimensions, which set splitter thickness at 0.0157 m (0.62 in.), and from the previously discussed Mach number considerations. The splitter nose was designed as an ellipse with a ratio of semi-major to semi-minor axis of 2.5:1, and the splitter trailing edge was designed as a boattail with a 15-degree included angle. In order to reduce the splitter incidence angle, and hence to eliminate undesirable flow separations at the fan aerodynamic design point, the splitter nose was inclined at an angle of 3 degrees with respect to the rig centerline as compared to a 7-degree angle for the major portion of the splitter. The splitter is supported by two sets of five struts which are circumferentially aligned with five exit duct support struts (Figure 14). These struts are contoured as 400 series airfoils.

## AIRFOIL DESIGN

### ROTORS

#### Airfoil Series

Rotor blades for both stages of the fan were designed using multiple-circular-arc (MCA) airfoils generated on conical surfaces which approximate streamsurfaces of revolution. As shown in Figure 15, each MCA airfoil section is defined by specifying a value of total chord, front chord, total camber, front camber, maximum thickness and its chordwise location, and leading and trailing edge radii. Blades of this airfoil series have been used successfully in several applications, providing much useful test data for design of airfoils in the transonic and high subsonic Mach number regimes. Such data have been applied to the present design.

#### Partspan Shrouds

Both rotors have a partspan shroud to provide mechanical stability. These shrouds are located at 66.5 and 60 percent span from the hub of rotor 1 and rotor 2, respectively, with relative spanwise positions chosen such that the second-stage rotor shroud lies approximately in line with the expected wakes from the first-stage rotor shroud, thus minimizing total loss and other aerodynamic penalties normally associated with the shrouds.

#### Chords, Thicknesses, and Numbers of Blades

A summary of rotor blading parameters is given in Table VI. Chords, solidities, and numbers of blades were chosen to be consistent with acceptable aerodynamic loadings, moderate axial lengths, structural requirements, low noise, and previous experience. In particular, to restrict propagation of blade-vane interaction noise, the numbers of blades and vanes were selected according to the relation  $s = 2r + 6$ , where  $s$  is the number of stator vanes in a given stage and  $r$  the number of upstream rotor blades. The number of rotor 1 blades was determined according to the relation  $s = 2r + 6$ , where  $s$  is the number of stator vanes in a given stage and  $r$  the number of upstream rotor blades. The number of rotor 1 blades was determined flutter-free operation and by maximum solidity limits which were set by channel flow area requirements. The number of rotor 2 blades was selected to provide a 5:4 ratio for the number-of-rotor-2 blades to the number-of-rotor-1 blades to give desirable fan noise characteristics (see the Acoustic Design Section).

TABLE VI  
ROTOR BLADING PARAMETERS

	R1	R2
Number of Airfoils	28	35
Airfoil Series	MCA	MCA
Aspect Ratio <sup>(1)</sup>	2.75	2.54
Aspect Ratio <sup>(2)</sup>	2.19	2.21
Taper Ratio <sup>(3)</sup>	1.232	1.028
Hub Chord - meter (inch)	0.0897 (3.530)	0.0859 (3.382)
Tip Chord - meter (inch)	0.1105 (4.350)	0.0883 (3.476)
Tip Solidity	1.18	1.18
Hub Solidity	2.28	2.14

- (1) Average length/axially projected hub chord  
(2) Average length/chord at tip  
(3) Tip chord/hub chord

Rotor maximum-thickness to chord ratios,  $t/c$ , (Figure 16) were selected to provide mechanical stability while maintaining minimum airflow blockage. The chordwise locations of maximum thickness for both rotors (Figure 17) were set to give the blades the minimum possible leading edge wedge angles without creating cusp-shapes in the front portion of the blades. Rotor total chords and front chords are shown in Figure 18.

### Incidence and Deviation Angles

Rotor leading and trailing edge metal angles (Figure 19) were determined from application of incidence and deviation criteria to the design velocity vectors. For rotor airfoil sections whose inlet relative Mach number exceeded 1.0, incidence angles ( $i_{ssa}$ ) were set at a location halfway between the leading edge and the point from which a Mach wave emanates that meets the leading edge of the following blade. A nominal design value of  $i_{ssa}$  of 1.5 degrees was chosen to account for development of the suction surface boundary layer, blockage at the blade leading edge, and bow wave losses. Actual values of incidence for rotors of the subject design (Figure 20) varied between approximately 1.0 and 2.4 degrees, the variation resulting from a selection of geometry to fulfill channel area requirements and to provide smooth blades. For subsonic sections, incidences were chosen at the leading edge at values consistent with minimum loss data from previous tests and with smooth distributions of blade geometry.

Rotor deviation angles were calculated using P&WA's cascade method modified by correction factors based on applicable rotor test data. Figure 21 shows the predicted deviations and comparisons with deviation angles calculated using Carter's Rule.

### Channel Areas

To provide sufficient fan flow capacity while allowing the rotors to operate near minimum loss, the minimum critical area ratio  $(A/A^*)_{\min.}$  in channels between adjacent blades for both rotors (Figure 22) was set at approximately 1.03 over most of the span. Desired channel areas were obtained by varying the chordwise distribution of airfoil camber. Near the location of each shroud, front camber was increased to provide higher values of  $(A/A^*)_{\min.}$ . In calculating  $A^*$  through the blade channels, losses were distributed in the following manner: no loss was applied ahead of the assumed normal shock at the blade passage entrance, a normal shock loss was applied at the blade passage entrance, and the remaining loss was distributed linearly through the rest of the channel.

The resulting profiles of front camber angle and chord-camber parameter are shown in Figure 23. Distributions of flow area ratio through the blade channels of both rotors are shown in Figure 24 for several spanwise locations. The distinctive shape of the  $A/A^*$  distribution at the root of rotor 1 is typical of a rotor root with past-axial turning [ref. 6].

### Rotor Geometry

Rotor geometry on design conical surfaces is summarized in Appendix C (Tables XX and XXII); for each airfoil section, two values of total and front camber are tabulated. Figure 25 gives a polar representation of a blade mean-camber-line and the two definitions used to calculate these values of camber. For manufacturing purposes, the airfoil sections were redefined on planes normal to the stacking line, a radial line through the center of gravity of the root conical section. Rotor blade coordinates for these redefined sections are tabulated in Appendix D (Tables XXIV and XXVI), and Figure 26 gives the airfoil coordinate definitions used in these tabulations.

## STATORS

### Airfoil Series

MCA airfoils were also used in design of the first-stage stator vanes since this series of airfoils offers greater control of channel area than more conventional airfoil series and the potential for lower stator losses at the rather high stator root inlet Mach numbers of the present design. The second-stage stators were designed as 65/CA vanes (circular arc meanline with 65 series thickness distribution) since these vanes will operate with inlet Mach numbers less than 0.65, a regime where 65/CA airfoils have low losses.

### Chords and Thicknesses

A summary of stator blading parameters is given in Table VII. To restrict propagation of blade-vane interaction noise, the numbers of vanes were selected according to the relation

$s = 2r + 6$  as discussed under Rotors. Stator chords and the locations of maximum thickness for both stators are shown in Figures 27 and 28. To provide low stator losses, maximum thickness-to-chord ratios were set at minimum values consistent with structural requirements. These thickness ratios (Figure 29) are somewhat higher than those for stators tested in previous NASA fans because of the higher aspect ratios of the present design. Any loss penalties should be small, however, since most of the thicker airfoils will operate with rather low inlet Mach numbers.

TABLE VII  
STATOR BLADING PARAMETERS

	S1	S2
Number of Airfoils	62	76
Airfoil Series	MCA	65/CA
Aspect Ratio <sup>(1)</sup>	5.03	3.89
Aspect Ratio <sup>(2)</sup>	3.81	3.73
Taper Ratio <sup>(3)</sup>	1.099	0.9709
Hub Chord - meter (inch)	0.0513 (2.020)	0.0489 (1.930)
Tip Chord - meter (inch)	0.0564 (2.220)	0.0475 (1.8707)
Tip Solidity	1.33	1.38
Hub Solidity	2.50	2.46

(1) Average length/axially projected hub chord  
(2) Average length/chord at tip  
(3) Tip-chord/hub chord

#### Incidence and Deviation Angles

Selection of design incidence angles and calculation of deviation angles for both stators (Figures 30 and 31) were based on P&WA's cascade system and minimum loss data from previous tests. The resulting metal angles are shown in Figure 32.

#### Channel Areas

Minimum values of channel area ratio  $(A/A^*)_{\min}$  near the stator 1 hub were set a few percent above the  $A/A^*$  for the corresponding stator inlet Mach number (Figure 33) according to a correlation of capture-area/throat-area ratio at minimum loss as a function of stator inlet Mach number [ref. 7]. The outer half of the blade has a front camber selected to give nearly

double-circular-arc (DCA) airfoils for this low Mach number portion of the vane. The resulting profiles of front camber and chord-camber parameter are shown in Figure 34, and the channel distributions of  $A/A^*$  for stator 1 are given in Figure 35. Channel area ratio was not a critical parameter in the design of stator 2 airfoils since the inlet Mach numbers are sufficiently low (0.50 - 0.65) that choking problems should not be encountered with the vanes selected by means of the P&WA correlation of cascade data.

### Stator Geometry

Stator geometry on design conical surfaces is summarized in Appendix C (Tables XXI and XXIII). For manufacturing purposes, the airfoil sections were defined on planes normal to a radial (stacking) line. The resulting blade coordinates are presented in Appendix D (Tables XXV and XXVII).

## INLET AERODYNAMIC DESIGN

### OBJECTIVES AND TECHNIQUES

The purpose of the inlet aerodynamic designs is to provide inlet configurations that meet the program acoustical requirements while providing a minimum length in order to approach practical requirements of aircraft installation. Two inlet configurations were chosen for the program: a baseline standard inlet cowl configuration and a translating plug, choked (sonic) inlet configuration. Contours of these two configurations are shown in Figure 36.

The principal reason a translating centerbody, sonic inlet was chosen is because it provides a means of controlling flow area to achieve throat Mach numbers that give the desired noise suppression for a range of fan operating conditions. Furthermore, this configuration requires a minimum inlet length without excessive boundary layer growth or separation. Originally a two-ring, acoustic inlet had been selected; however, that design was discarded when the sonic inlet configuration was decided upon. A summary of the limited work done on the two-ring inlet is provided in Appendix E.

An inlet fabricated previously for another program is to be used as the baseline standard inlet cowl. This inlet provides a one-dimensional throat Mach number of 0.68 and has an inlet-length to fan-tip-diameter ratio ( $L/D$ ) of 1.03 and an overall contraction ratio ( $A_{\text{highlight}}/A_{\text{throat}}$ ) of 1.65 — "highlight" is defined as the farthest forward point on the inlet cowl (Figure 36). The aerodynamic contours of the sonic inlet were designed using a transonic axisymmetric flow analysis and a modified Reshotko-Tucker mass-momentum integral boundary layer solution. The inlet contours for both the baseline and sonic inlet configurations were selected to minimize the velocity overspeed along the surface downstream of the throat which should result in the best diffuser performance with the least distortion at the fan face.

It should be noted that the inlet flow for the aircraft approach condition used in the aerodynamic design of the sonic inlet was assumed to be 80 percent of design flow, which is believed to be the lowest practical flow for a sonic inlet design within present constraints.

Any lower flow assumption would necessitate lengthening the inlet beyond practical mechanical and flight engine limits. The 80 percent design flow condition is theoretically possible with a variable, fan-duct nozzle, permitting fan operation at a higher speed (approximately 80 percent design speed) and a lower pressure ratio (1.19) at the desired thrust condition for aircraft approach.

The geometries of the fixed outer inlet cowl and the inner translating centerbody are shown in Figure 36 in the fully extended, intermediate, and fully retracted positions. These positions are specified as the approach position at 80 percent design flow, the takeoff position at 92.6 percent design flow, and the cruise position at 100 percent design flow. The one-dimensional throat Mach numbers associated with these positions are respectively 0.9, 0.9, and 0.71.

## **SONIC INLET GEOMETRY**

### **Inlet Cowling and Centerbody**

Since the fan aerodynamic design was essentially complete when the sonic inlet aerodynamic design was initiated, the inlet design had to be compromised to retain the fan root flow angle associated with the conventional spinner. This resulted in an overall inlet length of about 1.2 meters (47.5 inches) for an inlet-length to fan-tip-diameter ratio ( $L/D$ ) approximately 1.45, which is somewhat larger than 1.0, the maximum ratio judged practical for a flight application. An  $L/D$  ratio of 1.0 would have been possible had it not been necessary to diffuse the inlet flow to a rather high area in order to retain the fan root platform contour.

A 0.0032 meter (0.25 inch) truncation, or step, was added at the trailing edge of the centerbody to improve boundary layer characteristics in the region where the centerbody meets the fan spinner (Figure 36). The maximum centerbody radius was set at 0.19 meter (7.39 inches) at the throat of the inlet. The minimum cowl radius was set at 0.37 meter (14.55 inches) at an axial station 1.02 meters (40.0 inches) upstream of the first-stage rotor hub leading edge (reference plane).

### **Sonic Inlet Lip Shape**

Since the sonic inlet is to be tested at static conditions only, an attempt was made to reproduce, as nearly as possible, the accelerations on the inlet surface which would be encountered at aircraft approach flight conditions. This was done by generating a 2.5:1 elliptical shape from the throat to approximately the inlet highlite station and then blending this contour to a circular arc by making them tangent and continuing the circular arc to complete the inlet contour. The overall contraction ratio ( $A_{\text{highlite}}/A_{\text{throat}}$ ) of this configuration is equal to 1.45.

## **INLET MACH NUMBER DISTRIBUTIONS, BOUNDARY LAYER CHARACTERISTICS, AND ESTIMATED PRESSURES RECOVERIES**

The outer wall Mach number and the boundary layer shape factor distributions were calculated for the baseline standard inlet configuration, and the results are shown in Figure 37 for the 100 percent speed, cruise flight condition. The shape factors are well under the separation limit of 2.2 to 2.5.

For the sonic inlet configuration, attempts were made to obtain a uniform Mach number profile at the inlet throat to meet acoustic criteria. As shown in Figure 38, the desired flat profile was achieved for the approach configuration at the throat, an axial distance of 1.016 meters (40 inches) upstream of the rotor 1 hub leading edge.

Mach number and shape factor distributions along the sonic inlet walls for the approach, cruise, and takeoff positions are shown in Figures 39 through 44. The Mach numbers along both inner and outer walls for the approach configuration (Figure 39) are quite similar, showing a peak Mach number of approximately 0.92 near the throat of the inlet, while peak Mach numbers for the cruise configuration (Figure 40) are 0.77 and 0.83 for the inner and outer walls, respectively. At takeoff (Figure 41), the inner wall Mach number reaches a peak of 0.98 near the inlet throat while the outer wall value is 0.81 at this location.

The shape factors for the wall boundary layers shown in Figure 42 for the cruise configuration indicate a stable boundary layer on the outer wall, but the inner wall boundary layer deteriorates rapidly as the flow approaches the centerbody truncation. This deterioration could lead to locally separated flow in this region — separation is indicated when shape factor reaches values of 2.2 to 2.5. This would, however, be followed by a reacceleration and reattachment of the flow on the spinner surface. A similar deterioration of shape factor in the area of centerbody and plug shaft truncation for the approach configuration is indicated in Figure 43 and an improvement in the boundary layer can be noted as the constant area portion of the inlet duct is reached; additional improvement will occur as the flow accelerates around the spinner. The takeoff configuration shown in Figure 44 has shape factor distributions similar to the cruise condition with the inner wall approaching a critically high value (2.17) near the intersection of the centerbody spinner. As in the cruise condition, the flow is expected to reattach on the spinner if any local separation occurs.

Baseline and sonic inlet total pressure recoveries were estimated from the analytical boundary layer solution and are presented in Table VIII.

**TABLE VIII**  
**BASELINE AND SONIC INLET TOTAL PRESSURE RECOVERIES**

INLET CONFIGURATION	FLOW CONDITION		TOTAL PRESSURE RECOVERY
	(%W $\sqrt{\theta/\delta}$ )	(Throat Mach No.)	
Baseline, Cruise	100	0.68	0.993
Sonic, T/O	92.0	0.90	0.975
Sonic, Cruise	100	0.71	0.987
Sonic, Approach	80	0.70	0.970

### STRUCTURAL AND VIBRATION ANALYSIS

Design of the fan blading included structural and vibration analyses to determine configurations that satisfy mechanical design requirements. The analyses included calculation of: blade-disk frequencies and their resonances with rig excitations, steady-state stresses, blade-vane flutter parameters, rig critical speeds, and full rotor system response due to imbalance at the rotor 1 location.

The material for rotor 1 blades is AMS 4973F (titanium alloy) and for rotor 2 blades is AMS 4928 (titanium alloy). The material for the stator vanes is AMS 5613 (stainless steel), and the material for the disks, hubs, spacers, and seals is AMS 5616 (stainless steel).

## **ROTORS**

### **Blade and Disk Vibration**

A partspan shroud is required for each rotor to avoid first bending resonances with first and second order rig-frequencies in the operating range. The airfoil geometry and shroud location were chosen to provide the best compromise between high speed margin with a 3E resonance (3E = 3 excitations per rotor revolution) and the speed at which a 4E resonance would occur. The shroud location selected for rotor 1 (i.e., 66.5 percent span from the hub) gives this rotor a predicted 5.6 percent 1st coupled mode (bending and torsion) 3E resonance frequency margin at 105 percent of design speed and positions the 1st coupled mode 4E resonance at 75 percent design speed (Figure 45). For rotor 1, no 2nd coupled mode or 3rd coupled mode critical resonances exist in the operating range.

During sonic inlet testing, the five support struts for the translating centerbody will create a 5E, 1st mode resonance on rotor 1 at 4800 rpm (Figure 45). This resonance is not considered a problem because the inlet struts are 0.254 meter (10 inches) forward of rotor 1 leading edge and the resonance occurs low in the speed range where the excitation energy is low.

The second-stage rotor, with a shroud location at 60 percent span from the hub, has a 1st coupled mode 3E resonance frequency margin of 5.4 percent and a 1st coupled mode 4E resonance at 72 percent design speed (Figure 46). For rotor 2, no 2nd coupled mode or 3rd coupled mode critical resonances exist in the operating range. The 5.6 and 5.4 percent margins on 1st coupled mode 3E resonance are adequate, based on previous test results that have shown good correlation with design predictions. Moreover, increasing these margins on 3E resonance would position the 1st coupled mode 4E resonance at higher speeds in the operating range. Due to these limiting 3E margins, the operational speed of the fan will be held to 105 percent corrected design speed during the test program.

Rotor blade tip chordwise bending modes are of great concern with the thin tip sections of modern fan blades. Excitations from inlet struts and stator vanes upstream and downstream of the rotor can interact with the natural frequency of these tip chordwise modes to produce high dynamic stresses. Figures 47 and 48 show that the tip chordwise bending mode resonances will not occur in the critical portion of the speed range (70 - 105 percent of design speed).

### **Rotor Blade Stresses**

Stresses due to centrifugal forces, air loads, and untwist forces were calculated for 105 percent of design speed, and the results are shown in Table IX. The allowable stresses for the blade material based on 338.6°K (150°F) metal temperature for rotor 1 and 421.9°K (300°F)

metal temperature for rotor 2 are also shown in this table. The maximum combined stresses of  $3.24 \times 10^8 \text{ N/m}^2$  (47,000 lbf/in.<sup>2</sup>) for rotor 1 and  $2.03 \times 10^8 \text{ N/m}^2$  (29,500 lbf/in.<sup>2</sup>) for rotor 2 are comparable to stress levels present in experimental and production blades and are well below the allowable stresses.

Gas bending stresses with centrifugal restorations were calculated at 105 percent of design speed. Airfoil stresses were minimized for the combination of load and no load conditions. The selected axial and tangential tilt of 0.00107 meter (0.042 inch) results in a maximum stress of  $4.1 \times 10^7 \text{ N/m}^2$  (6,000 lbf/in.<sup>2</sup>) for rotor 1 and  $2.8 \times 10^7 \text{ N/m}^2$  (4,000 lbf/in.<sup>2</sup>) for rotor 2.

TABLE IX  
SUMMARY OF ROTOR STEADY STRESSES

105% of Design Speed –  $\text{N/m}^2 \times 10^{-7}$  (lbf/in.<sup>2</sup>  $\times 10^{-3}$ )

	ROTOR 1	ROTOR 2
P/A	20.0 (29)	14.5 (21)
Centrifugal Untwist	8.3 (12)	3.1 (4.5)
Gas Bending	4.1 (6)	2.8 (4)
Combined	32.4 (47)	20.3 (29.5)
Allowable	60.7 (88)	53.1 (77)

Modified Goodman diagrams (Figures 49 and 50) indicate that at the maximum steady stress points the maximum allowable vibratory stresses for rotors 1 and 2 are  $10.67 \times 10^7$  (15,500 lbf/in.<sup>2</sup>) and  $12.72 \times 10^7 \text{ N/m}^2$  (18,500 lbf/in.<sup>2</sup>), respectively. During testing, a vibratory stress limit of  $6.89 \times 10^7 \text{ N/m}^2$  (10,000 lbf/in.<sup>2</sup>) will be imposed. Since no low order resonances are expected in the high speed operating range, the actual vibratory stress levels that will be encountered during testing should be less than the  $6.89 \times 10^7 \text{ N/m}^2$  (10,000 lbf/in.<sup>2</sup>) limit set as part of the test procedures.

### Rotor Blade Flutter

Flutter is a self-excited, self-sustaining vibration which occurs in either a torsional or bending mode or a combination of both. To prevent rotor blade flutter, a partspan shroud is required for each rotor of the two-stage fan. Values of flutter parameters for the shrouded blades were calculated at 105 percent of design speed, the operating speed considered most critical in regard to flutter, and these values were compared with correlated test data from previous programs. The calculated values of reduced-velocity parameters ( $2 V'_1 / c \omega_b$ ) and torsional-twist-to-bending-deflection ratio ( $\psi c/d$ ) for the 1st coupled mode flutter are summarized in Table X and lie within the range of P&WA experience where flutter problems have not been encountered. Values of reduced-velocity parameter ( $2 V'_1 / c \omega_t$ ) for torsional flutter, calculated at 105 percent speed (0.95 for rotor 1 and 1.2 for rotor 2) are also well within the range where flutter has not been experienced. The torsional frequency,  $\omega_t$ , is based on the entire blade.

TABLE X  
ROTOR FIRST COUPLED MODE FLUTTER PARAMETERS

ROTOR	REDUCED VELOCITY PARAMETER ( $2 V'_1/c \omega_b$ )	TORSIONAL TWIST/ BENDING DEFLECTION ( $\psi c/d$ )
1	2.75	0.16
2	3.05	0.14

### Partspan Shrouds

The partspan shrouds were sized and positioned to satisfy aerodynamic and structural requirements, including the 3E margin requirement. Shroud design parameters and stresses are summarized in Table XI, and a sketch of the shrouds is shown in Figure 51. Bearing stresses for the shroud are  $3.55 \times 10^7 \text{ N/m}^2$  (5,150 lbf/in.<sup>2</sup>) for rotor 1 and  $3.45 \times 10^7 \text{ N/m}^2$  (5,000 lbf/in.<sup>2</sup>) for rotor 2, which are below values tested successfully on P&WA research rigs, e.g.  $5.86 \times 10^7 \text{ N/m}^2$  (8500 lbf/in.<sup>2</sup>). The shrouds were designed to fit together sufficiently tight to provide adequate damping of vibrations without "shingling".

The  $Z^*$  ratios, a measure of the relative stiffnesses of the shroud and adjacent airfoil as defined in Appendix A, are within the realm of successful experience.

TABLE XI  
PARTSPAN SHROUD PARAMETERS  
(105% Speed)

	ROTOR 1	ROTOR 2
Spanwise Location (% Span From Hub)	66.5	60.0
Contact Angle - deg.	55.0	70.0
$Z^*$ Ratio	1.30	1.49
Bearing Stress - $\text{N/m}^2 \times 10^{-7}$ ( lbf/in. <sup>2</sup> )	3.55 (5,150)	3.45 (5,000)
Bending Stress - $\text{N/m}^2 \times 10^{-7}$ ( lbf/in. <sup>2</sup> )	40.0 (58,000)	29.1 (42,246)
Thickness - meter (inch)	0.005 (0.20)	0.0046 (0.18)

## Disk and Attachment Stresses

Conventional dovetail attachments were selected for the blades of both rotors. The calculated and allowable disk and attachment stresses for critical locations are listed in Table XII. All calculated values fall below the maximum allowed. In addition, the dynamic stress ratio (airfoil root stress divided by attachment stress) is above the minimum recommended value of 2.0, indicating that the attachment can withstand vibratory stresses greater than those the airfoil can tolerate.

TABLE XII  
ROTOR DISK AND ATTACHMENT STRESSES  
(105% Design Speed)

LOCATION	TYPE OF STRESS	CALCULATED STRESS/ALLOWABLE STRESS $\text{N/m}^2 \times 10^{-7}$ (lbf/in. <sup>2</sup> $\times 10^{-3}$ )	
		ROTOR 1	ROTOR 2
Blade Attachment	Combined	27.6/53.1 (40/77)	17.2/59.3 (25/86)
	Bearing	26.2/59.3 (38/86)	20.0/66.2 (29/96)
Disk	Tangential (avg.)	26.2/66.2 (38/96)	42.7/58.6 (62/85)
	Radial (max.)	15.9/53.8 (23/78)	11.0/47.6 (16/69)
Front Seal	Hoop	22.1/96.5 (32/140)	37.1/95.2 (53.8/138)
	Bending	4.1/96.5 (6/140)	13.8/95.2 (20/138)
Rear Seal	Hoop	22.1/96.5 (32/140)	37.1/95.2 (53.8/138)
	Bending	8.3/96.5 (12/140)	10.3/95.2 (15/138)

## STATORS

### Stator Vibration

Stator frequencies were calculated from a coupled bending-torsion analysis which included a model with the following end conditions:

- bending motion - moment restraint at airfoil hub and tip
- torsional motion - free at tip and restraint at spindle/actuation-arm junction (includes torsional flexibility of actuator arm).

As shown in Figures 52 and 53, the first two bending and torsion modes for stators 1 and 2 will not be excited by blade-passing orders in the operating range. Adequate margin on the first bending mode 3E resonance exists throughout the operating range and, based on past experience, higher order excitations should not result in vibrational problems.

### Stator Stresses

Stator vane bending stresses due to air loads were calculated at 105 percent design speed. The maximum bending stress for stator 1 was calculated as  $3.03 \times 10^8 \text{ N/m}^2$  (44,000 lbf/in.<sup>2</sup>)

and for stator 2 as  $2.99 \times 10^8 \text{ N/m}^2$  (53,500 lbf/in.<sup>2</sup>), which are considerably lower than the allowable stresses of  $58.6 \times 10^7 \text{ N/m}^2$  (85,000 lbf/in.<sup>2</sup>) and  $52.4 \times 10^7 \text{ N/m}^2$  (76,000 lbf/in.<sup>2</sup>) for stators 1 and 2, respectively. Stress allowables are based on vane material properties which are a function of metal temperatures. Vane metal temperatures used to determine allowable stresses for stator 1 and stator 2 are 65.56°C (150°F) and 148.89°C (300°F), respectively. Since no critical resonances are predicted in the operating range, vibratory stress levels are expected to be low. A maximum vibratory stress level of  $\pm 6.89 \times 10^7 \text{ N/m}^2$  ( $\pm 10,000 \text{ lbf/in.}^2$ ) will be imposed during test operation.

### Stator Flutter

Flutter parameters were calculated for both stators and compared with correlated test data. Values of the dimensionless reduced-velocity parameter for bending flutter ( $2V/c\omega_b$ ) calculated for stators 1 and 2 were 2.1 and 1.4, respectively, which are within the successful (no flutter) area determined through experience. A similar conclusion was indicated by the values of reduced-velocity parameter ( $2V/c\omega_t$ ) for torsional flutter, which were computed as 2.05 and 1.87 for stators 1 and 2, respectively.

### INTERSTAGE SEALS

The resonances were checked for the interstage rotor sideplate and stator seals (Figure 9) because of the long, cantilevered, stator inner-shrouds required for acoustic considerations. Frequencies of the seals were obtained from shell revolution structural analysis programs. The hoop stiffness effects of the stator inner shroud honeycomb construction were included in the vibration analysis. Resonances for all rotor and stator seals are above the 25 percent frequency margin requirement at 105 percent of design speed, as shown in Figures 54 and 55.

### SONIC INLET SUPPORT STRUTS

Frequencies were calculated for the fan inlet strut using fixed-end conditions. The resulting frequencies are shown in Figure 56. The blade passing frequency for rotor 1 does not excite the fundamental bending and torsion modes. There are no low order resonances (1E and 2E) in the operating range. Static load (one-G) plus the maximum aerodynamic load on the centerbody causes a maximum stress of  $2.95 \times 10^7 \text{ N/m}^2$  (4280 lbf/in.<sup>2</sup>) on the inlet struts at the inner and outer diameter fillet welds. This is well below the allowable stress of  $54.5 \times 10^7 \text{ N/m}^2$  (79,000 lbf/in.<sup>2</sup>) for the AMS 5613 material used. The dimensionless, reduced-velocity parameter ( $2V/c\omega_b$ ) for bending flutter was calculated to be 1.25, within the successful (no flutter) area determined through experience. The torsional flutter, reduced-velocity parameter ( $2V/c\omega_t$ ) was calculated to be 0.6, also in the stable area.

### CRITICAL SPEEDS AND FORCED RESPONSE

A rotor-frame critical-speed analysis was performed to determine the vibrational characteristics of the fan, with and without the sonic inlet configuration. The analysis was based on models which included all significant structural members of the rig and used the spring-mass system shown in Figure 57 for the baseline standard engine inlet cowling and Figure 58 for the sonic inlet.

## Baseline Standard Inlet Cowling Configuration

Two critical speeds occur within the rig operating range at 4811 rpm and 8764 rpm for the standard inlet cowling configuration. Two other critical speeds occur at 10,729 rpm and 15,777 rpm, which are above the expected maximum operating speed (8785 rpm). The mode shapes of the 4811 rpm, 8764 rpm and 10,729 rpm speeds are shown in Figure 59. The mode at 8764 rpm has only 1.6 percent of the total of the rotor strain energy and, hence, is of little concern. The modes at 4811 rpm and 10,729 rpm have significant motion of the fan rotors and have more than 25 percent of the total strain energy in the rotating components. To determine whether a bearing damper is needed to reduce the vibratory amplitudes of these modes, a forced response analysis was performed on the system with and without a front bearing damper for these two critical speeds. This analysis was similar to the critical-speed analysis except that an unbalance was simulated and the resultant vibratory deflections calculated. Deflections were calculated at the first-stage rotor plane and at the flexible diaphragm behind the second bearing for an unbalance of  $72 \times 10^{-5}$  kg-m (one oz-in.).

A damper was chosen for the front bearing due to the relatively high  $7.6 \times 10^{-4}$  m (0.030 in.) deflection at the rotor for a  $72 \times 10^{-5}$  kg-m (one oz-in.) unbalance at the lowest critical speed without a damper. The damper would reduce this sensitivity to  $0.13 \times 10^{-4}$  m (0.0005 in.) per  $72 \times 10^{-5}$  kg-m (one oz-in.). The rotor assembly will be balanced to better than  $36 \times 10^{-5}$  kg-m (0.05 oz-in.) unbalance but may reach  $17 \times 10^{-5}$  kg-m (0.25 oz-in.) during testing. This will give a maximum deflection of  $0.030 \times 10^{-4}$  m (0.00012 in.) at the rotor at 4811 rpm and  $0.46 \times 10^{-4}$  m (0.0018 in.) at 10,729 rpm, well within the tip clearance tolerance. Vibration accelerometers and amplitude pickups will be used to monitor rig and drive system vibration during testing.

## Sonic Inlet Configuration

The addition of the sonic inlet did not change the critical-speed predictions of the standard inlet fan although it did create two additional natural frequencies at 2215 rpm and 8909 rpm, both out of the normal operating range. The mode at 8909 rpm, although close to the 105 percent speed line, should not present a problem since only a rather small fraction of the rotor strain energy is involved.

An analysis was made to determine the amount of radial "closure" at the sonic inlet throat in its fully extended position due to static (one - G) stress and dynamic deflections at all critical speeds. A schematic is presented in Figure 60 defining radial closure and showing the relative locations of the centerbody and bearing supports. The static (one - G) radial closure at the throat is  $2.3 \times 10^{-4}$  m (0.009 in.). The maximum total inlet throat dynamic closure in the operating range due to a  $0.51 \times 10^{-4}$  m (0.002 in.) deflection at each bearing support is  $2.3 \times 10^{-4}$  m (0.009 in.) static plus  $2.5 \times 10^{-4}$  (0.010 in.) dynamic, for a total of  $4.8 \times 10^{-4}$  m (0.019 in.) occurring at 8685 rpm. This total deflection is judged to be acceptable, and the probability of any resulting wall-separation or inlet total pressure distortion should be minimal. The effect of structural damping, not included in this analysis, will reduce the dynamic deflections further.

## ACOUSTIC DESIGN

Known concepts of low noise turbofans were incorporated in the design of this two-stage fan. A low tip-speed and moderate design aerodynamic loadings were chosen to minimize generated noise. The number of blades and vanes were chosen to "cutoff" blade-passing tones, and an axial blade spacing of two chords was selected to minimize blade interaction noise. However, to meet the extremely low levels implied by FAR 36 minus 20 PNdB, the basically quiet fan must also incorporate extensive noise suppression in the inlet and exhaust duct. The noise spectra of the basic fan design were estimated, and the desired noise attenuations identified. Acoustic treatment was selected using both analytical and empirical models, and a final prediction of noise reduction was made. A sonic suppression device was selected to attenuate inlet radiated noise in lieu of inlet acoustic splitters (Appendix E). An aft acoustic splitter was incorporated to provide the required suppression of aft radiated noise.

### SONIC INLET, ACOUSTIC CONSIDERATIONS

An inlet operating with a completely choked throat does not transmit sound upstream. In a rig or engine, the exact variation of attenuation as throat Mach number increases toward 1.0 is a function of the details of the inlet design. Extensive information on this subject is available in the literature and from a variety of tests performed at Pratt & Whitney Aircraft. At full choke, the amount of attenuation that can be measured is not a function of design but depends on flanking path and background noise levels. The sonic inlet for this rig was designed for a Mach number of 0.9 with the capability of running at full choke or less. In order to allow operation at part-choke conditions for reduced distortion generation, a limited amount of acoustic treatment was incorporated in the sonic inlet design so that full-choke noise attenuation characteristics could be approximated. Selection and design of the sonic inlet for this rig were based on aerodynamic, structural and engine compatibility considerations that are described in the Inlet Aerodynamic Design section of this report. The only acoustic design criterion used was that the flow disturbances produced by the sonic inlet hardware be minimized so that aft-radiated fan interaction noise could be kept as low as possible.

A translating centerbody was selected as the most practical compromise among acoustic, aerodynamic, and mechanical design criteria. The centerbody will be tested in three axial-positions representing the ATT engine (STF 433 engine) [ref. 1] conditions of cruise (design), takeoff, and approach with the latter two positions having capability of sonic inlet Mach numbers.

### FLOWPATH AND BLADE GEOMETRY

To reduce the interaction tone noise at blade-passing frequency, the numbers of fan blades and vanes were chosen using the Tyler-Sofrin criterion [ref. 8] which specifies that if the number of stator vanes ( $s$ ) is greater than twice the number of rotor blades ( $r$ ), interaction noise generated at subsonic tip-speeds will decay within the inlet and exit ducts of a fan. The numbers actually selected (see Tables VI and VII) satisfy the relationship  $s = 2r + 6$  for all adjacent blade row combinations except stator -1/rotor -2 which, due to mechanical and aerodynamic constraints limiting the number of stator 1 vanes, satisfies the relationship  $s = 2r - 8$ .

Axial spacings between blade rows were selected to reduce a residual blade-passing tone noise associated with blade/vane wake interactions. As shown in Figure 61, this noise component decreases rapidly as spacing is increased up to two or three chord lengths relative to the upstream blade row. After two or three chords spacing, further reductions in noise cannot be obtained without severe weight and length penalties. The values selected for the configuration to be tested in the current program are two aerodynamic tip chord lengths; however, the capability for alternate closer spacing is provided in the mechanical design of the rig.

An additional noise control feature was incorporated in the fan design for psychoacoustic purposes. A ratio of blades  $35/28 (=5/4)$  in the two stages was chosen to avoid, as far as possible, dissonant chords usually present in multistage machines. This ratio is called a "major third" in musical theory and, by western standards, is considered "consonant". Psychoacoustic tests, using oscillators and a broadband noise generator, were run at P&WA to simulate a number of twin rotor builds. Rotor frequency ratios selected according to musical principles was found to produce less annoying spectra than those selected randomly, but this advantage held only at low frequencies, roughly below 1000 Hz. At higher frequencies typical of flight operations (approach and takeoff), the advantage of harmonious tones tended to disappear. However, the harmonic ratio concept was retained in the subject two-stage fan since it could do no harm and should provide a less annoying spectrum at speeds corresponding to some airport ground operating conditions, such as taxiing and idling.

## RIG SPECTRA PREDICTIONS

As in the case of the full scale ATT engine (STF 433), noise spectra for the two-stage rig were predicted using one-third octave band data for an existing two-stage fan engine, the JT3D. This procedure may appear to have a disadvantage in that the differences in the ratio of the number-of-rotor-2-blades/number-of-rotor-1-blades,  $35/32$  in the JT3D and  $35/28$  in the present rig, prevent accurate spectral simulation. However, the  $35/28 = 1.25$  ratio is sufficiently close to  $1.26 (\sqrt[3]{2})$  to insure that both rotor tones are in neighboring third octave bands, so that for purposes of PNdB calculations and for selecting sound absorbing liner parameters the predicted spectral shapes should be satisfactory.

To predict the rig spectrum at a particular condition (e.g., approach), the blade linear tip speed was found for the approach RPM. At this tip speed, fan data from the JT3D engine were selected. To convert these spectral data to the higher rig blade-passage frequencies, the one-third octave JT3D spectra were shifted to the right by the required number of third octaves.

Next, corrections for changes in size, blade-vane spacing, and pressure ratio were applied, as noted below. A correction of 2 dB was added to each frequency band to allow for the estimated increase in aft radiated noise associated with use of the sonic inlet. This amount was obtained from a set of choked inlet tests run on a JT8D engine in the late 1960's and represents both the backscattering at the sonic throat of forward propagating sound and additional noise generation caused by blade interaction with inlet flow velocity disturbances produced by the sonic inlet hardware.

The corrections mentioned above were as follows:

- Blade-vane spacing,  $\text{dB} = 10 \log (\text{projected chord ratio}) = -3.5 \text{ dB}$
- Fan size correction,  $\text{dB} = 20 \log (\text{diameter ratio}) = -3.9 \text{ dB}$
- Fan pressure ratio,  $\text{dB} = 20 \log (\text{pressure rise}) = +3.8 \text{ dB}$

The spacing correction was applied in the third octaves containing blade-passage tones; other corrections were applied across the spectrum. These corrections were based on results of an FAA funded fan noise research program (Contract No. DOT-FA69WA-2045) and extensive documentation of P&WA engine noise characteristics. They were incorporated into a computer program that predicts the spectral characteristics of study engines.

The resulting predicted rig source sound-pressure-level (SPL) spectra at a 45.7 m (150 ft) radius for the angle of maximum perceived-noise-level (PNL) aft of the rig are presented in Figure 62.

## TREATMENT ATTENUATION TARGETS

To determine the appropriate acoustic treatment, the dominant annoying frequency range first had to be identified. For the inlet, this is described under Acoustic Treatment Selection. For aft noise, the dominant annoying frequency range was determined from source noise spectra transformed into subjective "NOY" values. These spectra were simply truncated until a required integrated value of target attenuation was established for the aft noise. Since the full-scale engine study [ref. 1] predicted a level just at FAR 36, and the goal of this contract is to achieve levels of FAR 36 minus 20 PNdB, a target attenuation of 20 PNdB was set as the treatment goal. Figure 63 shows the resulting aft attenuation spectrum at approach and takeoff with a peak attenuation near 3500 Hz.

## ACOUSTIC TREATMENT SELECTION

### Inlet

To provide improved attenuation of forward-radiated noise during operation with the sonic inlet not at full choke, a limited amount of treatment was applied to the walls of the sonic inlet. The inlet treatment was designed to be mainly effective in absorbing the upstream traveling waves (i.e., treatment was tuned to attenuate waves propagating forward from within the fan). The forward attenuation spectrum expected from the inlet treatment is shown in Figure 64 and represents a perceived noise level of 3 PNdB.

The inlet treatment was restricted to axial locations where the wall Mach number does not exceed 0.7 at any of the operating points. Flow separation at the wall could occur because of surface roughness in a region of flow diffusion if the treatment had been extended to regions of higher Mach number. With the translating centerbody in the forward (approach) position, the lengths of treatment exposed are approximately 0.482 m (19 in.) on the inner wall and 0.599 m (22 in.) on the outer wall to provide a treatment length to passage height

ratio of about 1.6. Retraction of the centerbody covers the treatment on the inner wall and reduces the ratio by about one-half. Backing depth is 0.635 cm (0.25 in.) and design facing sheet percent open area is six percent both for the inner and outer wall treatments. These values were chosen, in accordance with methods described in the next section, to tune the inlet treatment to the center of the inlet attenuation target spectrum.

### Interstage and Aft Fan Duct

The treatment in the interstage region was selected to attenuate the lowest blade-passing-frequency (28E at approach); the long aft duct treatments, including treatment on the inner and outer walls and on both sides of the single splitter, were tuned for the center of the target, about 3200 Hz (Figure 63). On the basis of empirical data, including curves of tuning versus backing depth and PNL reduction versus treatment-length to duct-height ratio, this single splitter configuration was found to be superior to the no-splitter and two-splitter designs. By selection of deeper backing depths for the duct wall treatment and more shallow depths for the splitter, a relatively thin, 0.016 m = (0.62 in.) splitter was possible and a minimum blockage achievable. At the same time, the attenuation spectrum, compared to a spectrum for the splitter and wall treatment tuned to the same frequency, could be broadened to cover the attenuation target. The facing sheet values shown in Figure 65 were chosen for an optimum combination of bandwidth and peak attenuation rather than for peak attenuation alone.

Preliminary estimates of required treatment area were made by reference to guideline curves of PNdB reduction as a function of treatment-length to passage-height ratio ( $L/H$ ) such as shown in Figure 66. This figure contains data from various tests, including several NASA funded programs, for fan ducts with  $L/H$  ratios up to 23. It has been observed in axial traverse tests at P&WA that the flattening of these curves at higher values of  $L/H$  is not due to a failure of long treatments to attenuate fan noise but rather to the limiting effect of flanking path noise and the presence of other noise sources, such as jet noise, on the overall observed attenuation spectrum. For the current program, NASA Quiet Two-Stage Fan Rig, an axial length of about 1.016 m (40 in.) available for treatment and a passage height of 0.178 m (7 in.) would result in  $L/H$  ratios of about 5.8 with no splitter, 12 with one splitter, and 20 with two splitters. The cross-sectional blockage of the splitters reduces the passage height, and this has been taken into account. The single-splitter configuration was taken as a starting point for the design on the basis of Figure 66 and various other considerations discussed above.

Tuning curves, such as shown in Figure 67, that relate treatment backing depth to frequency of peak attenuation were used for initial selection of backing depths. Generally, the initial value of facing sheet installed-resistance is taken to be equal to the value of the dimensionless frequency parameter in Figure 67 at the design point. A succession of iterations was then performed in which attenuation spectra were calculated by means of an analytical solution of the wave equation for the principal mode in the duct [ref. 9] for incremented values of backing depths and facing sheet resistances until an optimum coverage of the attenuation target was found.

## PREDICTED ATTENUATIONS – INTERSTAGE AND AFT TREATMENT

On the basis of the procedures previously described, the attenuations shown in Figure 68 were obtained. PNL numbers for takeoff and approach at 45.7 m (150 ft) radius and maximum PNL are summarized in Table XIII.

TABLE XIII  
ANALYTICALLY PREDICTED FAN AFT PNL AT 45.7 METER  
(150 FOOT) RADIUS

CONDITION	DESIGN SPEED	PNL UNTREATED	PNL TREATED	PNL ATTENUATION
Approach	70%	112.3 dB	92.6 dB	19.7 dB
Takeoff	94%	125.0 dB	104.2 dB	20.8 dB

The results of the analytical design system indicate a reduction of approximately 20 PNdB in aft noise.

## COMPETING NOISE SOURCES

In tests it is often difficult to realize large predicted values of duct attenuation. Fan jet mixing noise and additional noise generated by the rig fan air scrubbing the test rig afterbody tend to obscure measurements of treated fan noise levels in the farfield. However, empirical estimates of jet mixing noise have determined that at low speeds (e.g., approach) the majority of fan noise attenuation should be measureable at the farfield microphones (Figure 69). Use of narrow band spectral analysis, which increases the ratio of tone to broadband noise, will facilitate detection of fan noise attenuation. Further signal detection will be provided by operating at the widest possible nozzle condition, which reduces the jet nozzle velocity and consequently the jet noise. At higher speeds, the high levels of jet noise will at least partially mask the effect of the treatment (Figure 70).

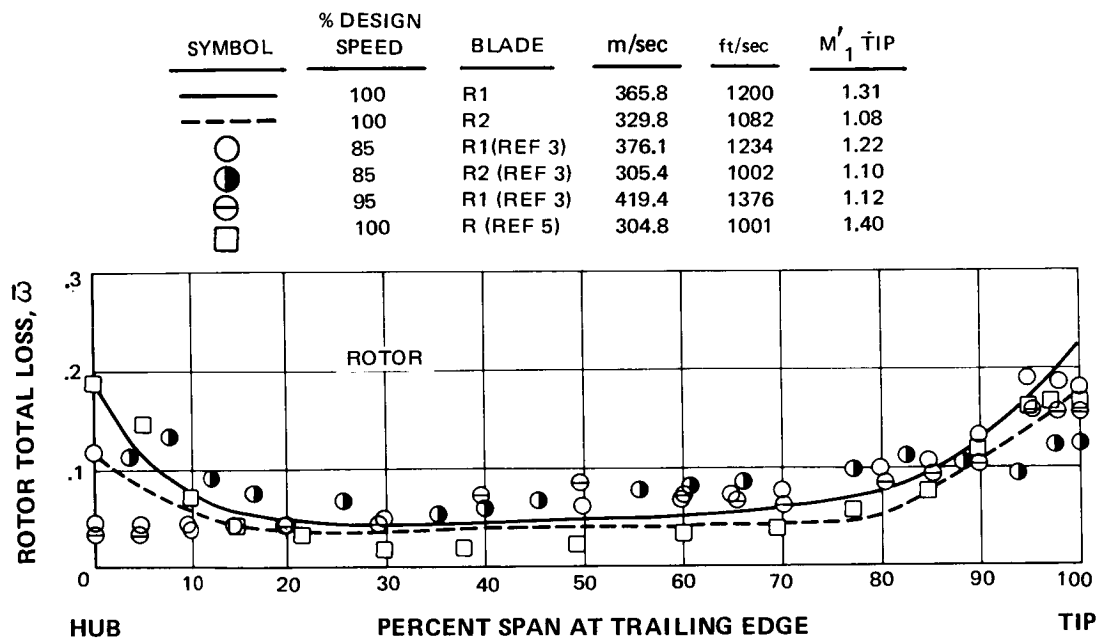
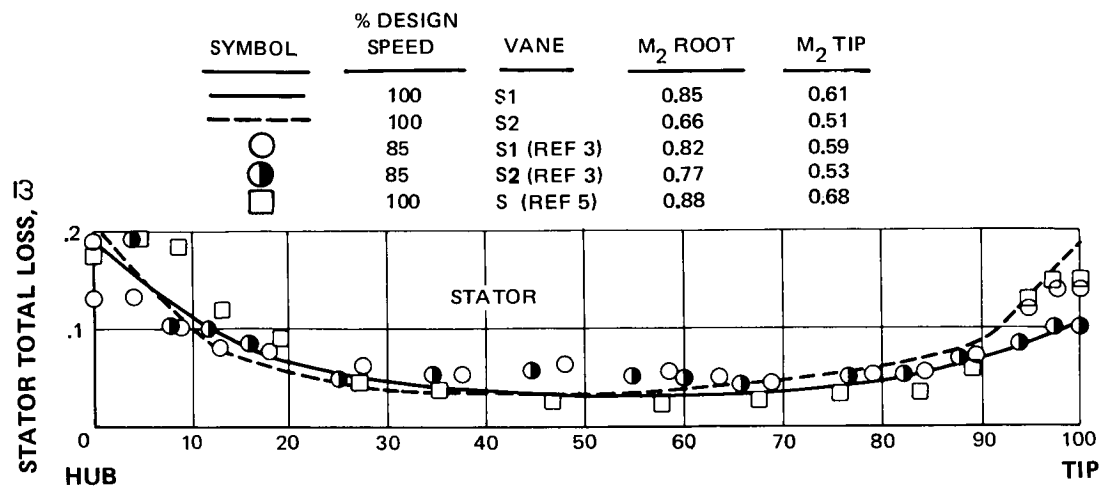


Figure 1 Rotor (lower) and Stator (upper) Total Loss Spanwise Profiles

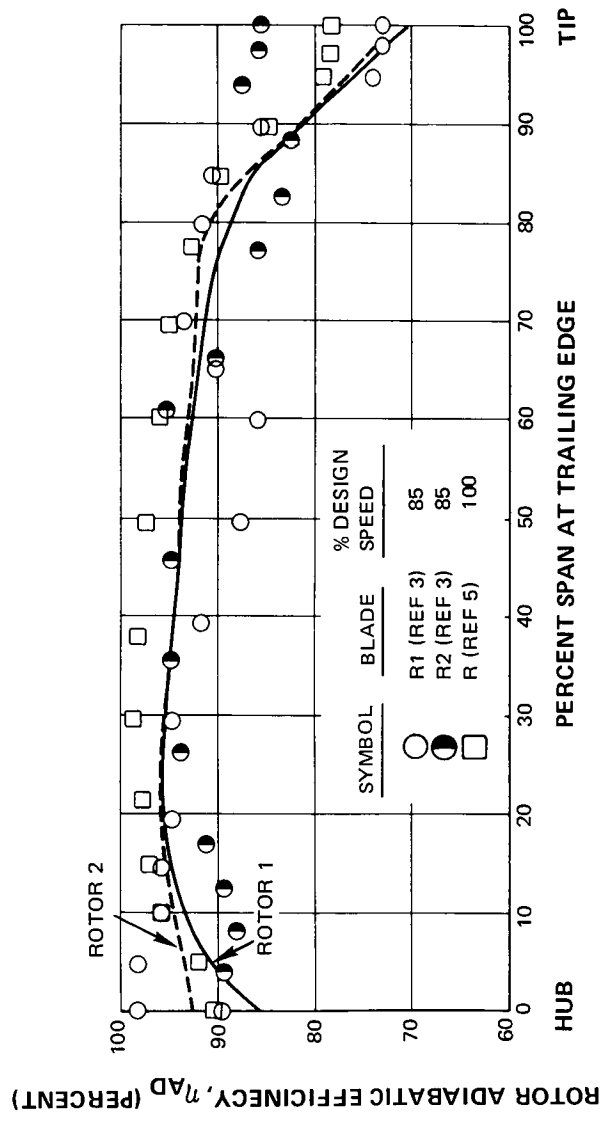


Figure 2 Rotor Adiabatic Efficiency Spanwise Profiles

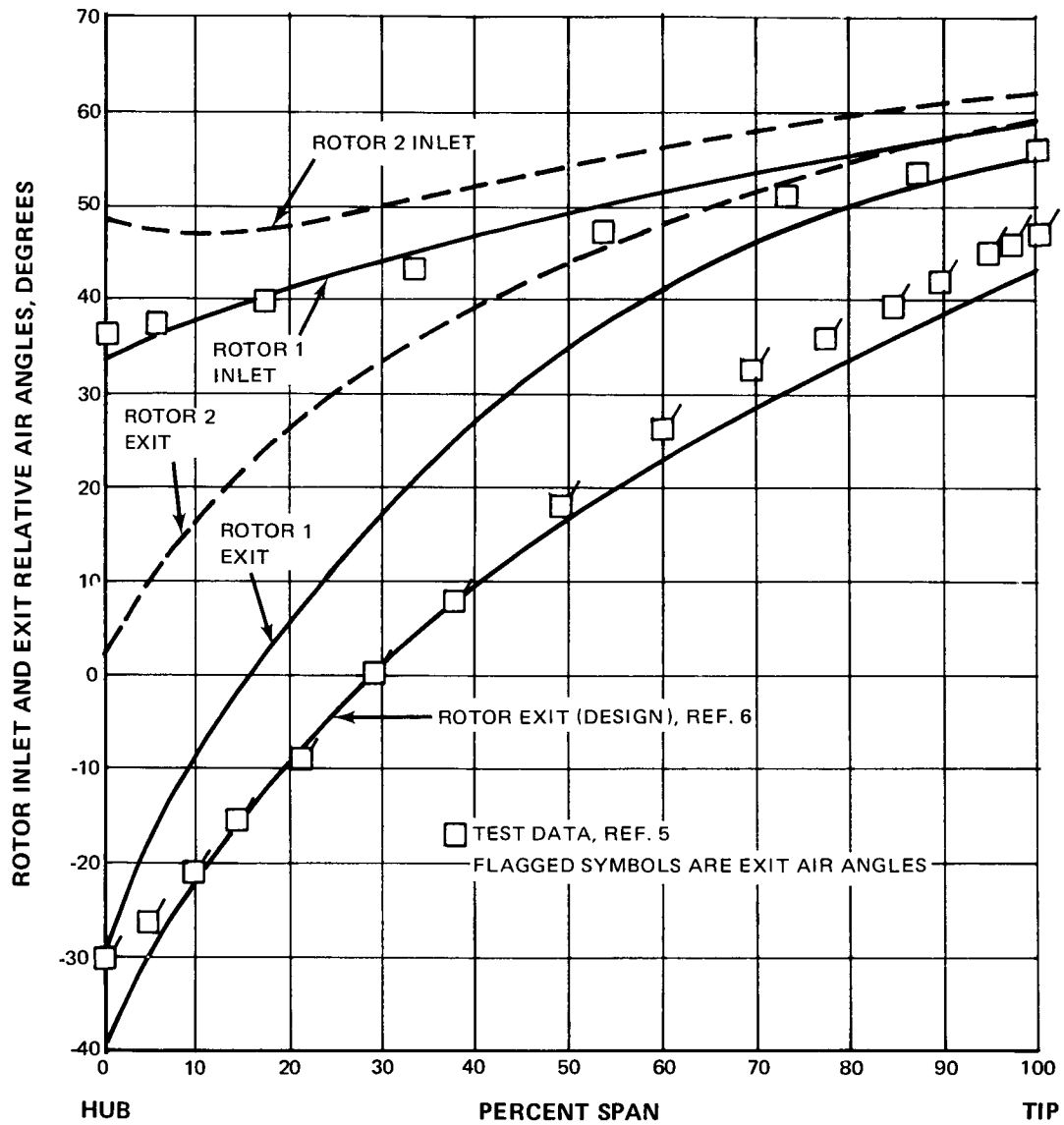


Figure 3 Rotor Inlet and Exit Relative Air Angles Spanwise Profiles

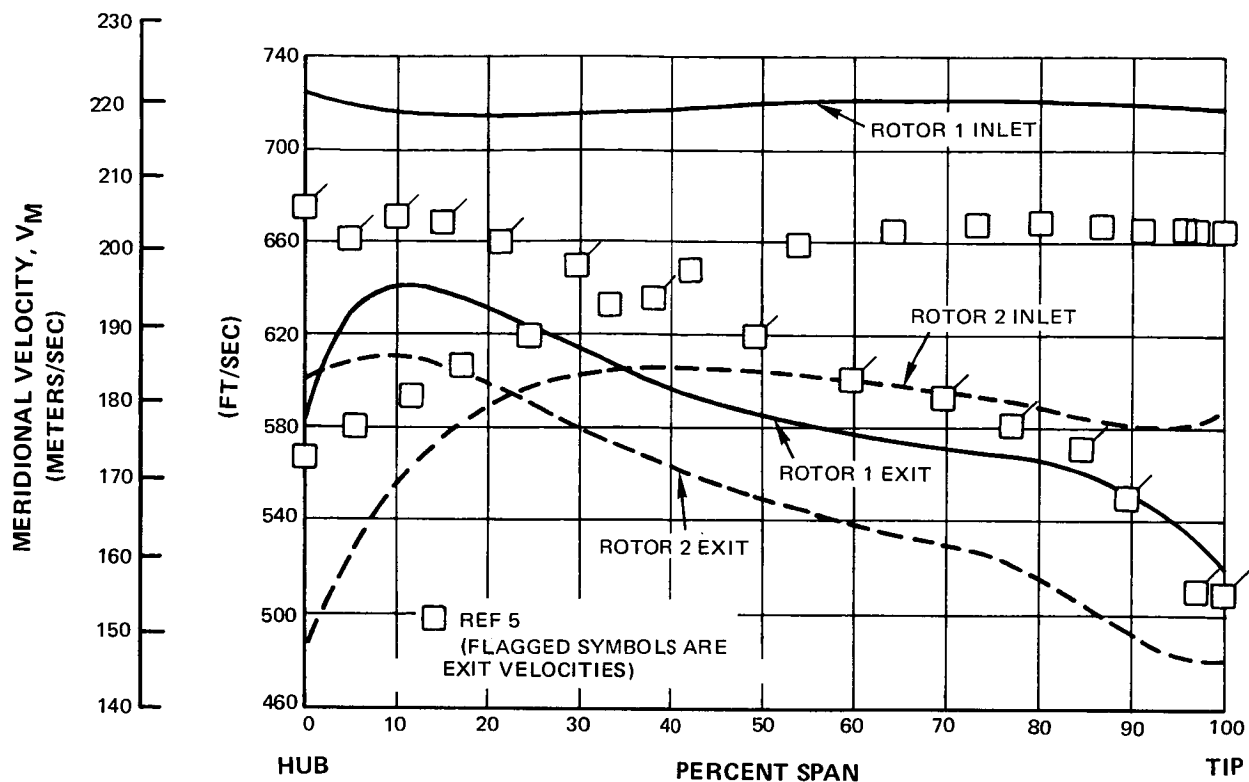


Figure 4 Rotor Meridional Velocity Spanwise Profiles

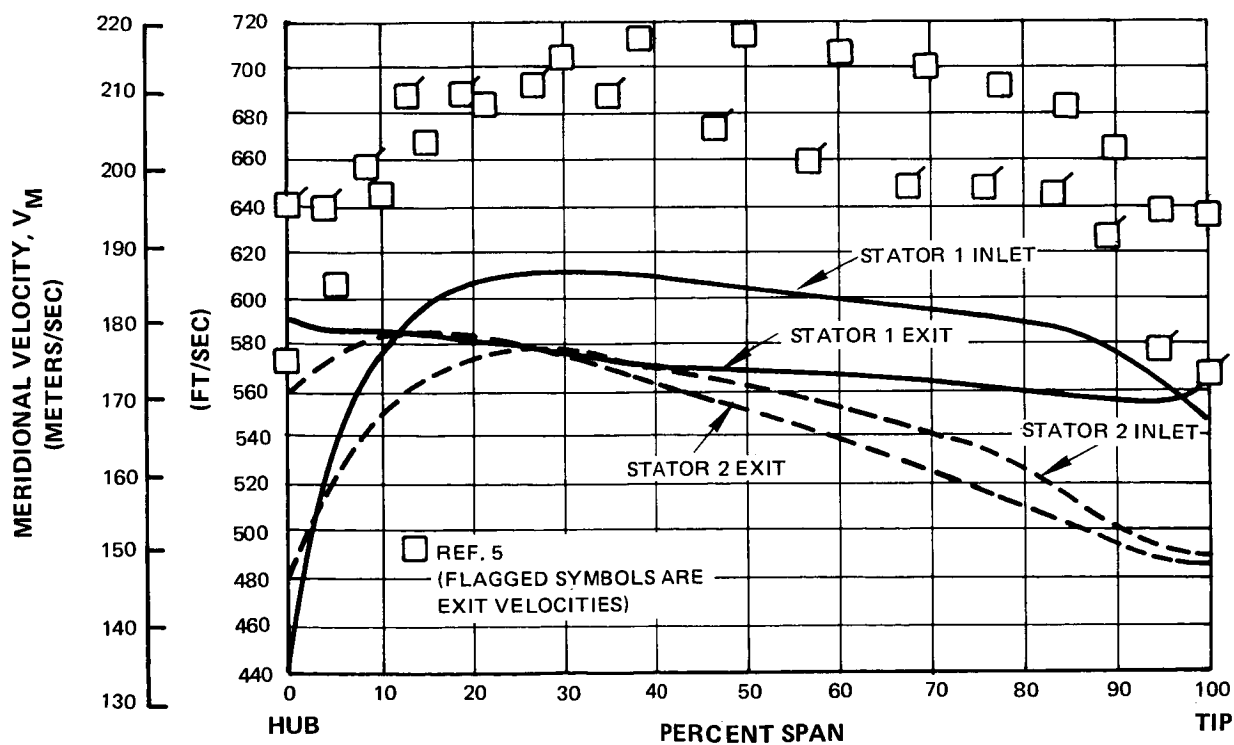


Figure 5 Stator Meridional Velocity Spanwise Profiles

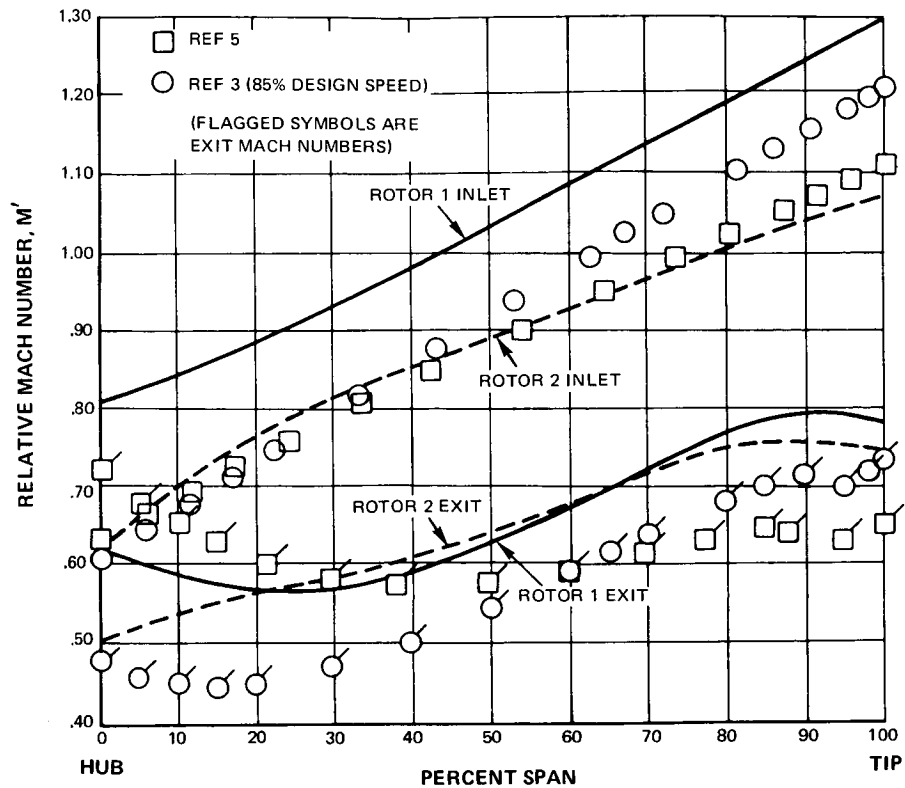


Figure 6 Inlet and Exit Mach Number Spanwise Profiles for Rotors

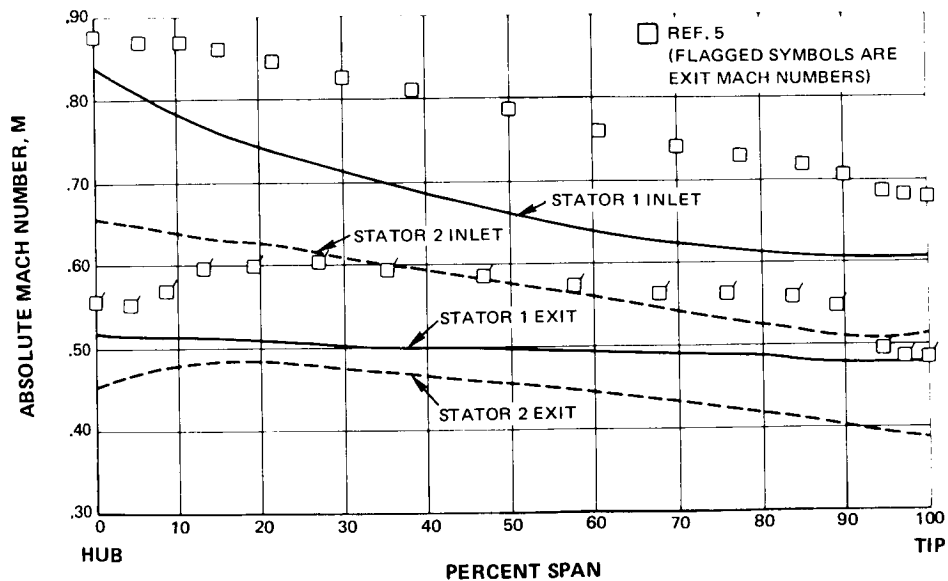


Figure 7 Inlet and Exit Mach Number Spanwise Profiles for Stators

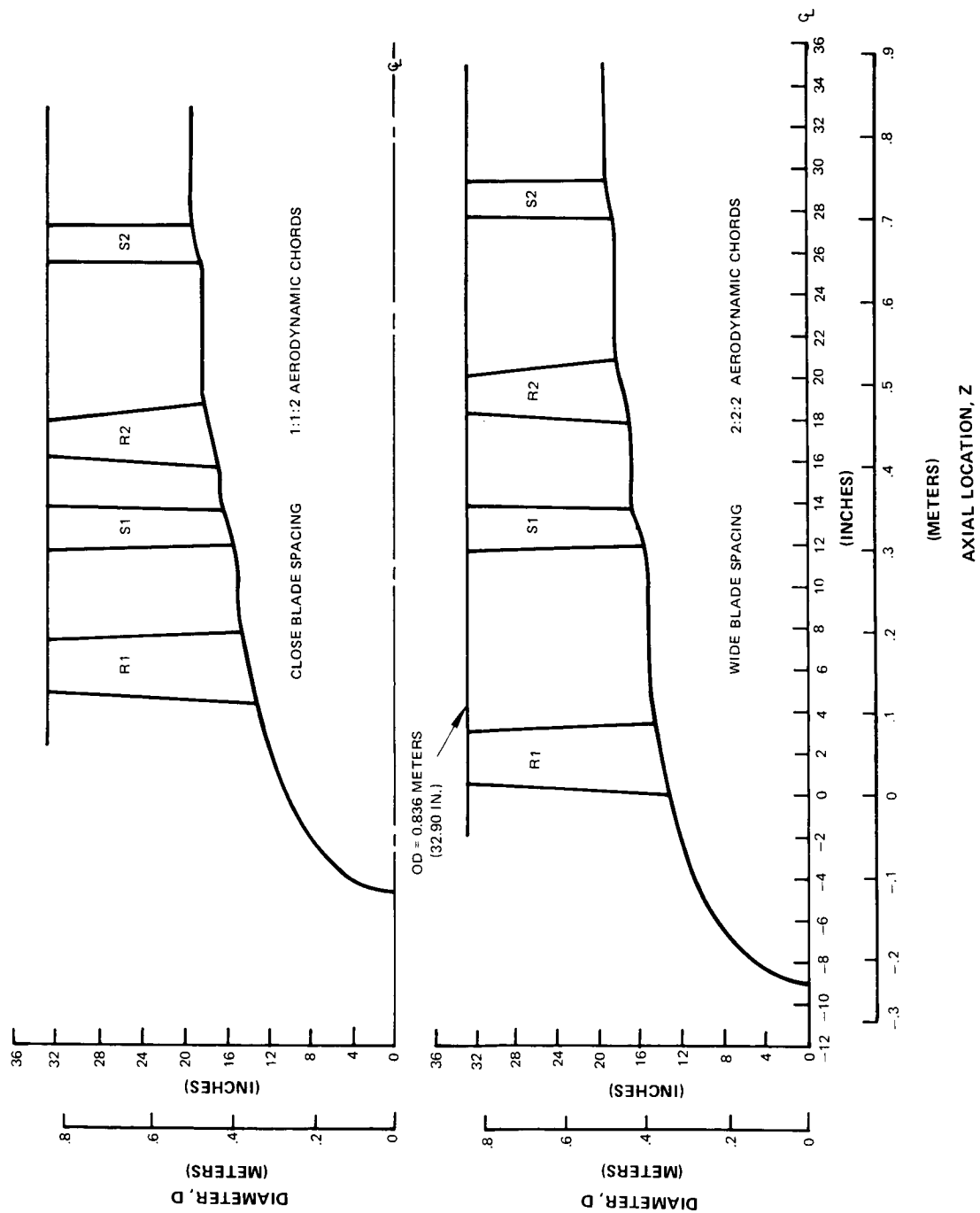


Figure 8 Fan Flowpaths

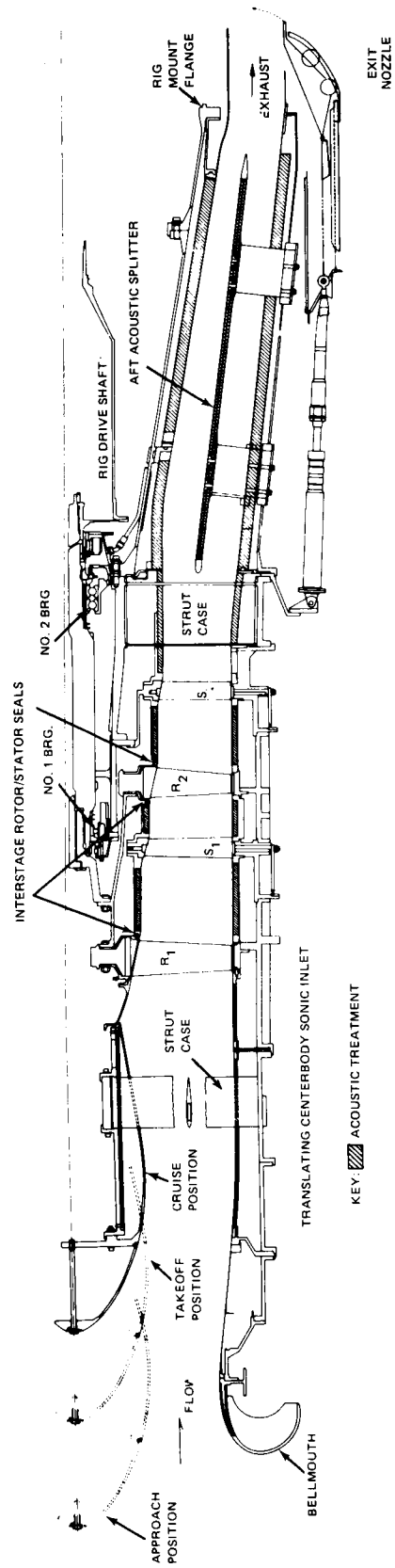


Figure 9 Schematic of the Quiet Two Stage Fan

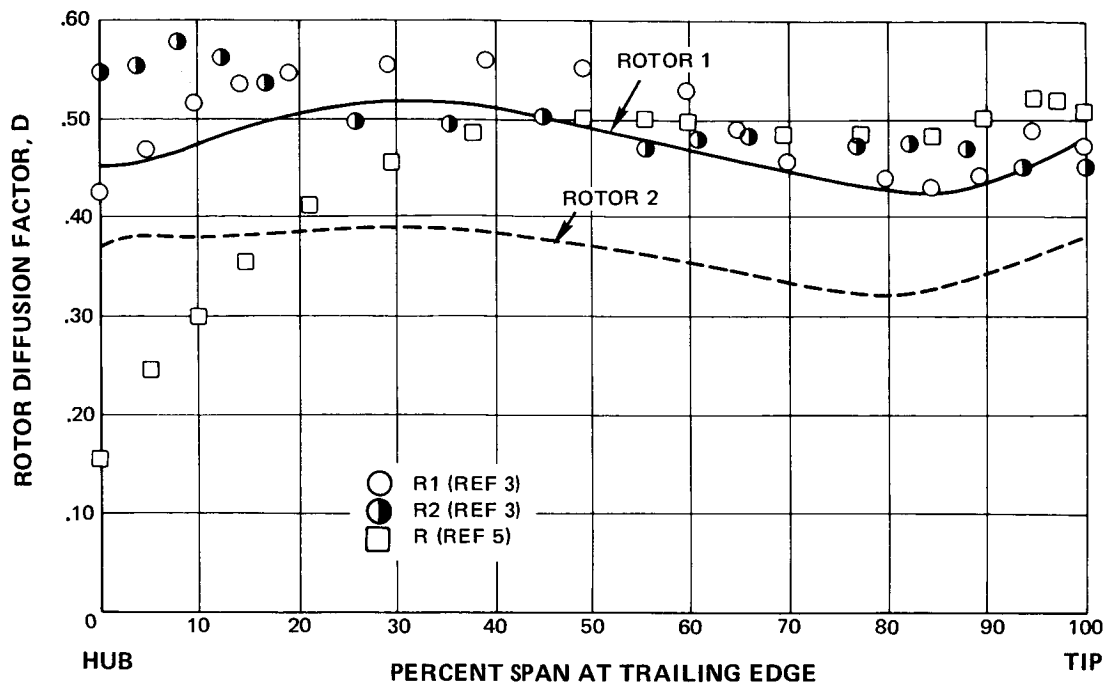


Figure 10 Rotor Diffusion Factor Spanwise Profiles

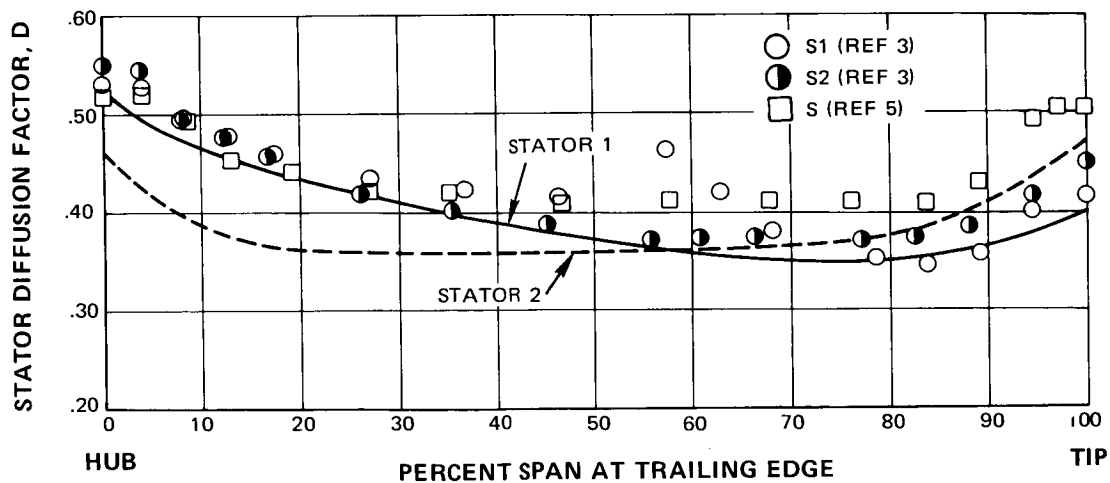


Figure 11 Stator Diffusion Factor Spanwise Profiles

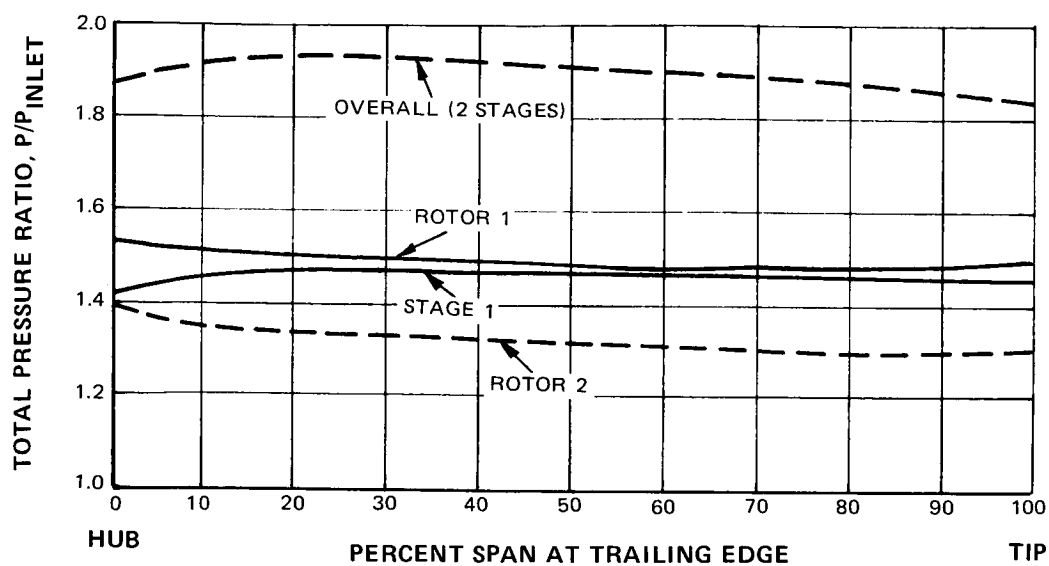


Figure 12 Total Pressure Ratio Spanwise Profiles

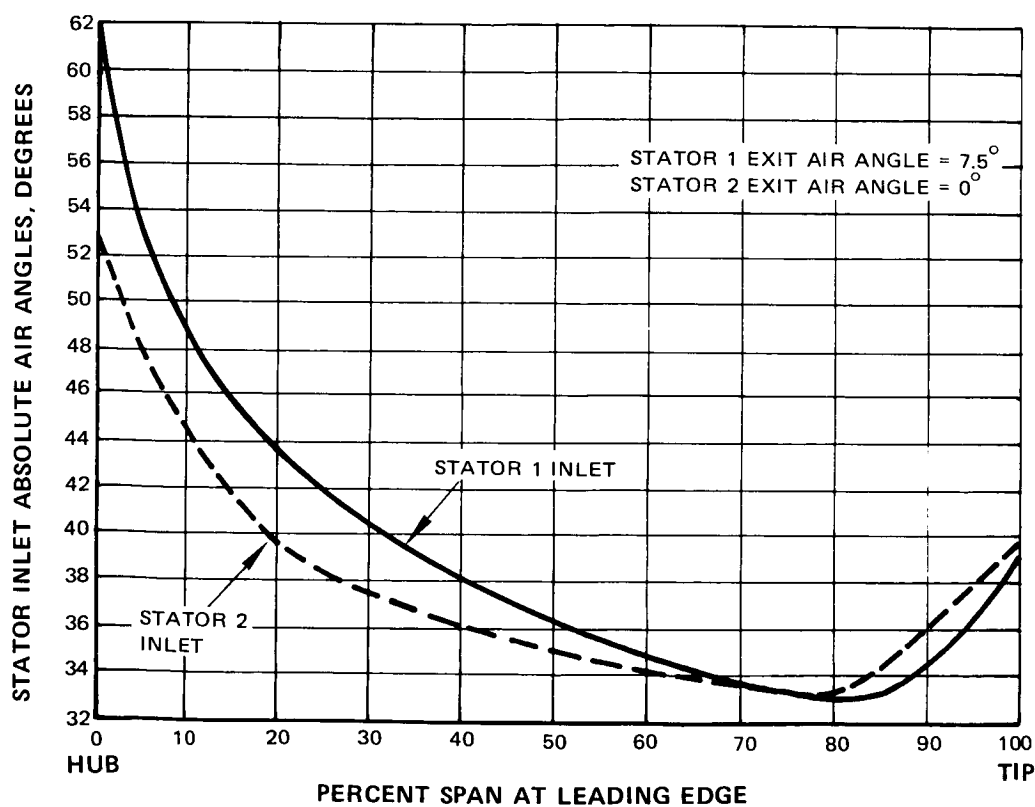


Figure 13 Stator Inlet and Exit Absolute Air Angle Spanwise Profiles

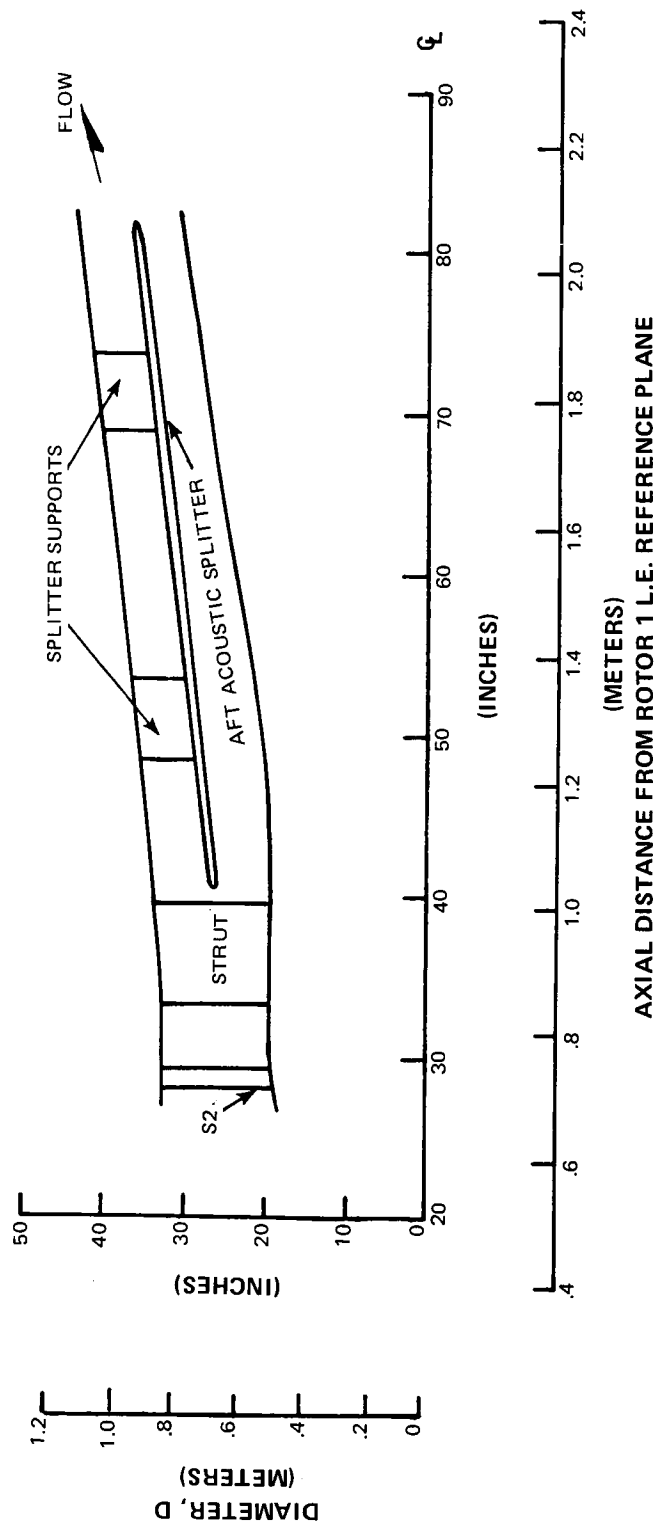


Figure 14 Fan Exit Duct and Acoustic Splitter Flowpath

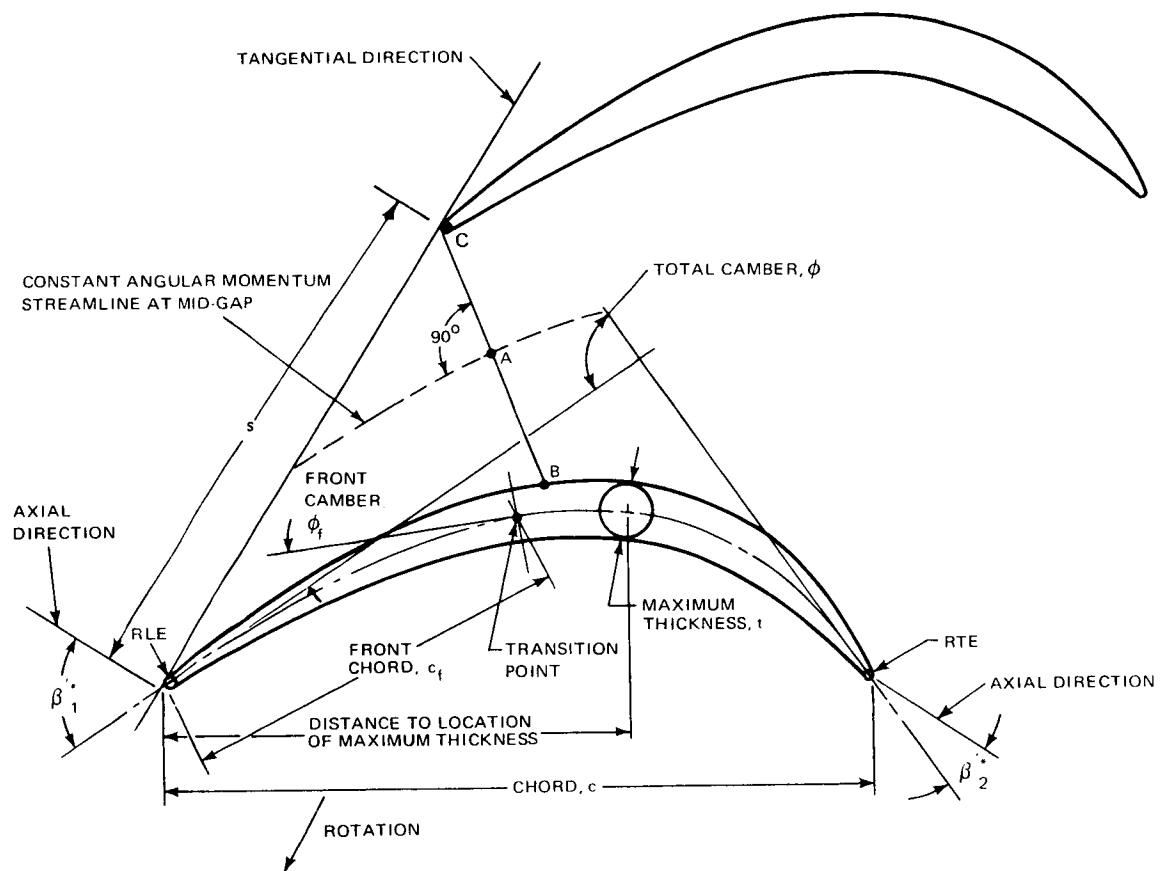


Figure 15 Multiple-Circular-Arc Airfoil Definitions

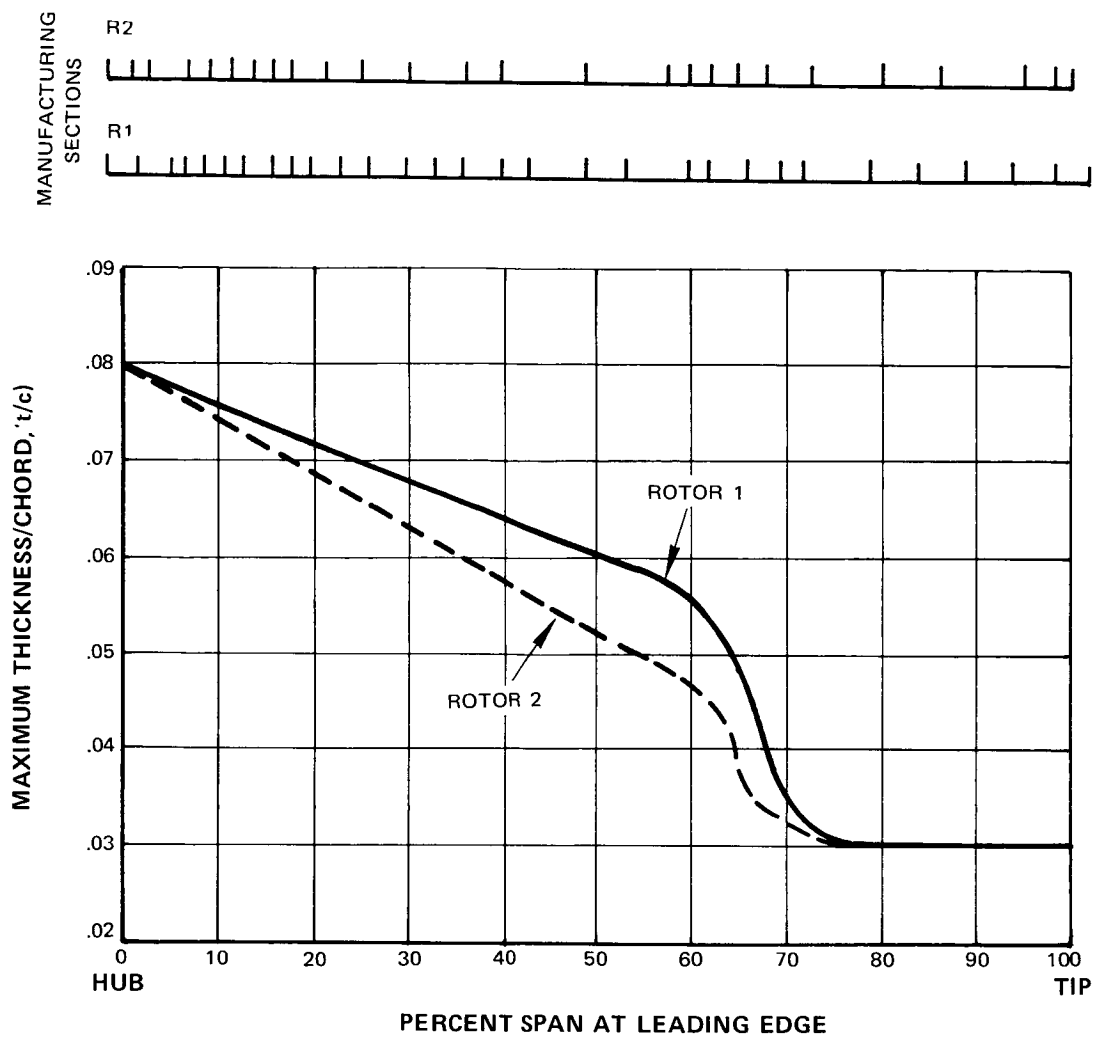


Figure 16 Rotor Airfoil Thickness Spanwise Profiles

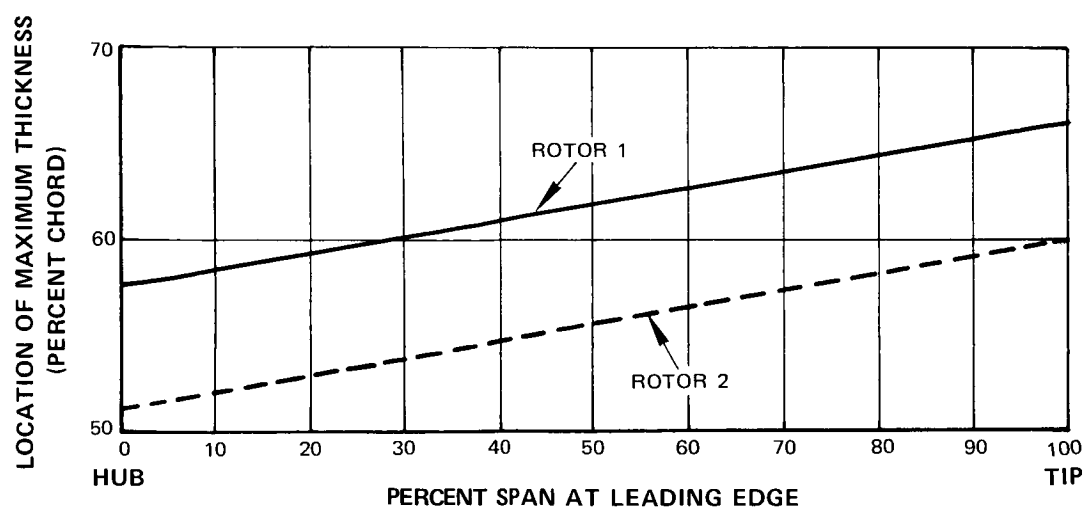


Figure 17 Rotor Chordwise Location of Airfoil Maximum Thickness Spanwise Profiles

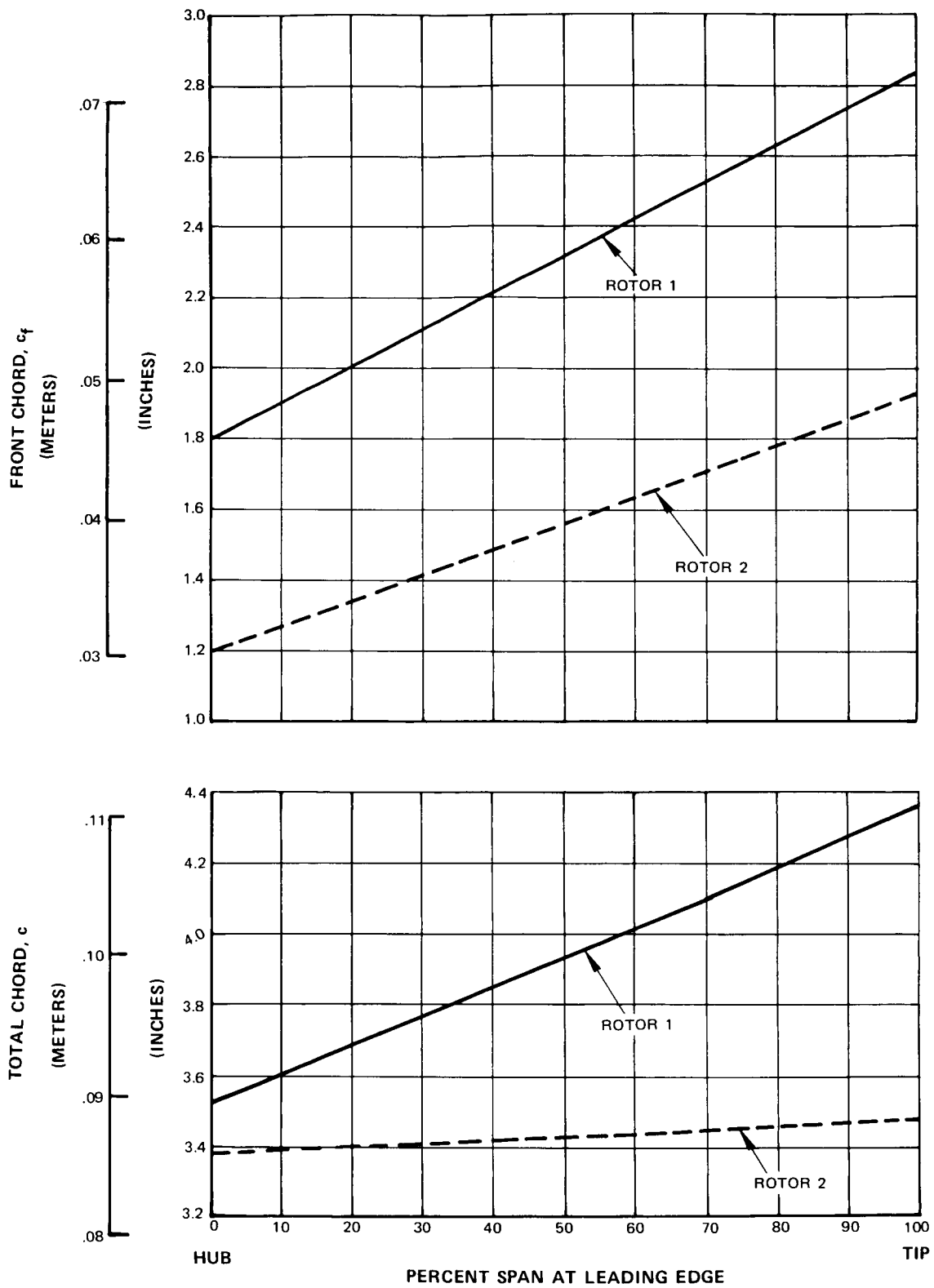


Figure 18 Rotor Chord Spanwise Profiles

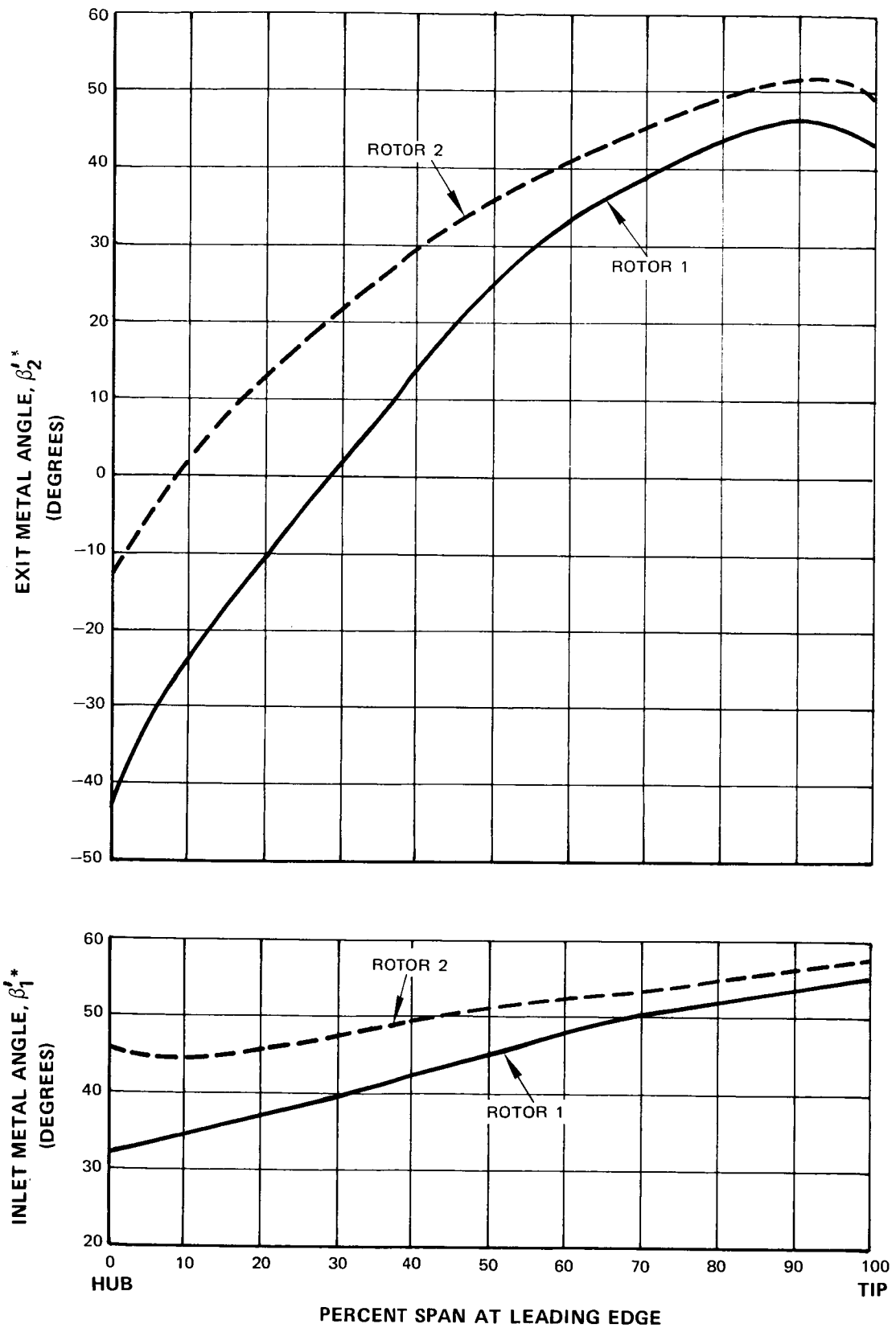


Figure 19 Rotor Inlet and Exit Metal Angle Spanwise Profiles

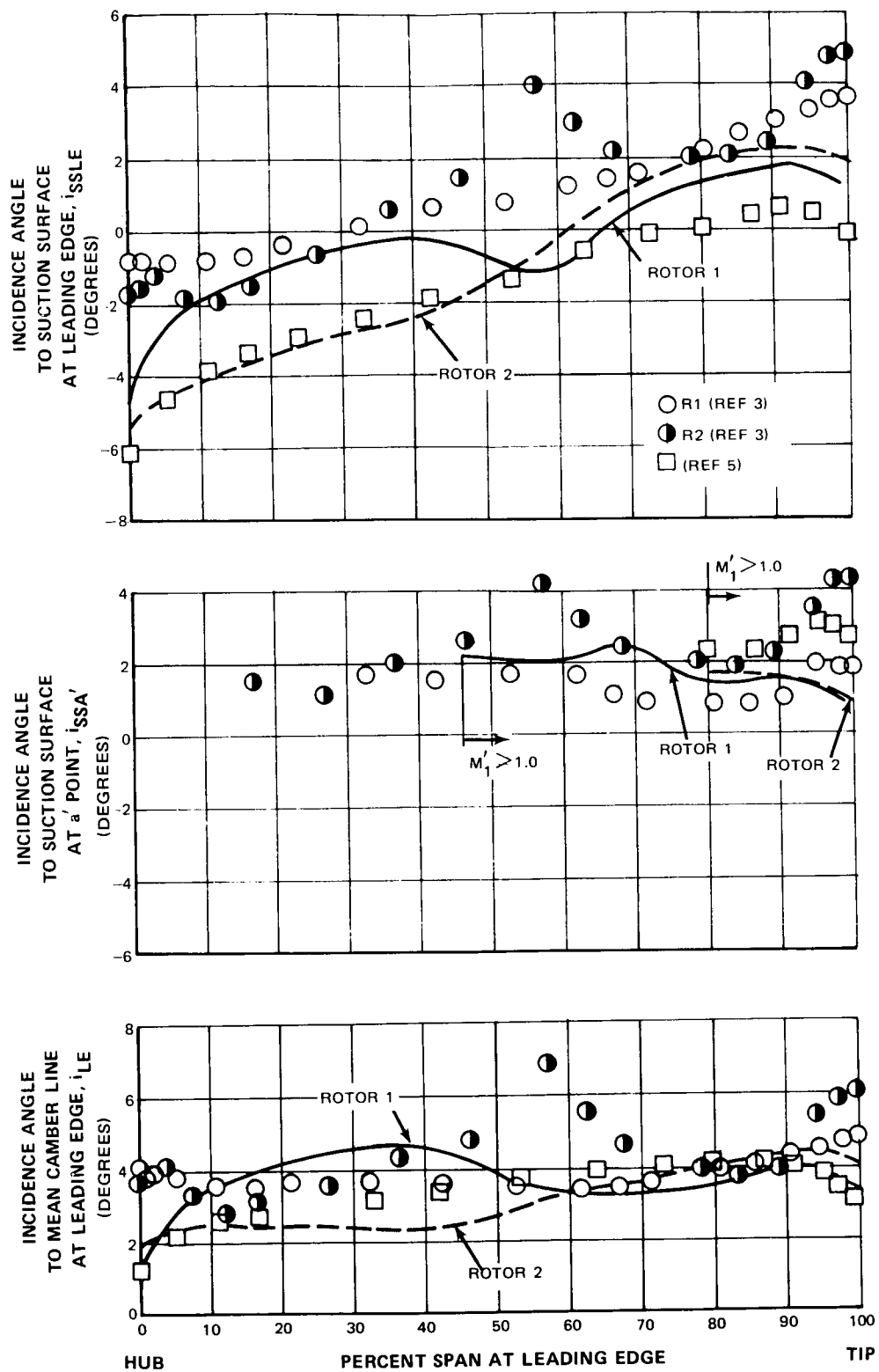


Figure 20 Rotor Incidence Angle Spanwise Profiles

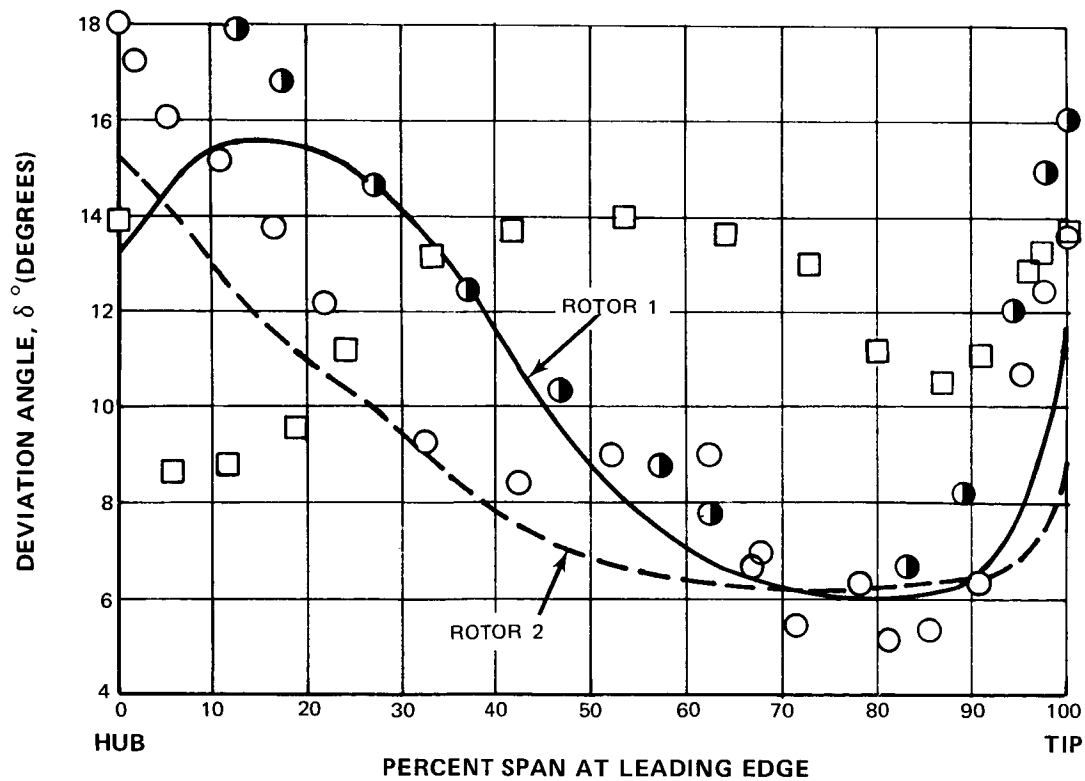
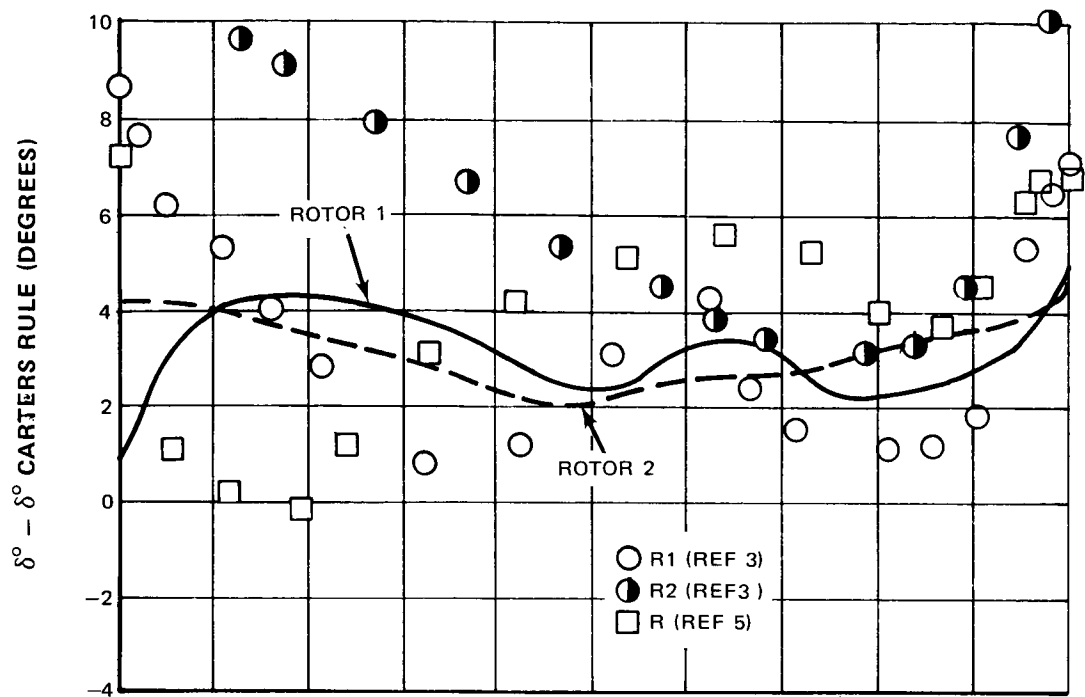


Figure 21 Rotor Deviation Angle Spanwise Profiles

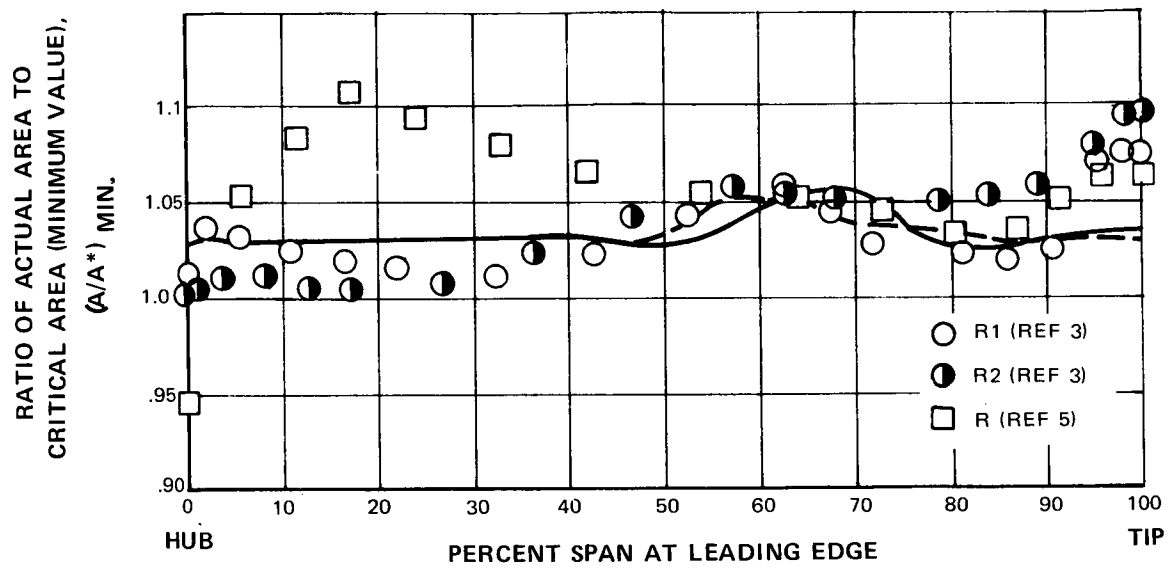


Figure 22 Minimum Rotor Channel Area Ratio Spanwise Profiles

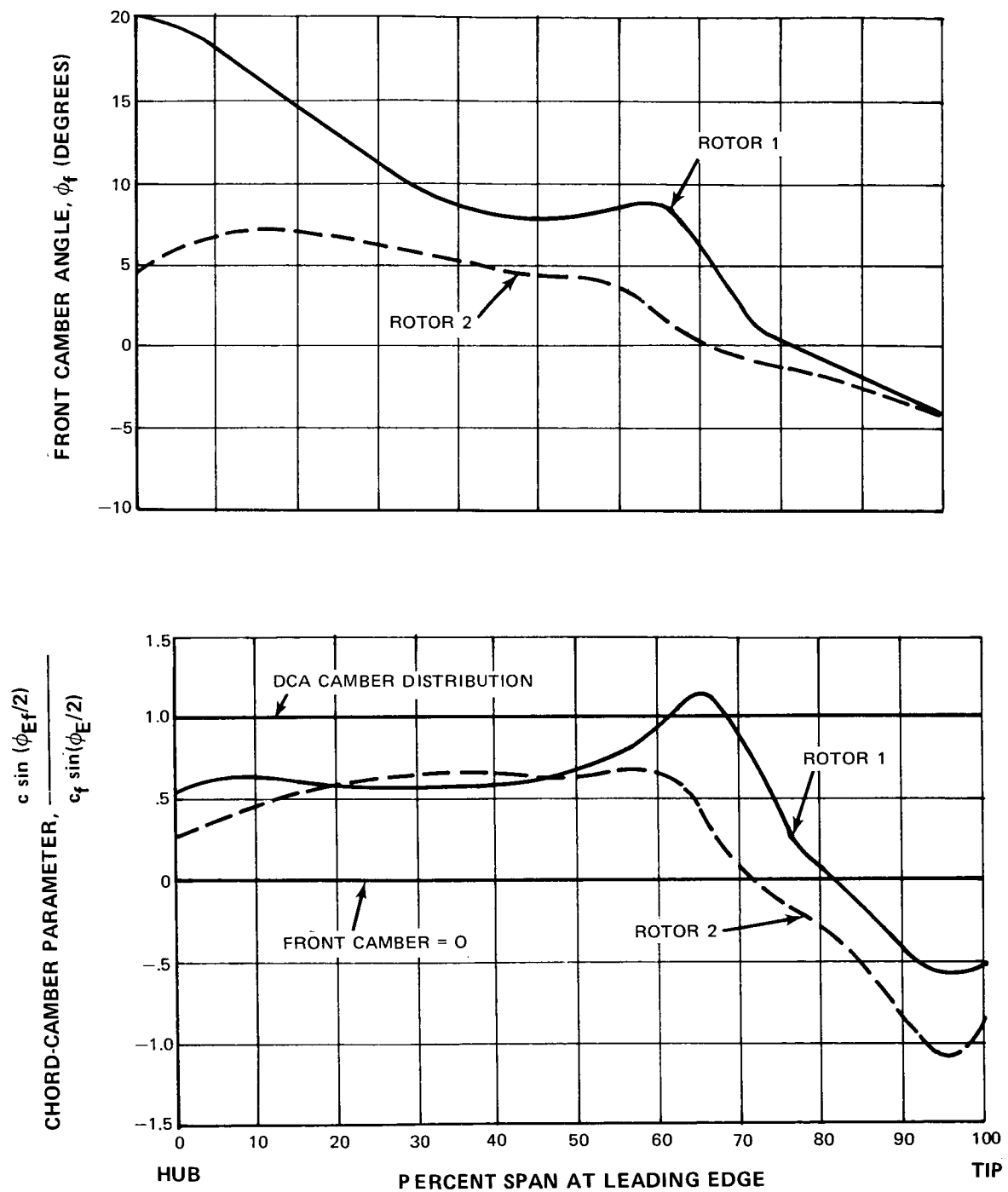


Figure 23 Rotor Front Camber Angle and Chord-Camber Parameter Spanwise Profiles

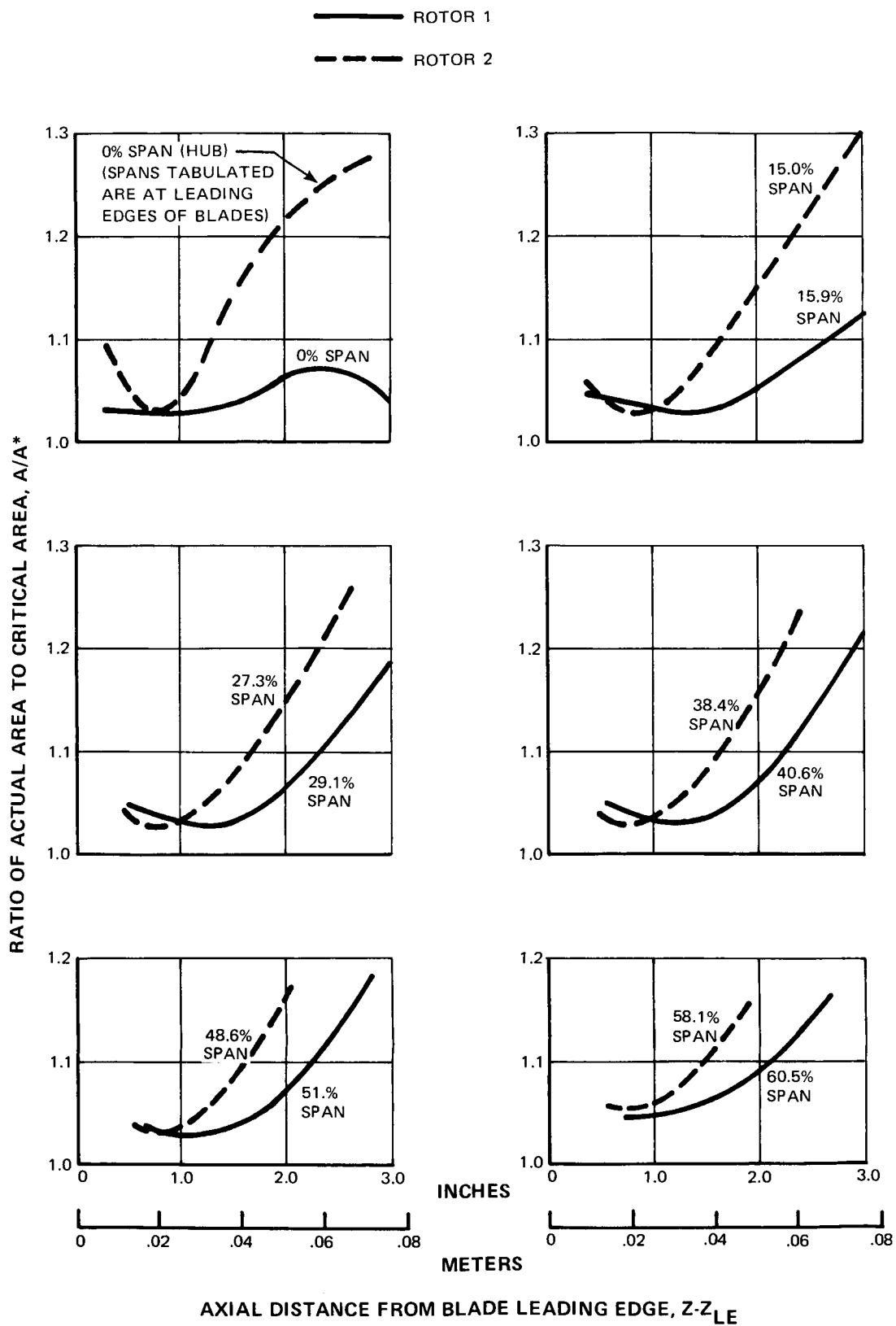


Figure 24 Rotor Channel Area Ratios Versus Axial Distance

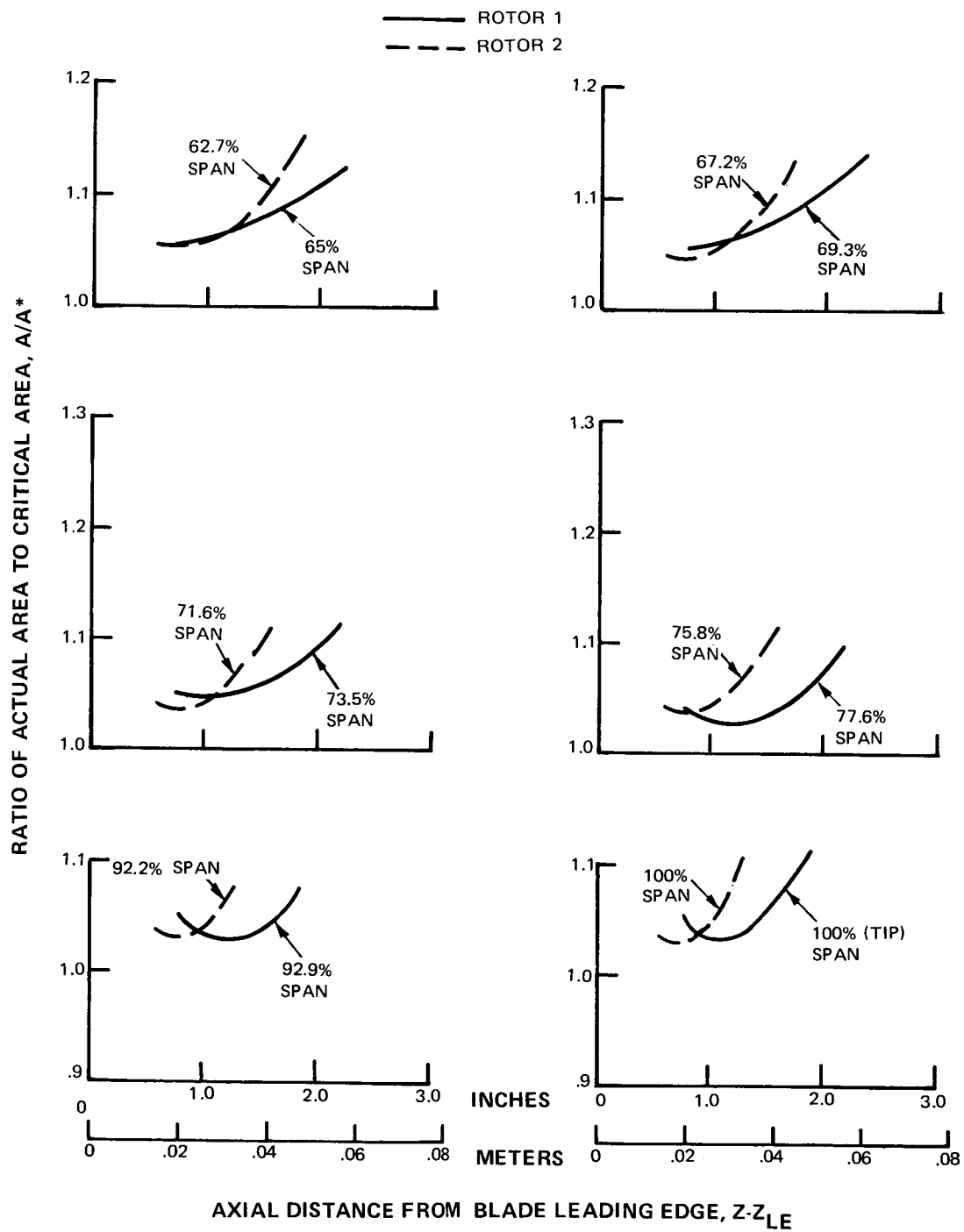


Figure 24 (Cont'd) Rotor Channel Area Ratios Versus Axial Distance

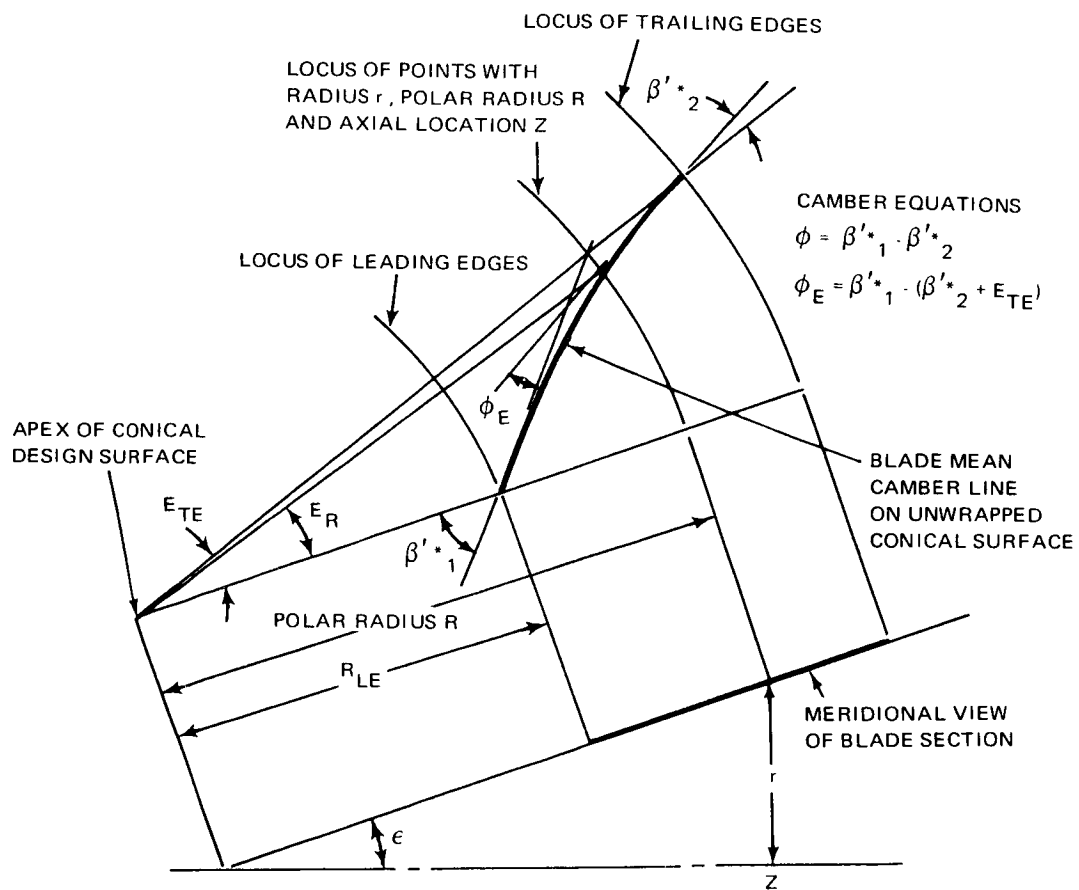


Figure 25 Meridional View and Polar Representation of Blade Mean-Camber-Line

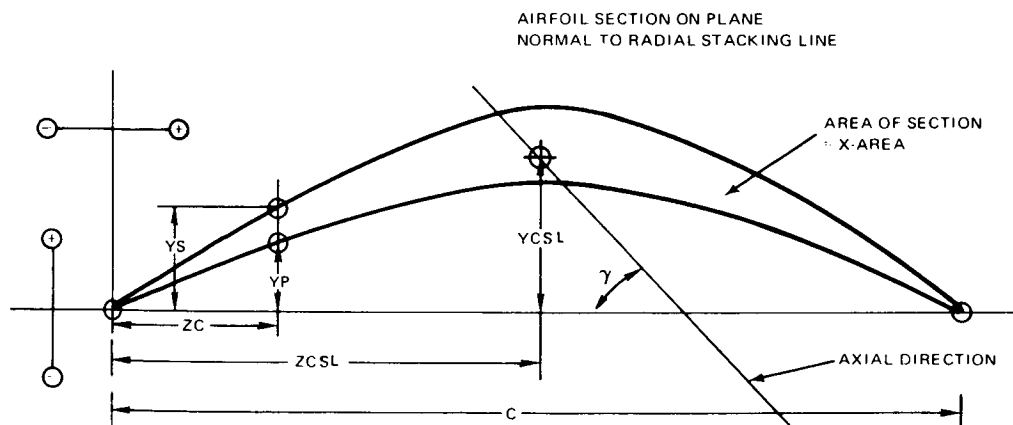


Figure 26 Airfoil Coordinate Definition for Manufacturing Sections

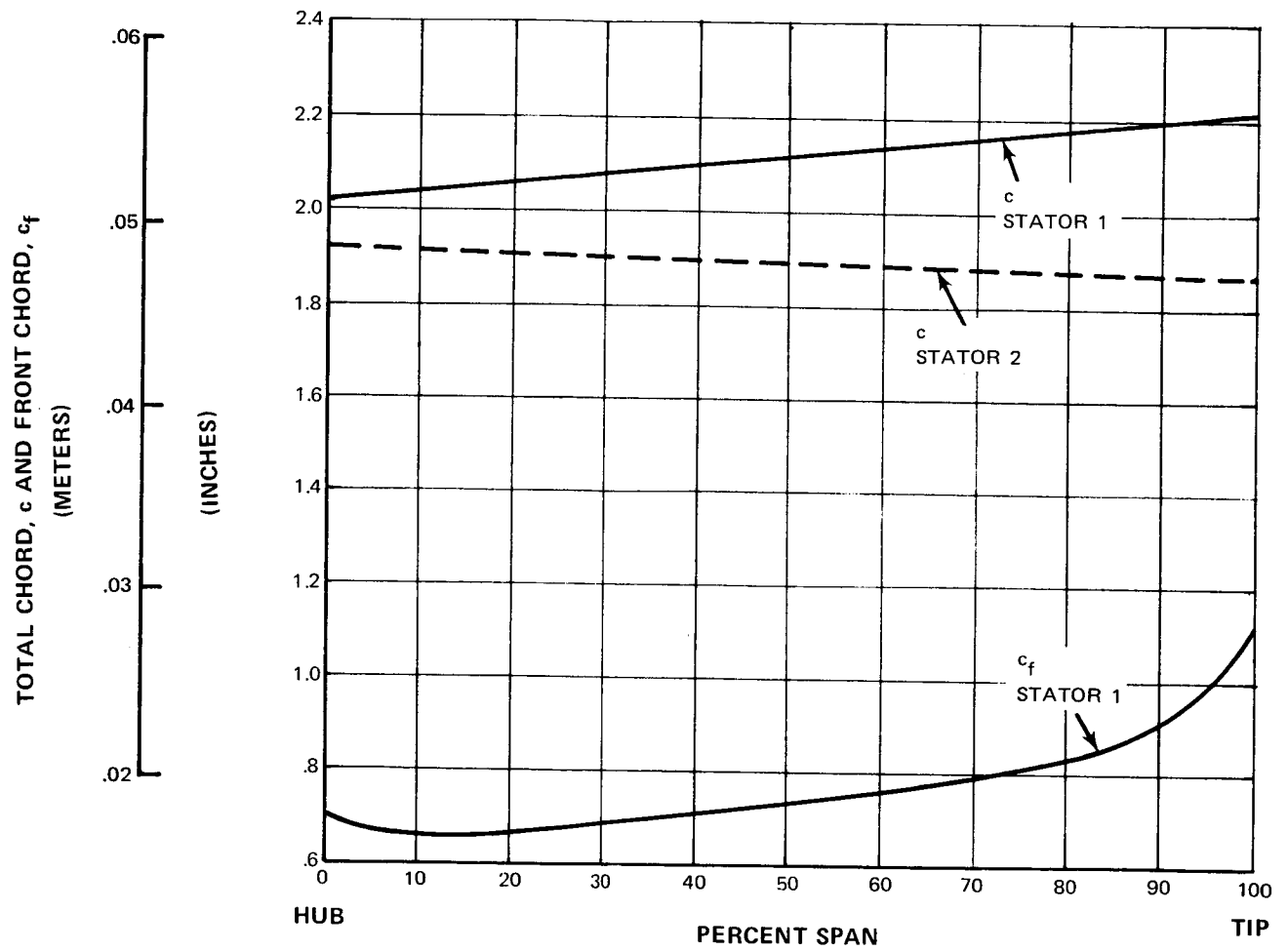


Figure 27 Stator Chord Spanwise Profiles

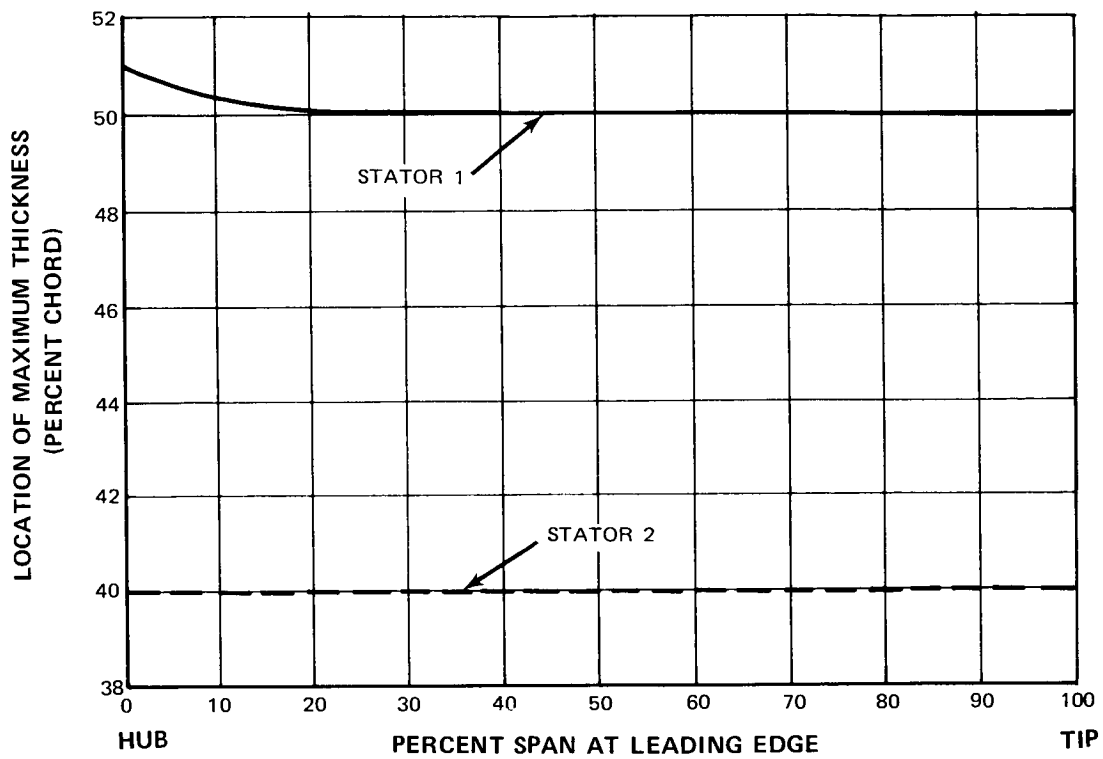


Figure 28 Stator Chordwise Location of Maximum Thickness Spanwise Profiles

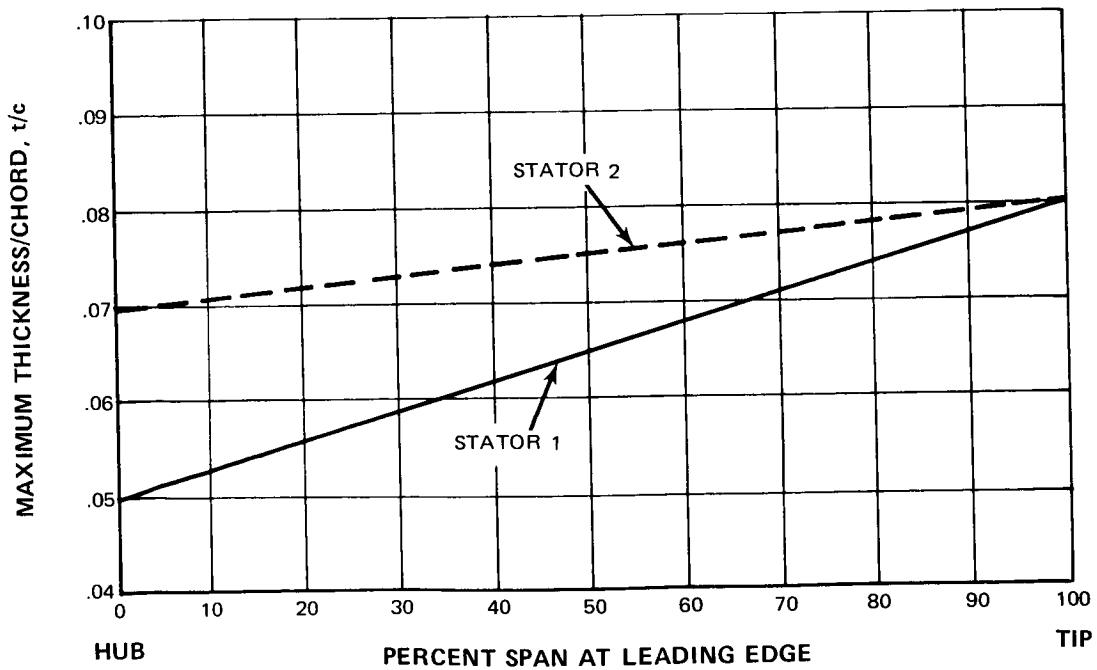


Figure 29 Stator Airfoil Thickness Spanwise Profiles

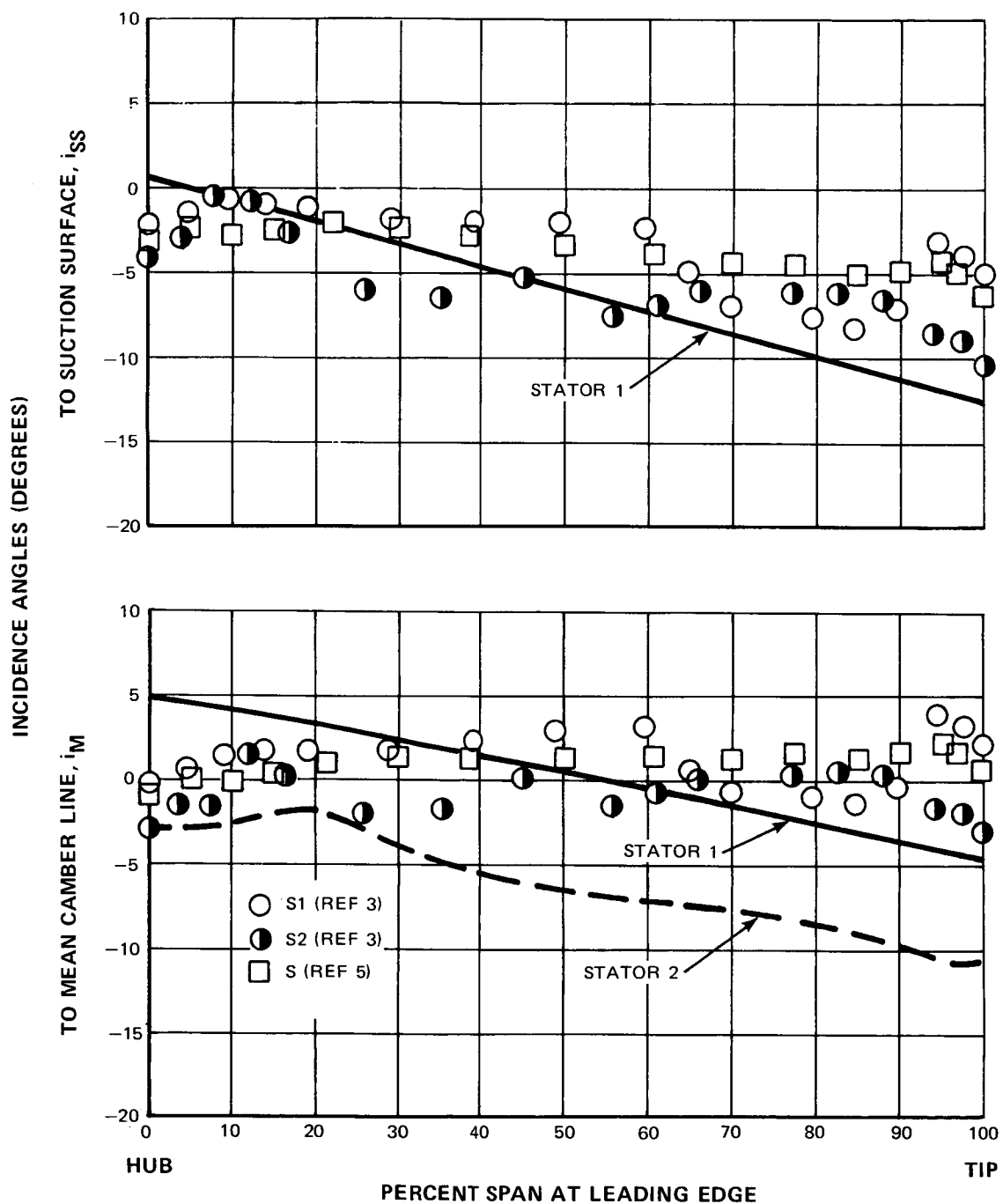


Figure 30 Stator Incidence Angle Spanwise Profiles

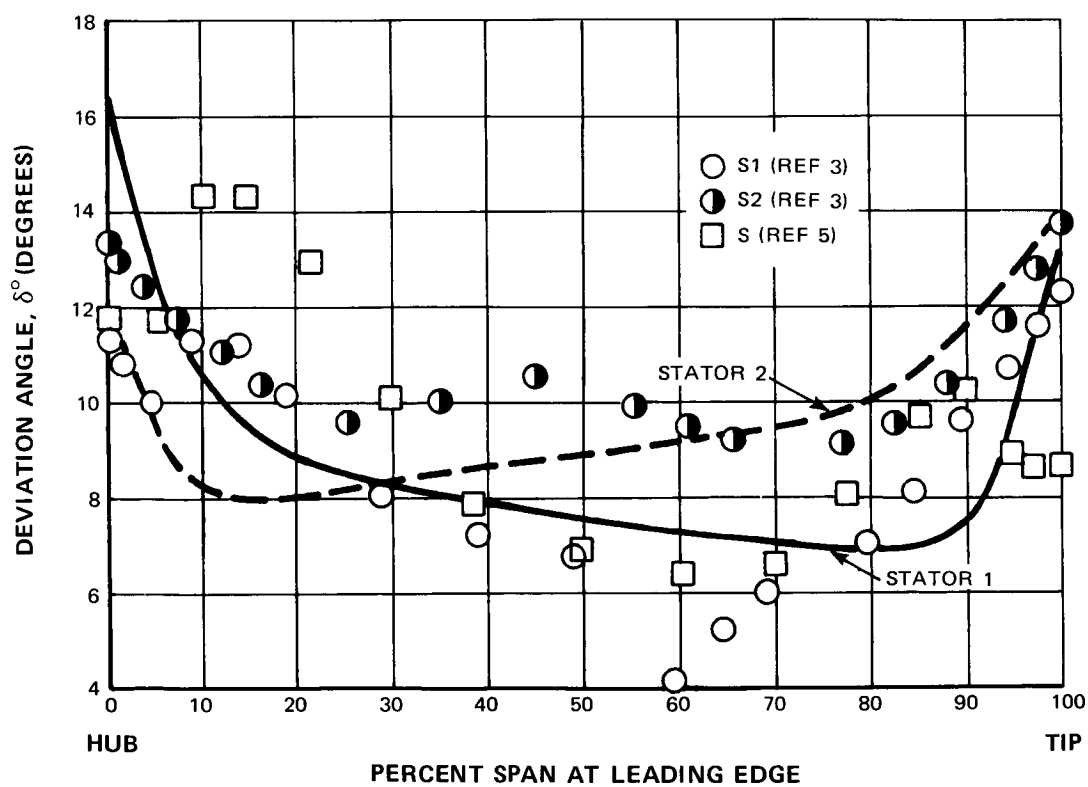
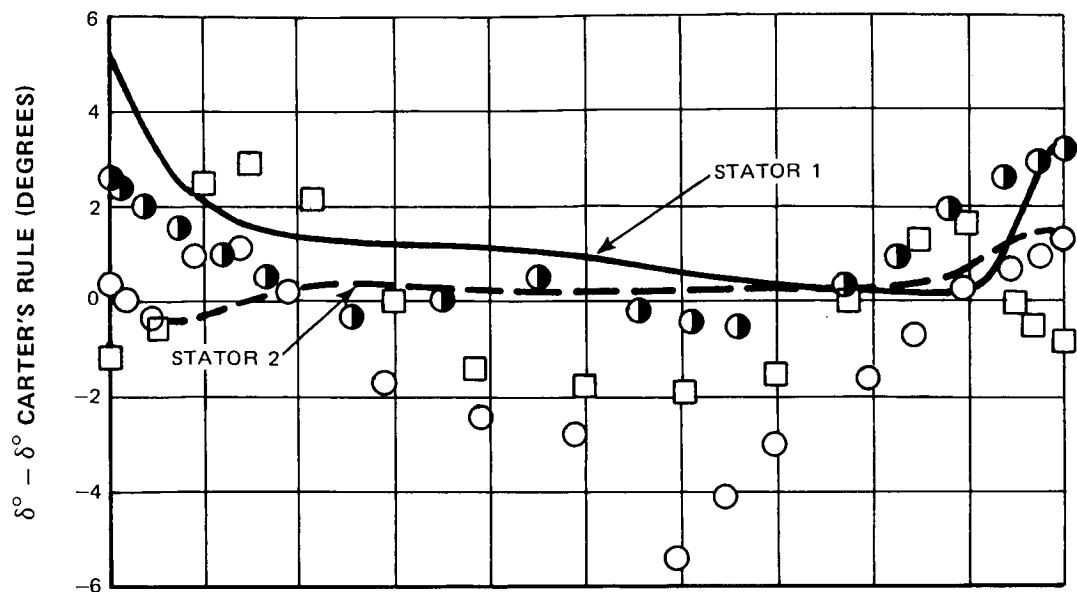


Figure 31 Stator Deviation Angle Spanwise Profiles

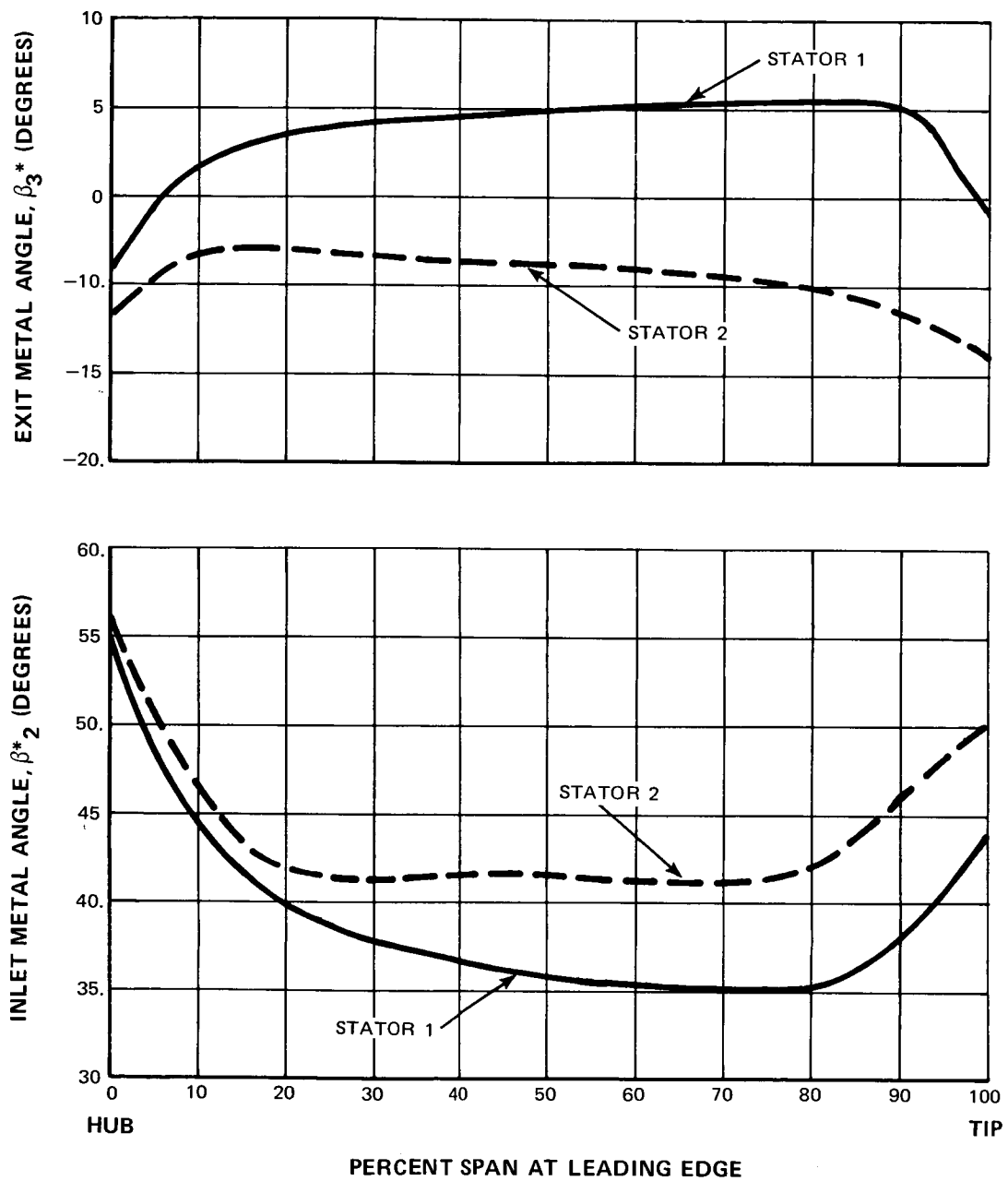


Figure 32 Stator Inlet and Exit Metal Angle Spanwise Profiles

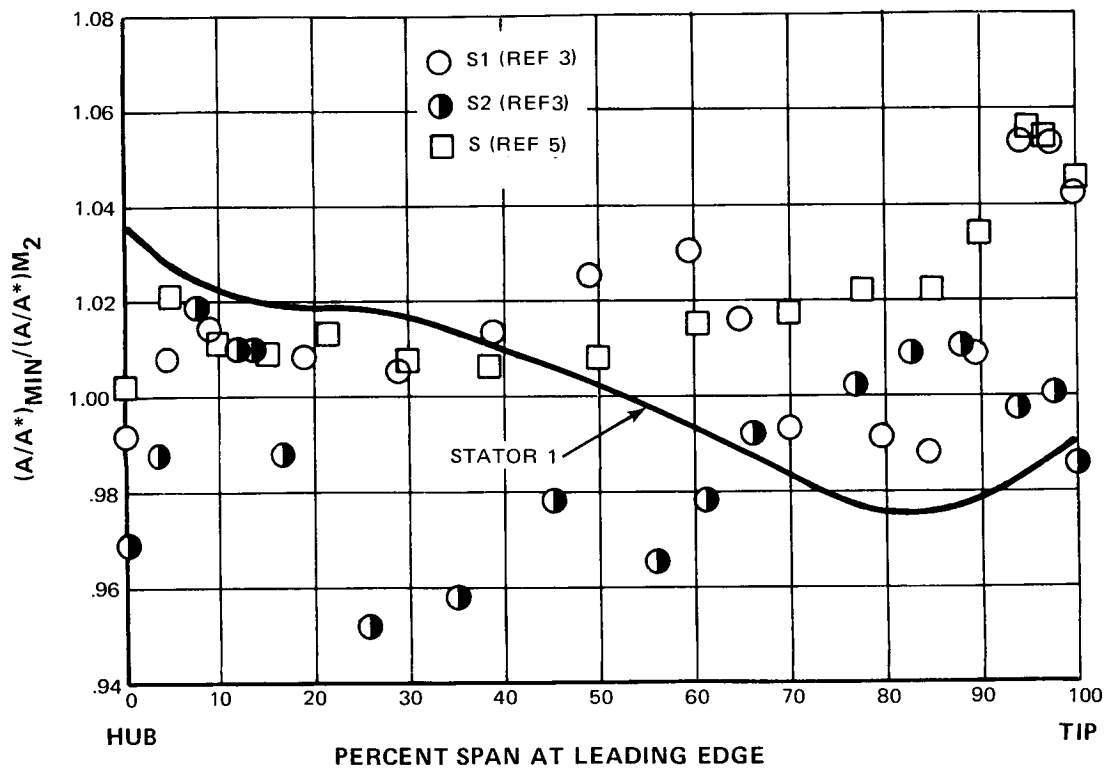


Figure 33 Ratios of Channel-Throat-Area to Captured-Area Versus Span for Stators

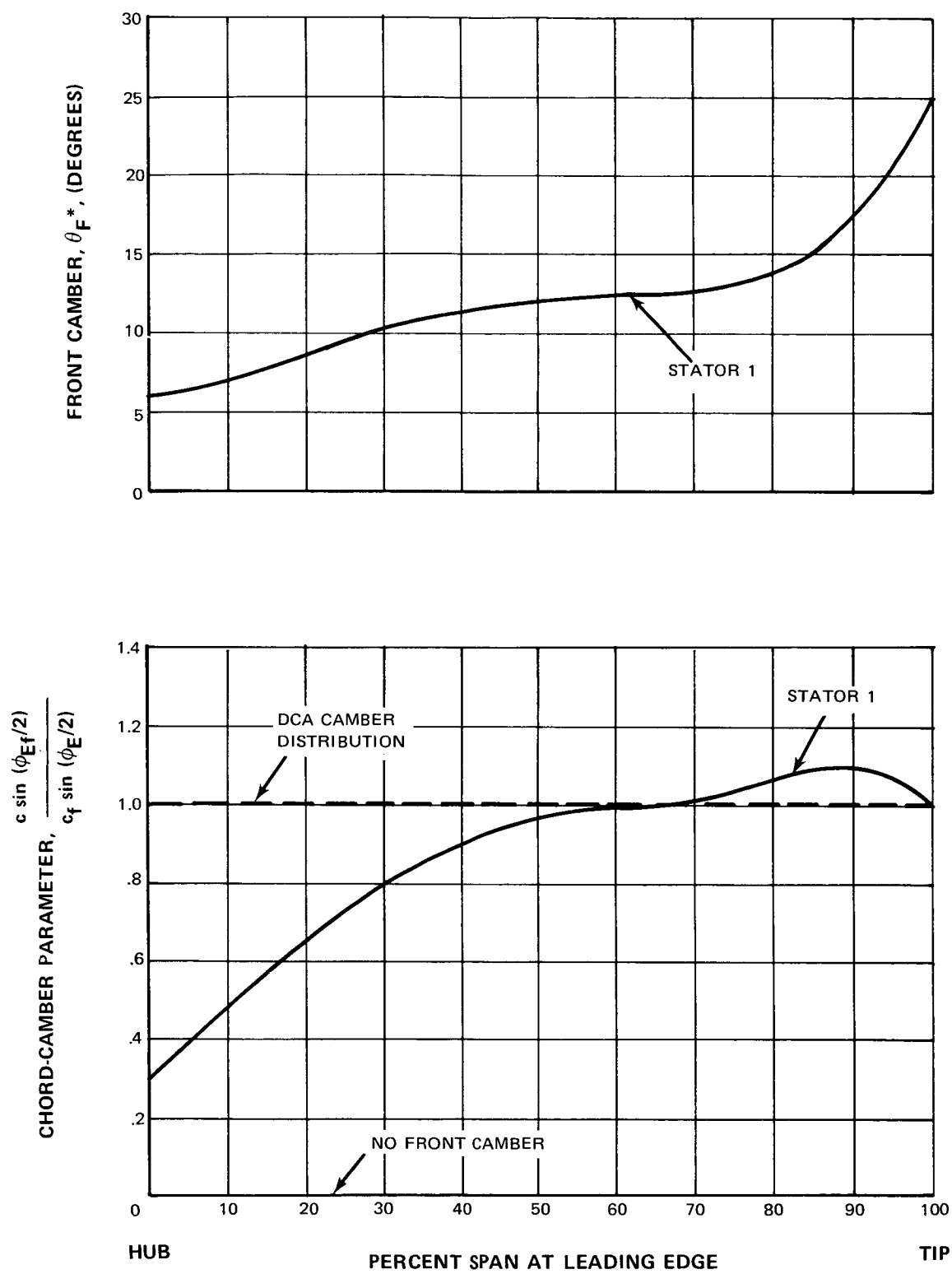


Figure 34 Stator 1 Front Camber Angle and Chord-Camber Parameter Spanwise Profiles

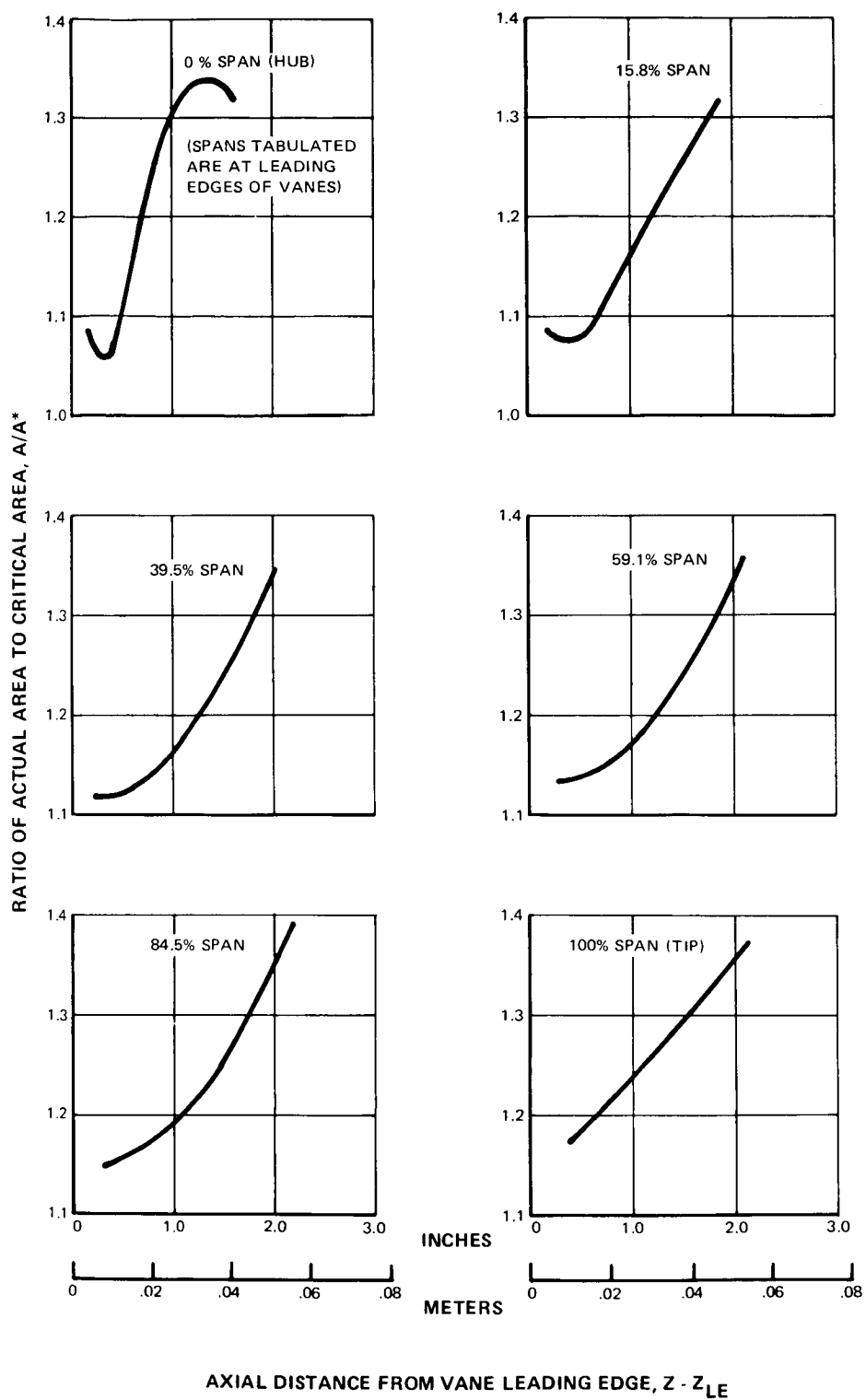


Figure 35 Stator 1 Channel Area Ratios Versus Axial Distance

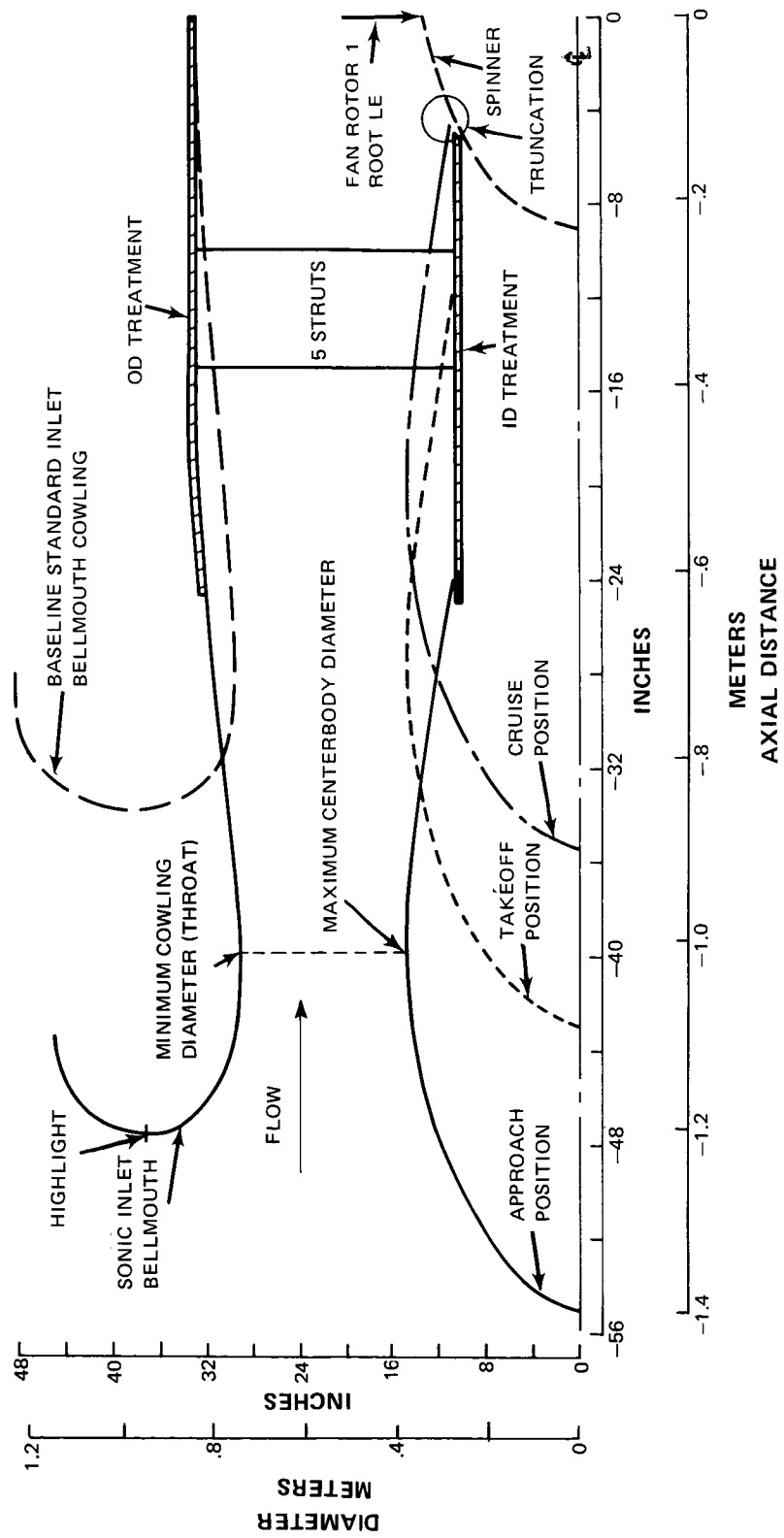


Figure 36 Baseline Standard and Sonic Inlet Geometries

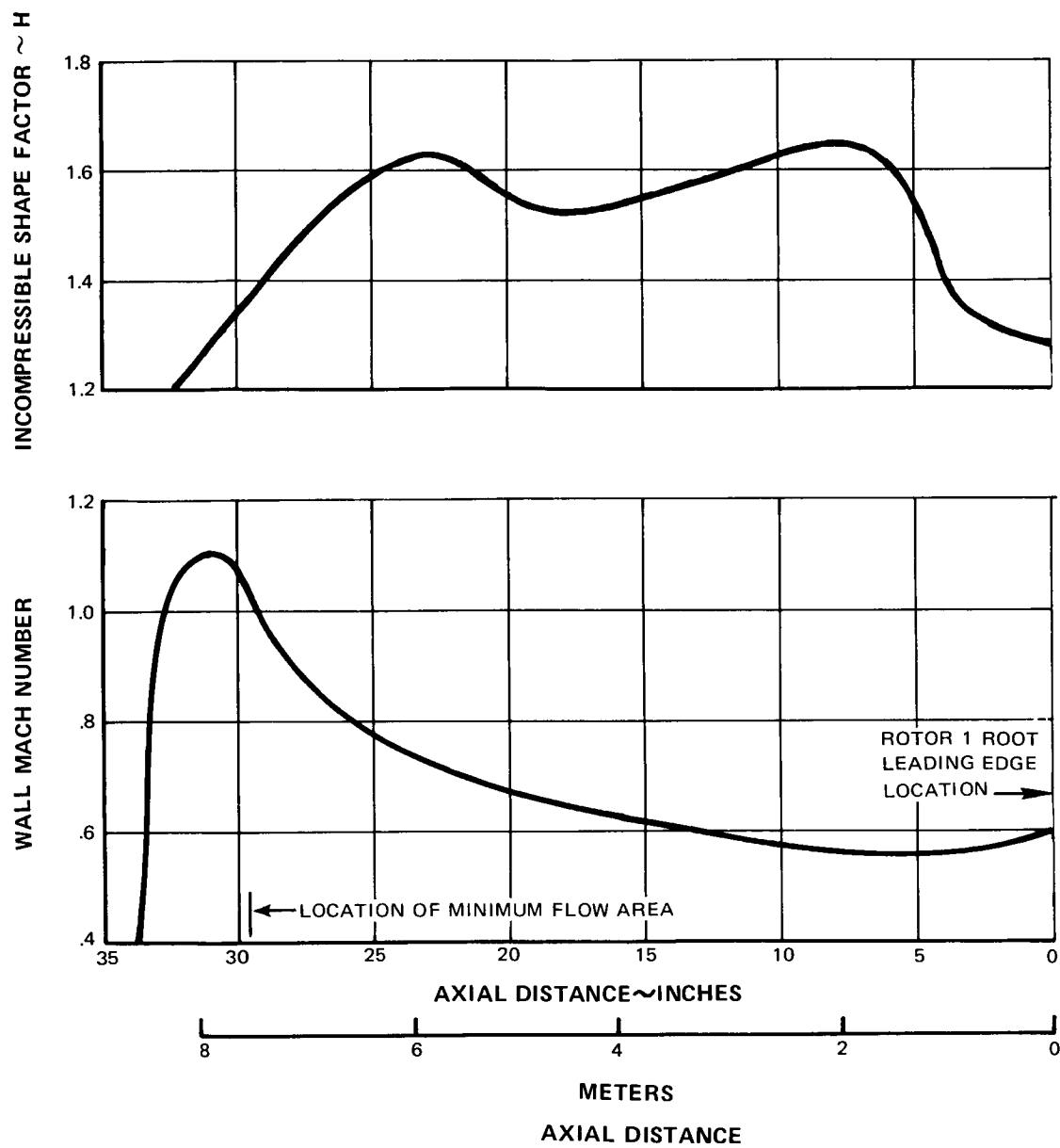


Figure 37 Baseline Standard Inlet Outer Wall Mach Number and Shape Factor Distributions

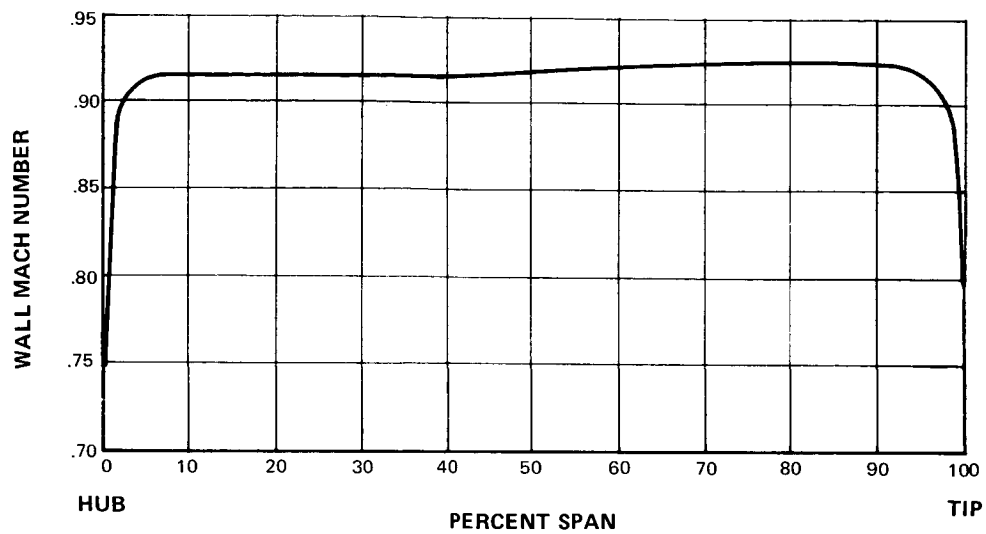


Figure 38 Sonic Inlet Throat Mach Number Spanwise Profile – Approach Configuration

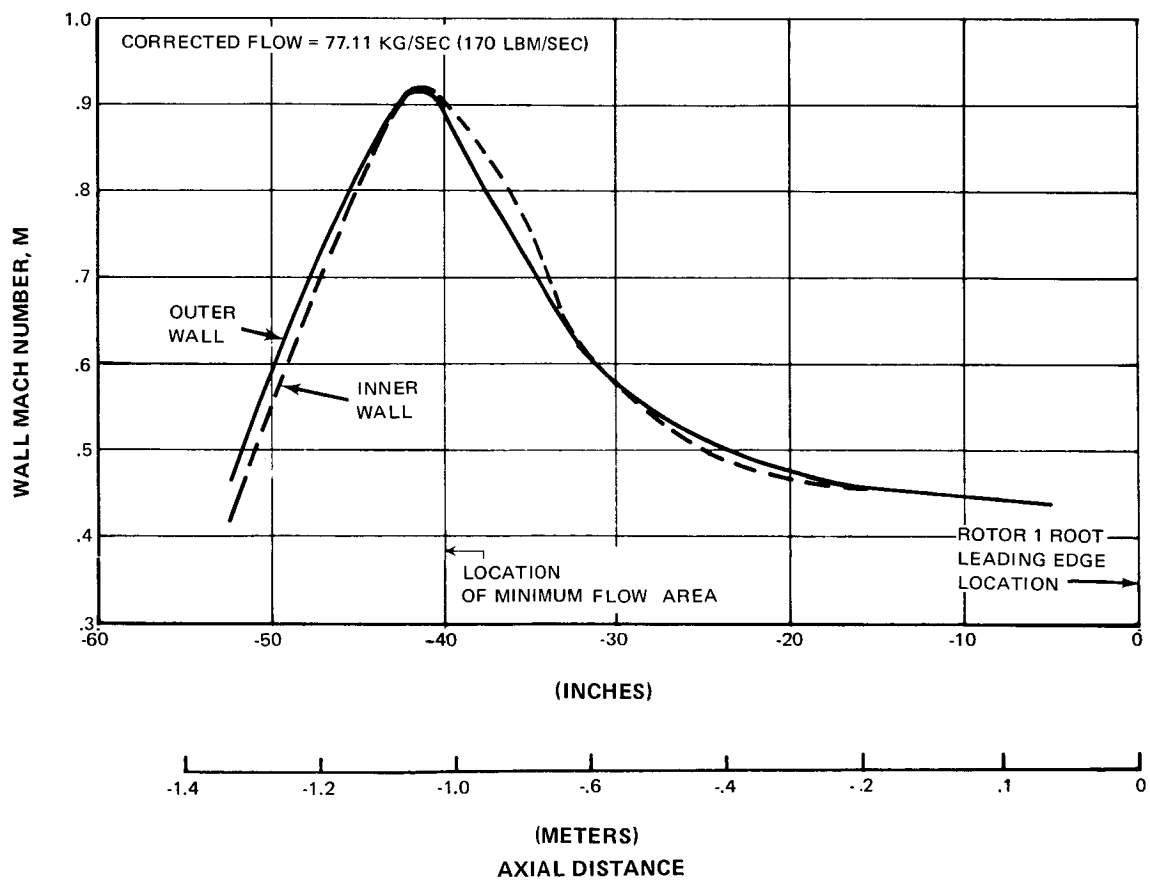


Figure 39 Mach Number Distributions Along Inlet Walls – Approach Configuration

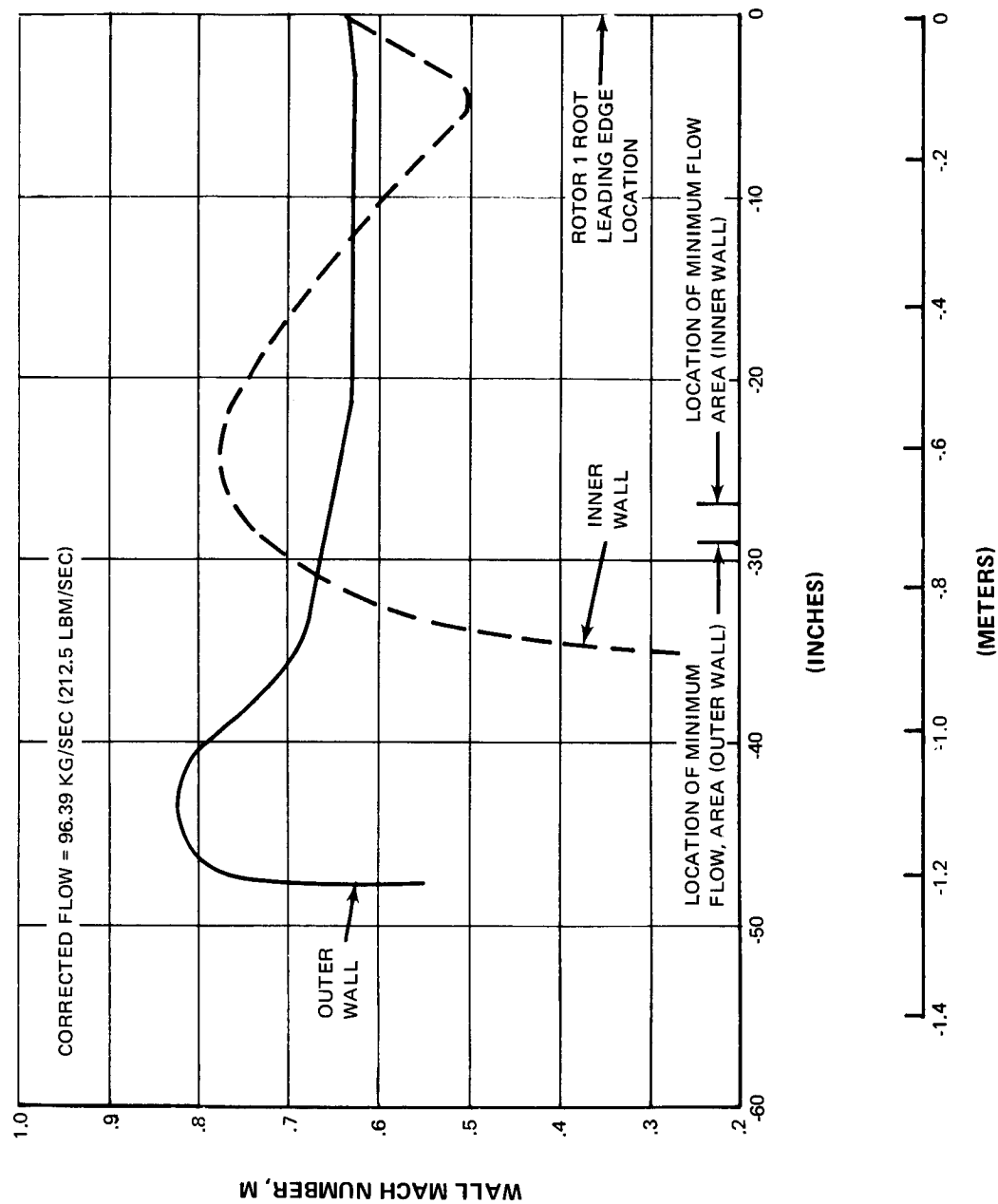


Figure 40 Mach Number Distributions Along Inlet Walls – Cruise Configuration

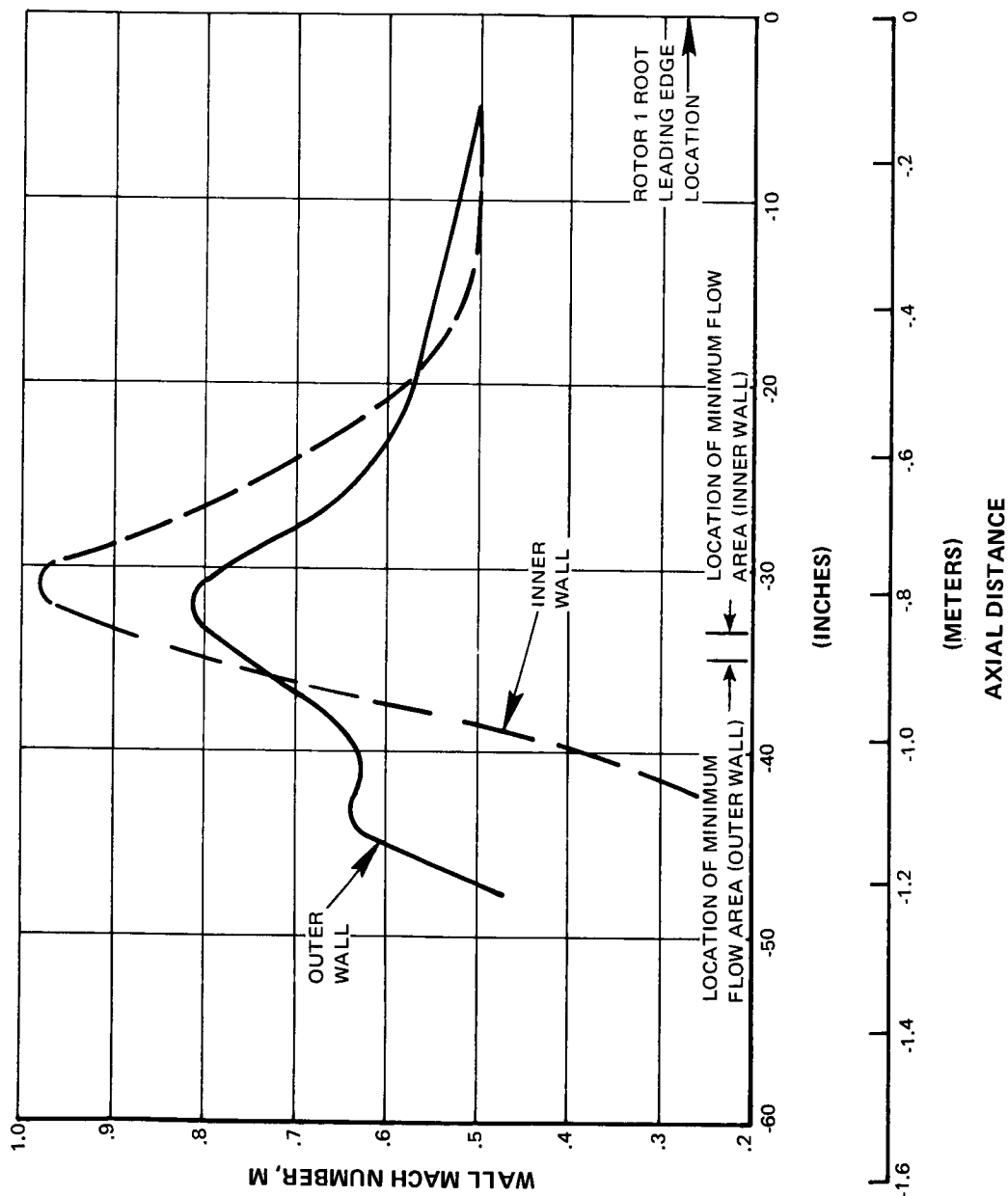


Figure 41 Mach Number Distributions Along Inlet Walls – Takeoff Configuration

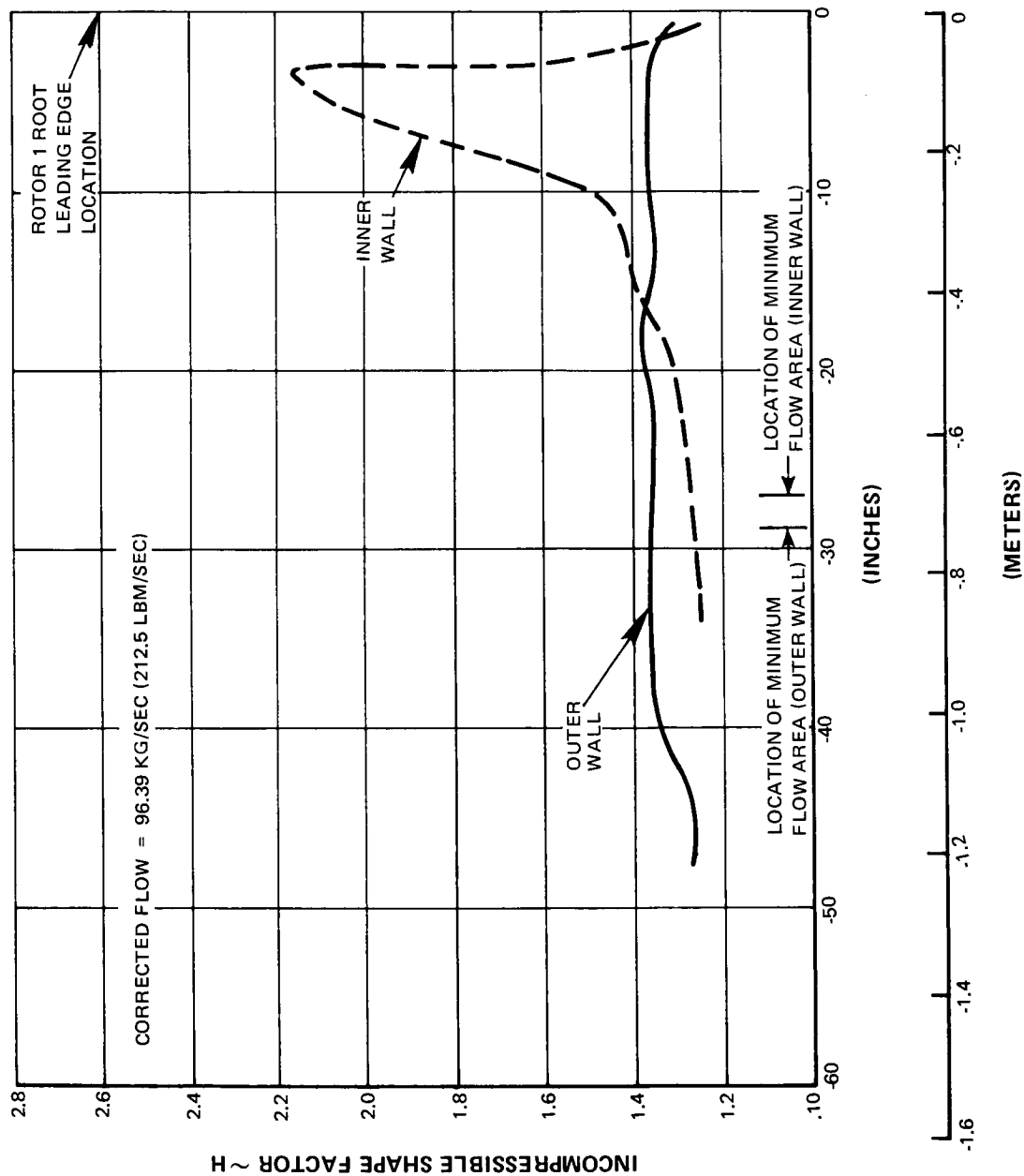


Figure 42 Boundary Layer Shape Factor Distributions Along Inlet Walls — Cruise Configuration

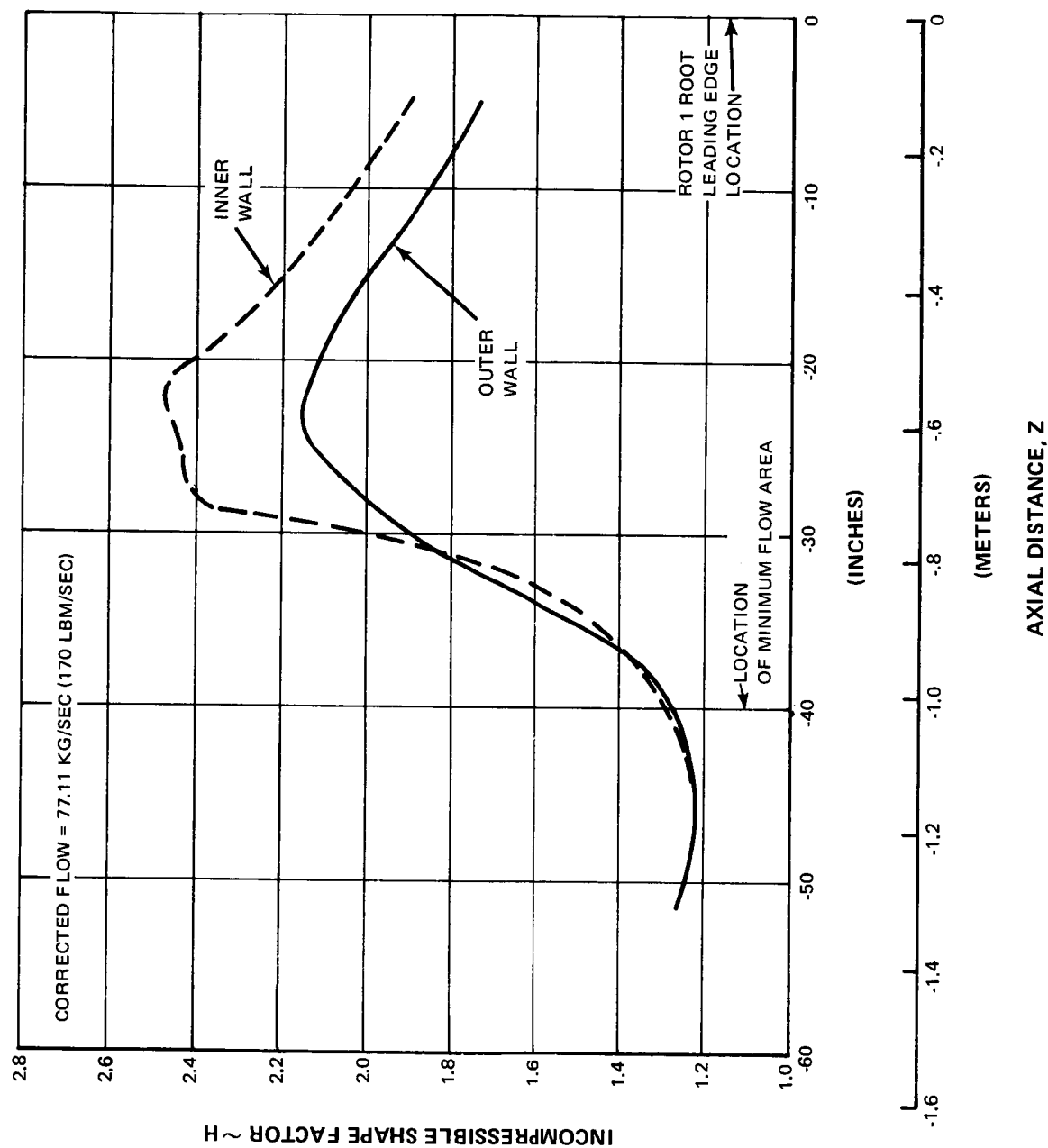


Figure 43 Boundary Layer Shape Factor Distributions Along Inlet Walls – Approach Configuration

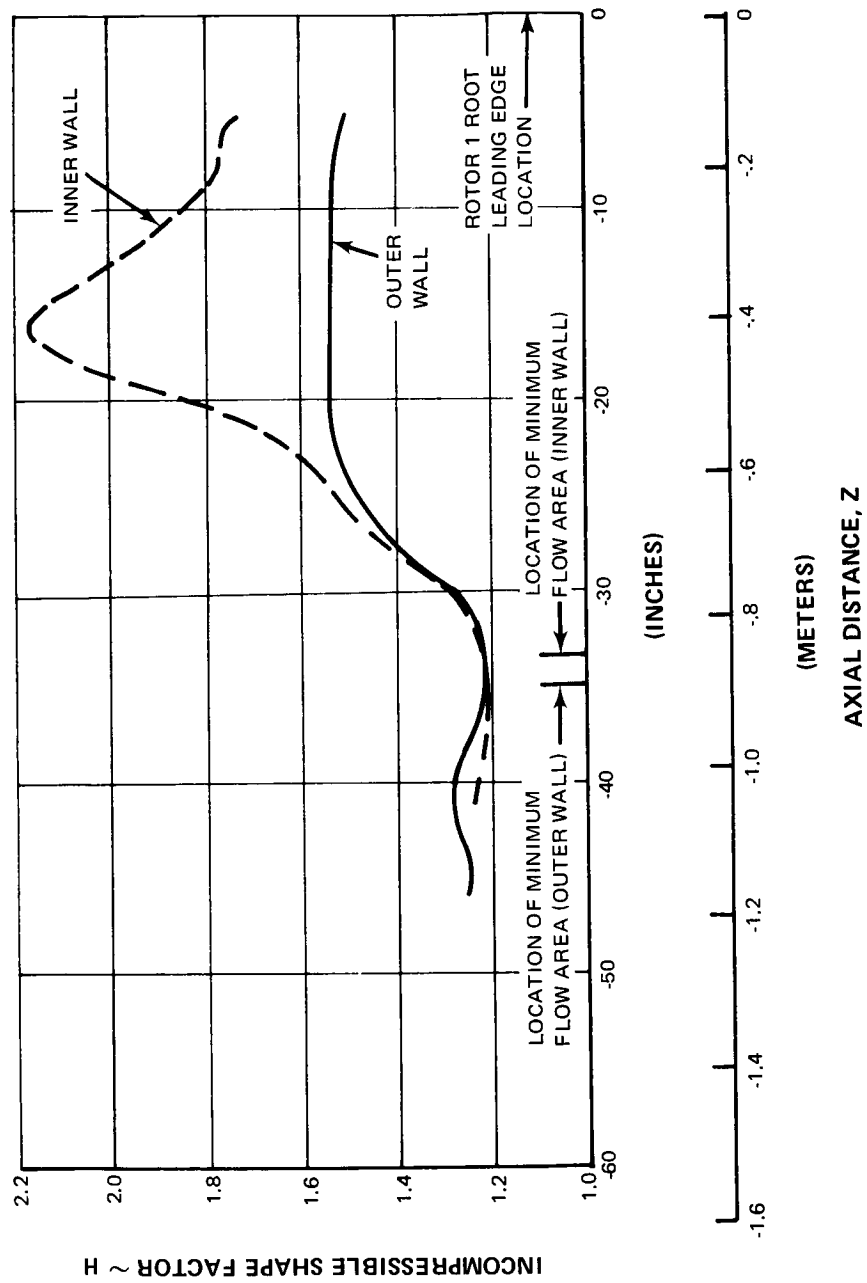


Figure 44 Boundary Layer Shape Factor Distributions Along Inlet Walls — Takeoff Configuration

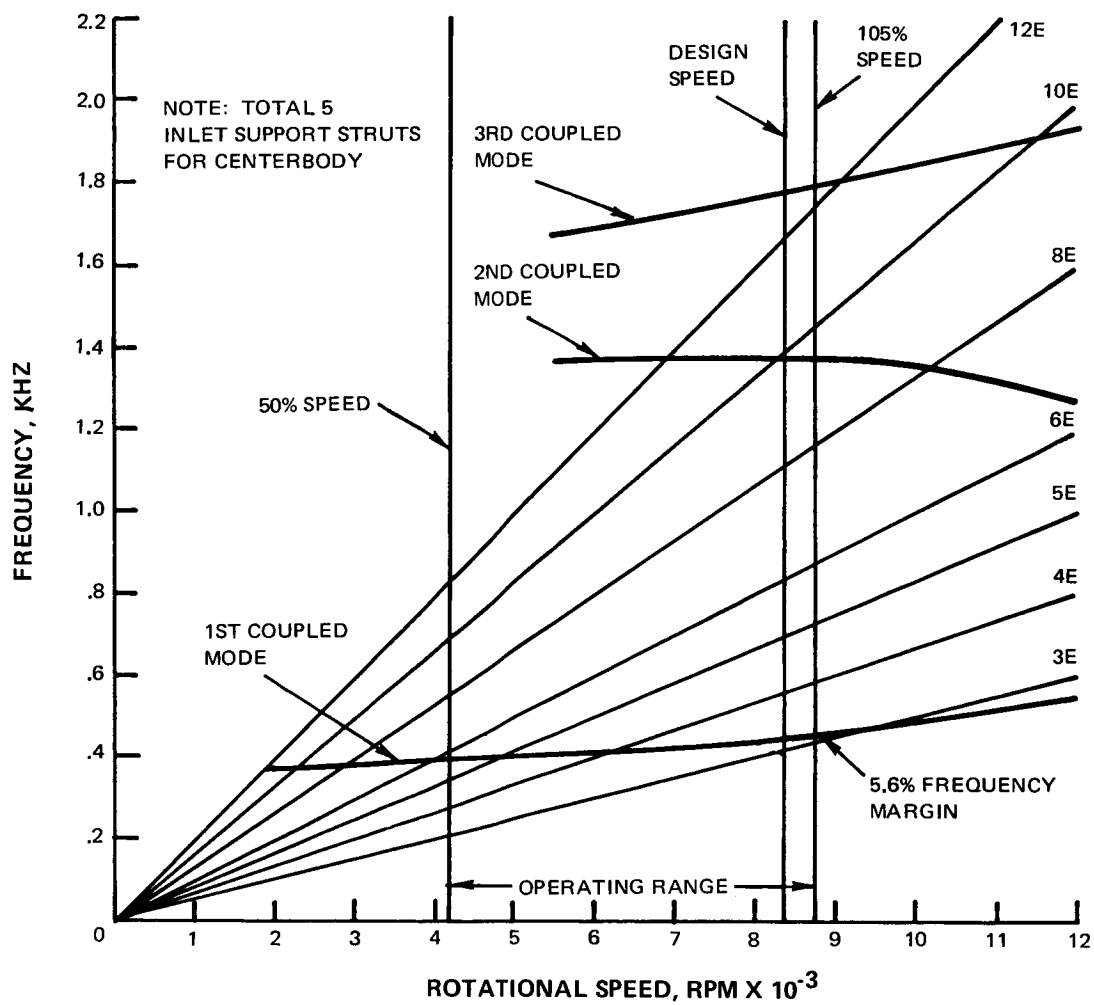


Figure 45 Rotor 1 Campbell Diagram

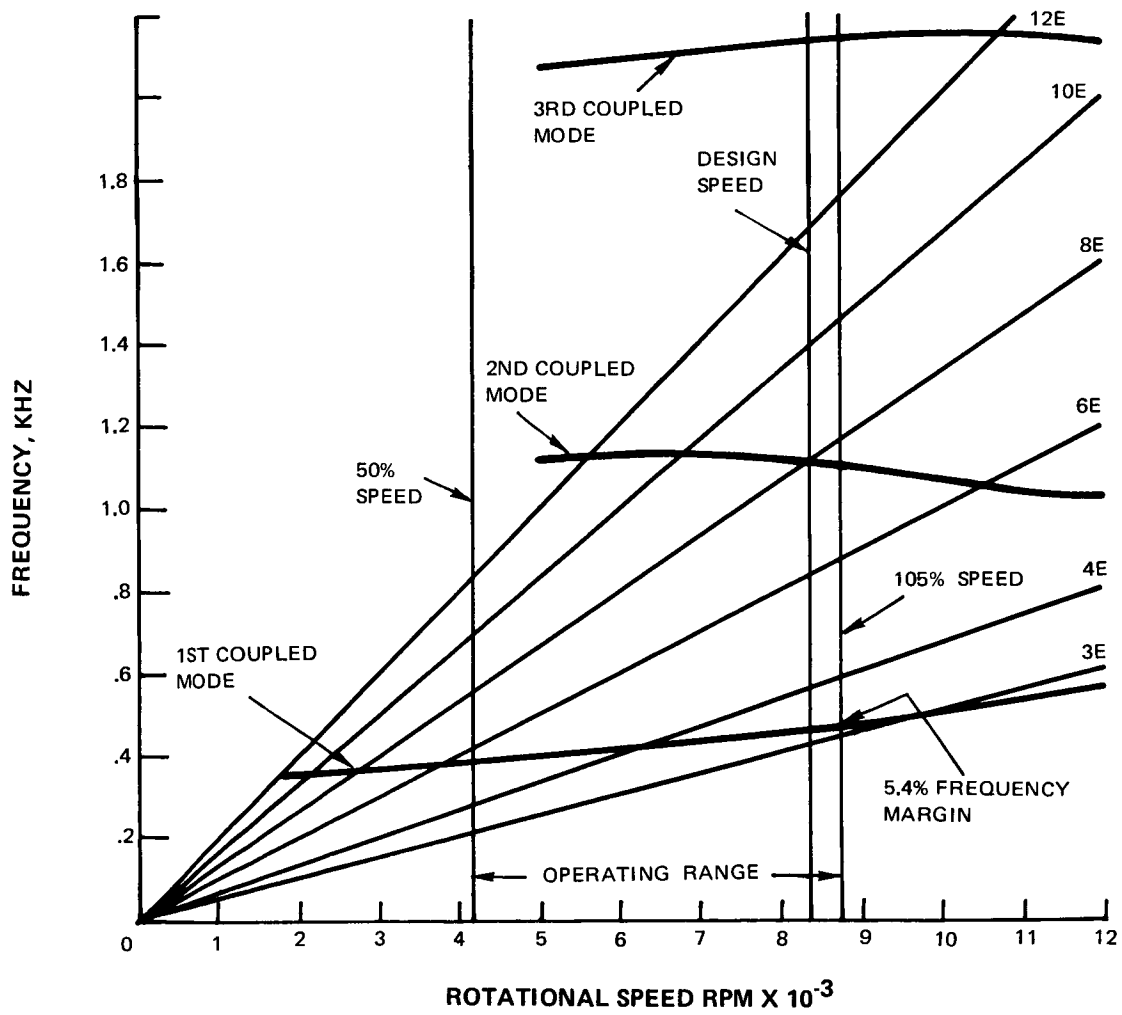


Figure 46 Rotor 2 Campbell Diagram

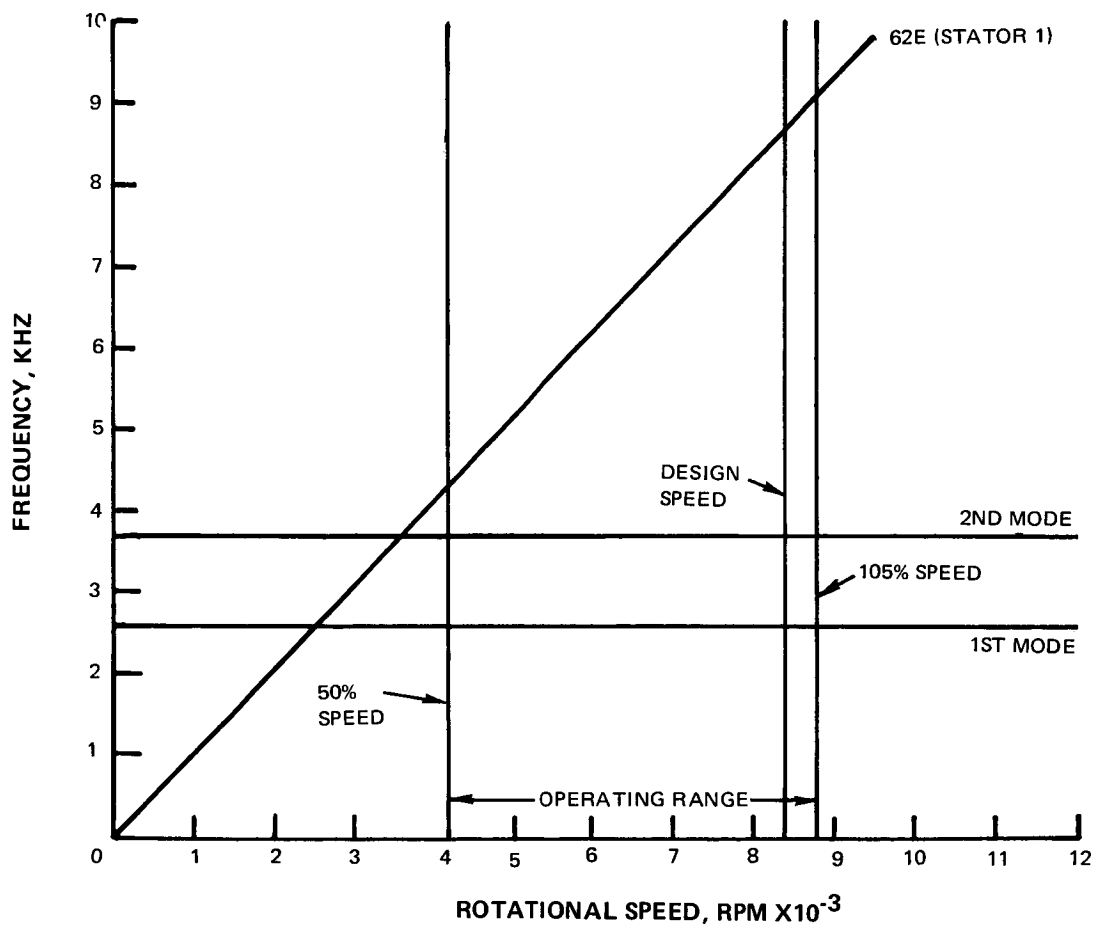


Figure 47 Rotor 1 Tip Mode Campbell Diagram

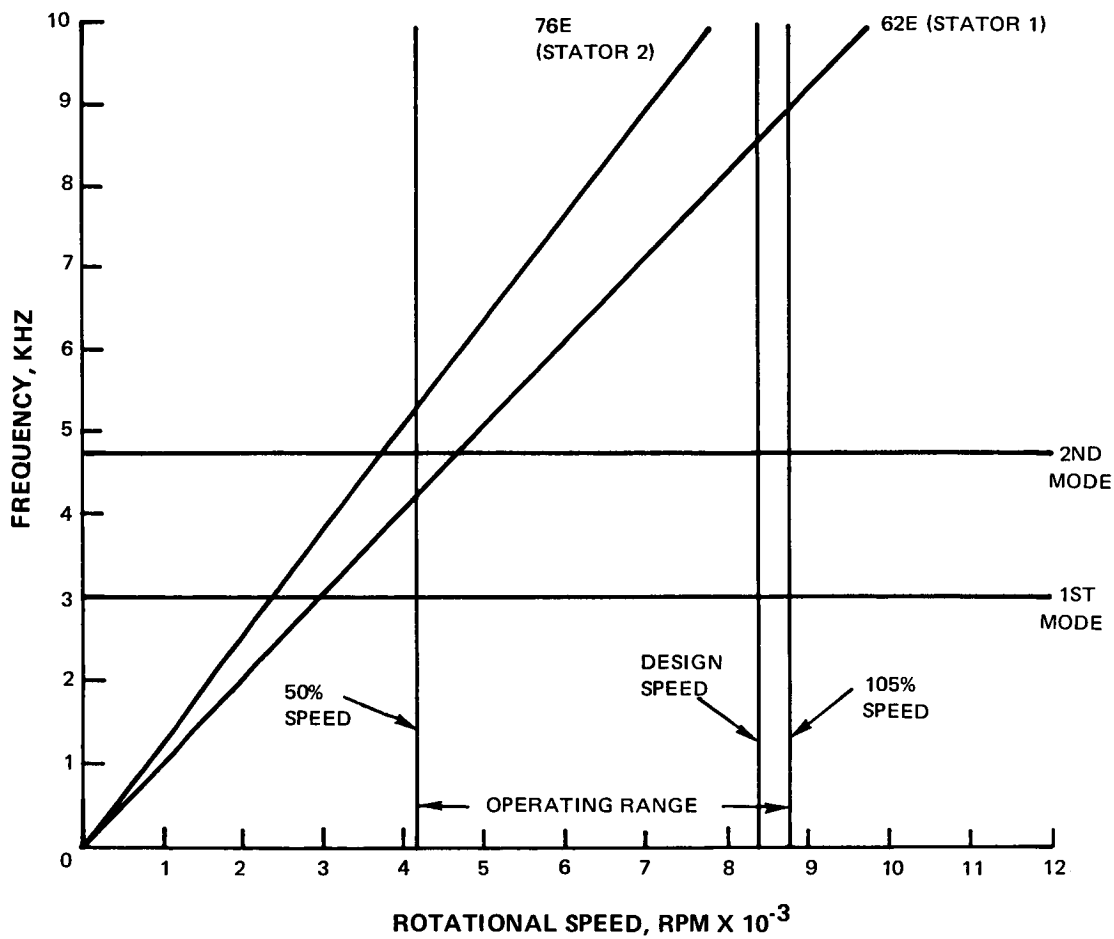


Figure 48 Rotor 2 Tip Mode Campbell Diagram

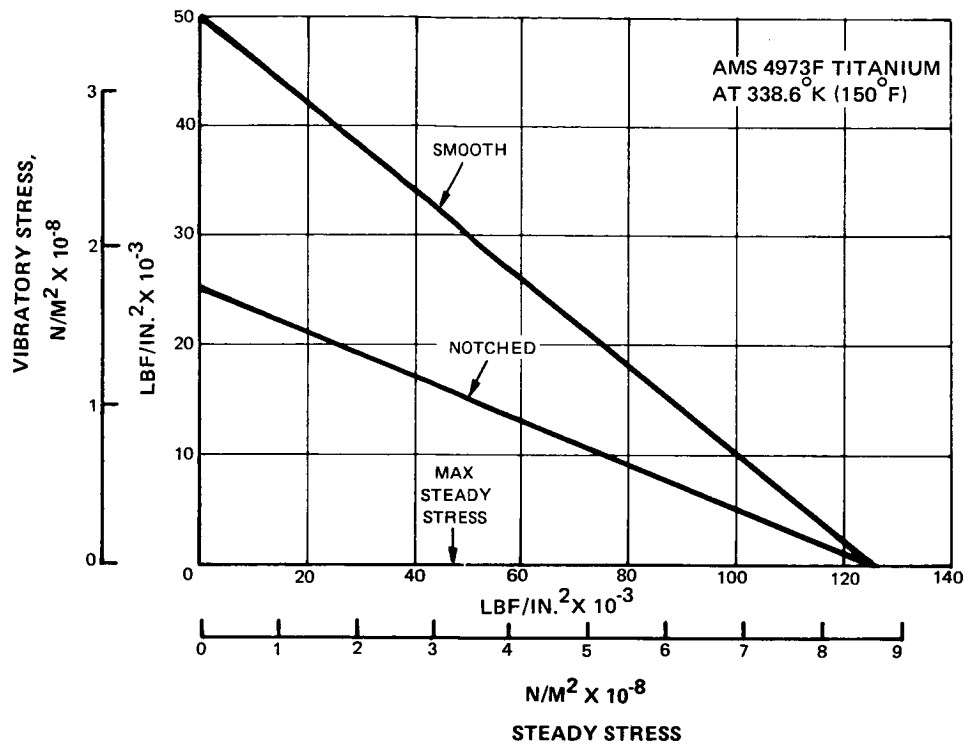


Figure 49 Rotor 1 Goodman Diagram

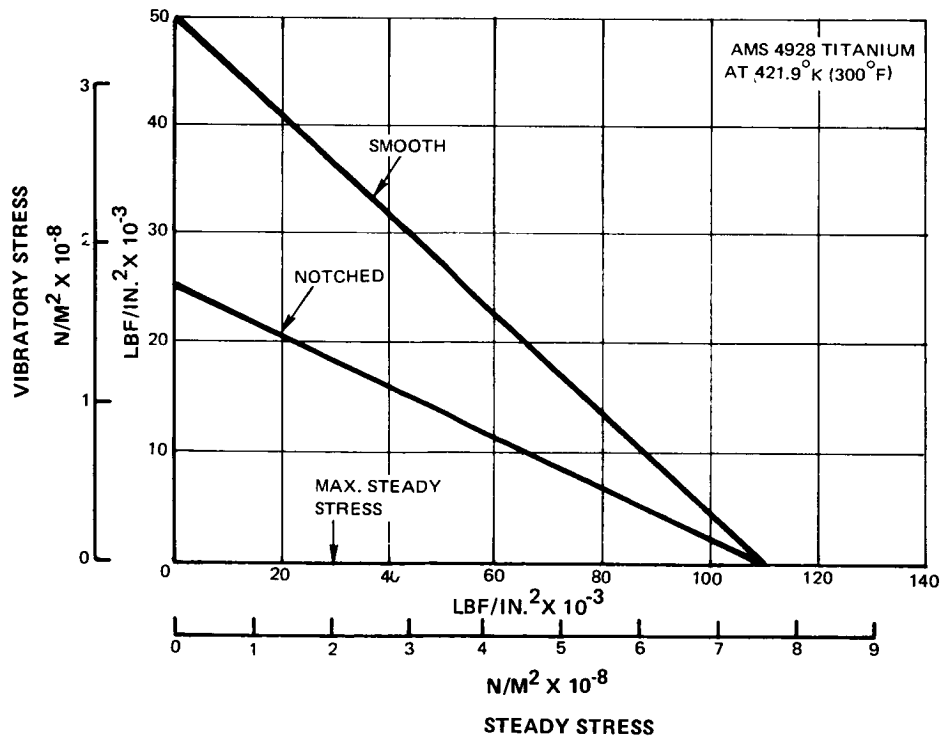


Figure 50 Rotor 2 Goodman Diagram

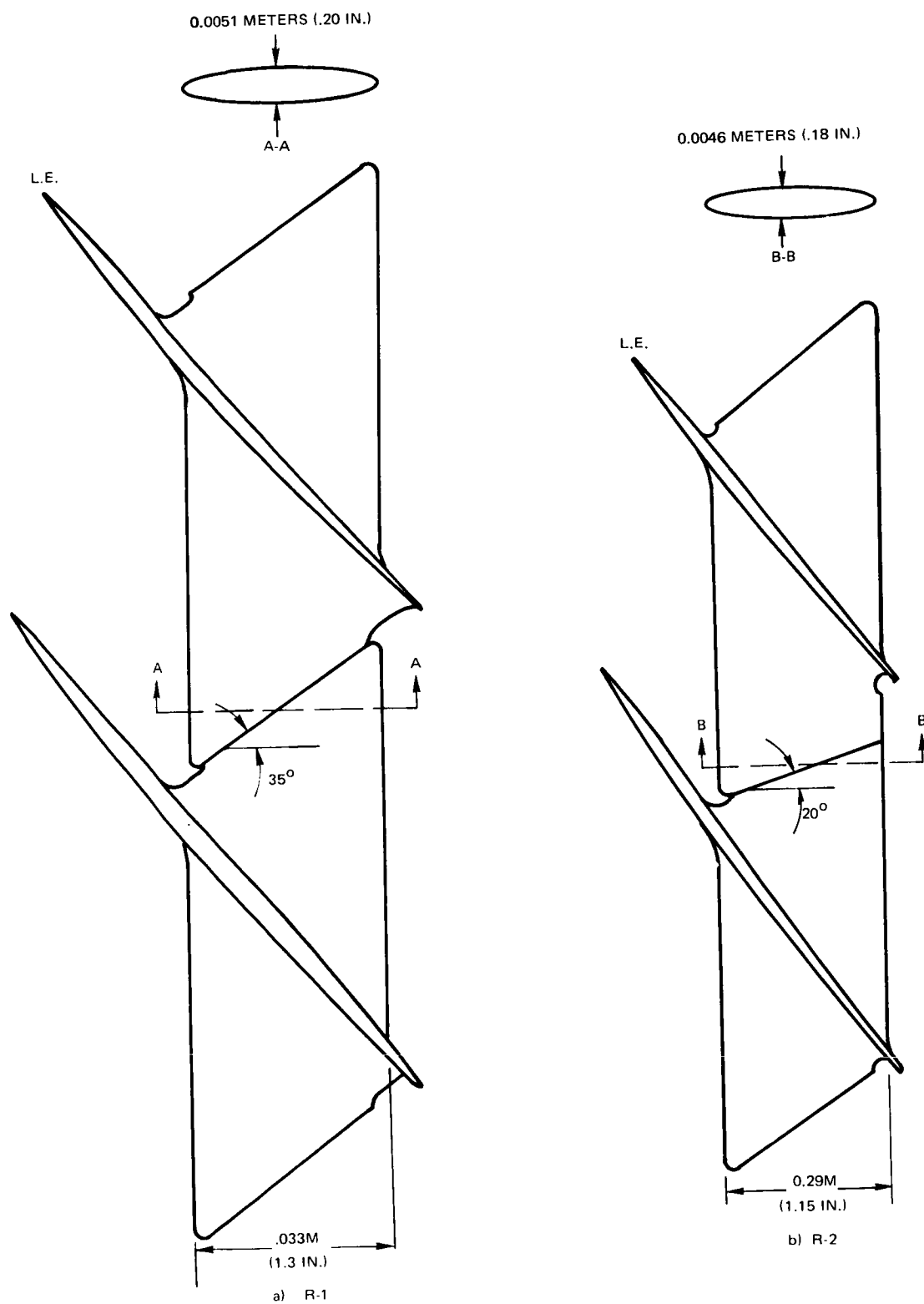


Figure 51 Schematic of Rotor Partspan Shrouds

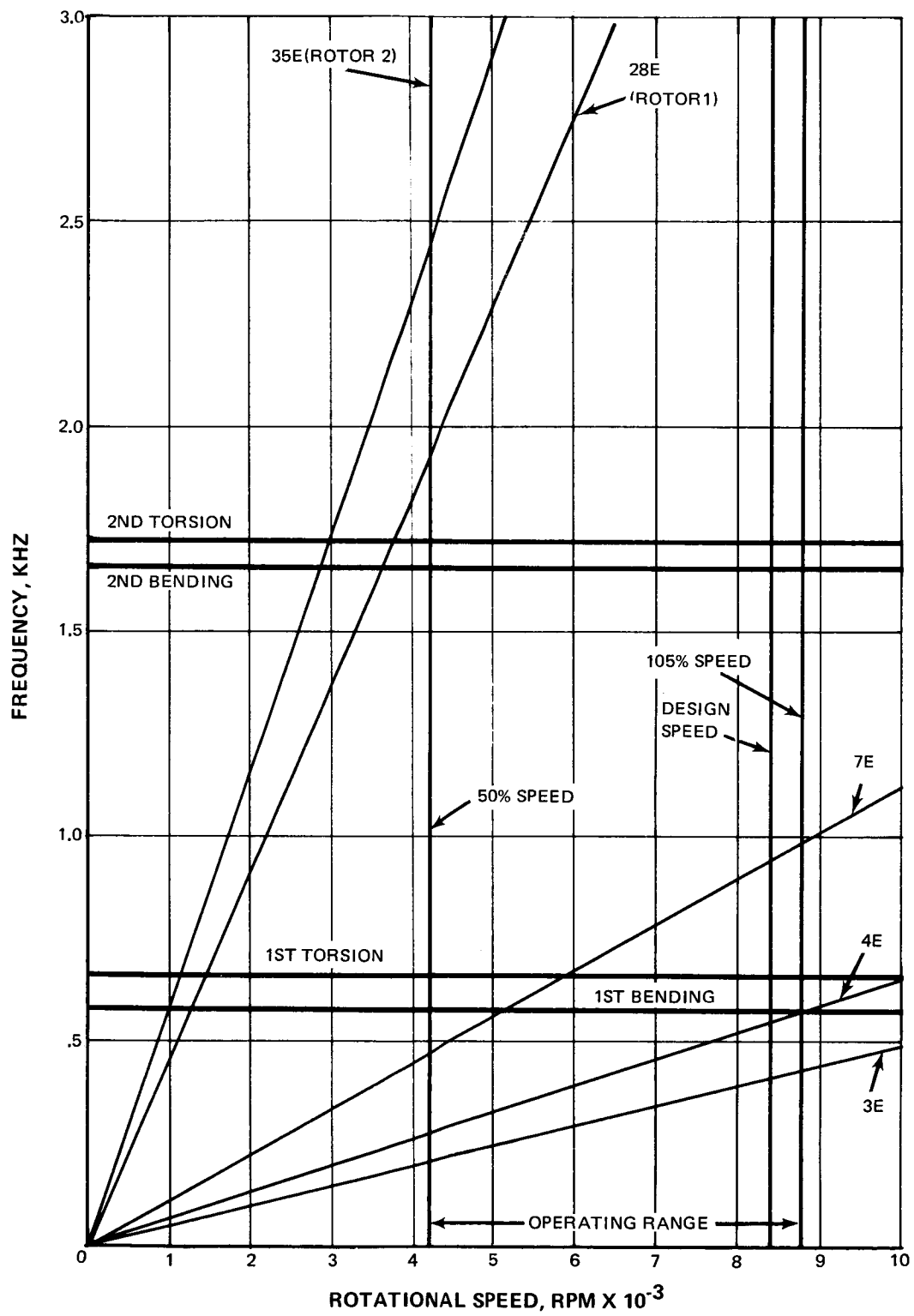


Figure 52 Stator 1 Campbell Diagram

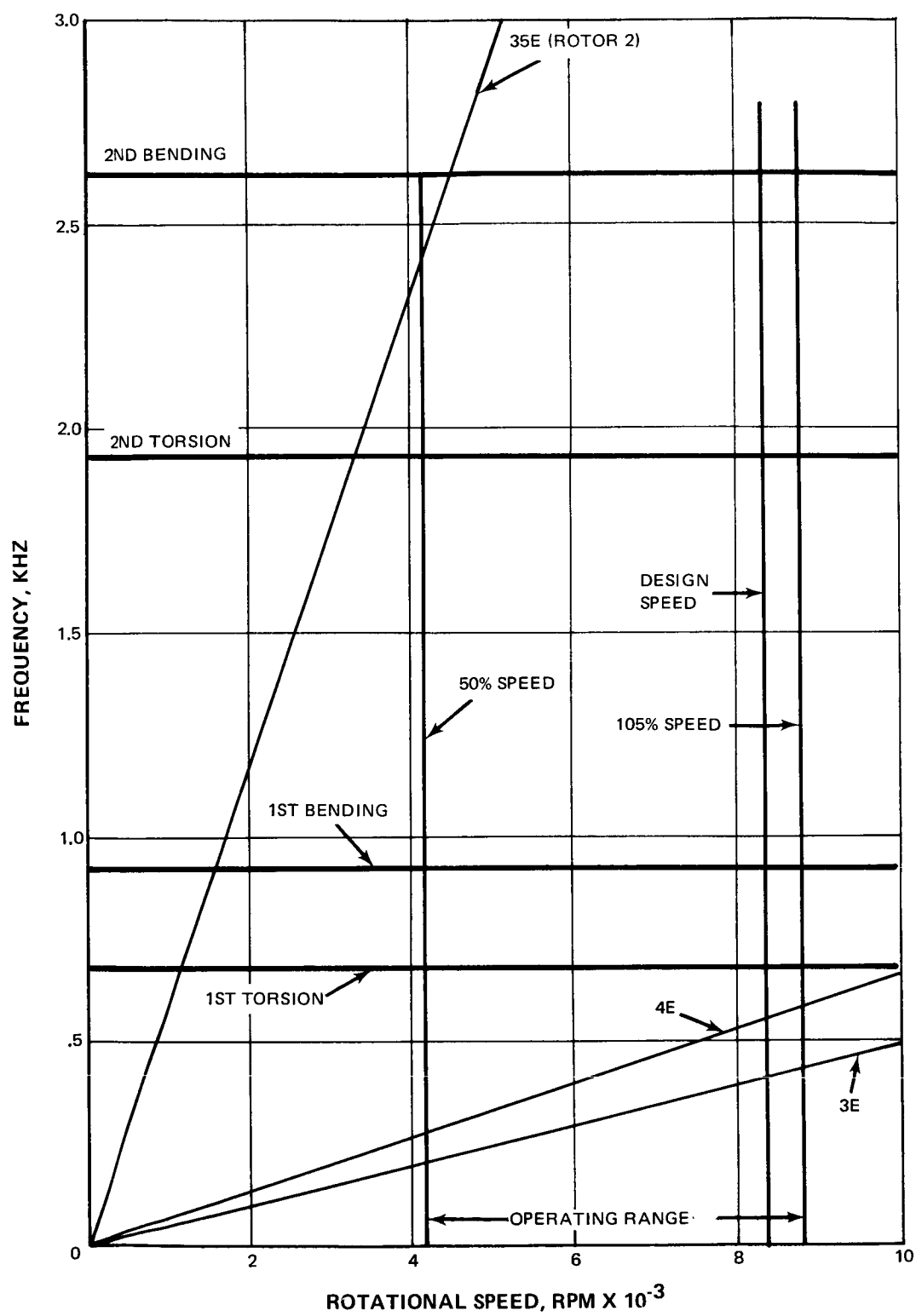


Figure 53 Stator 2 Campbell Diagram

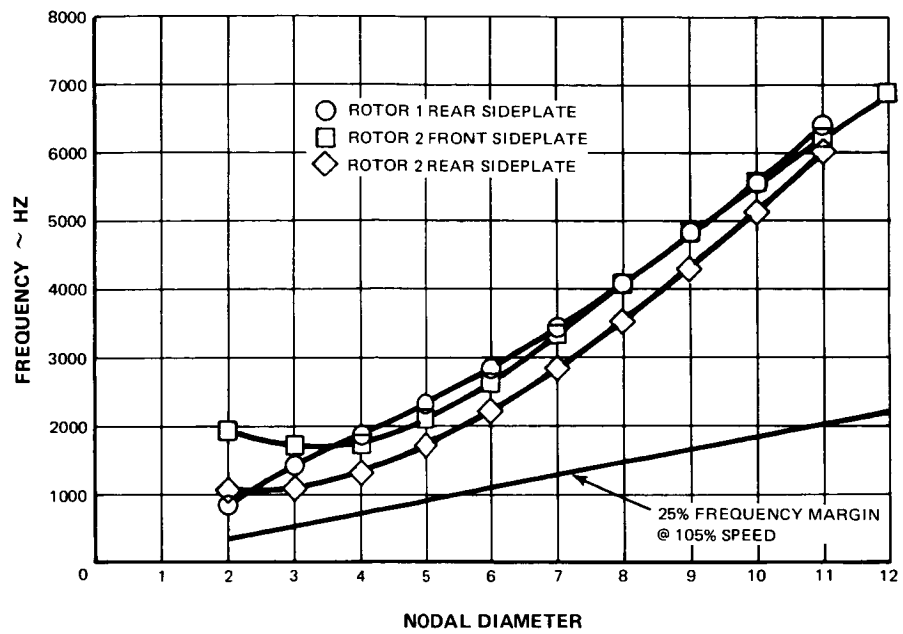


Figure 54 Rotor Sideplate Seal Resonance

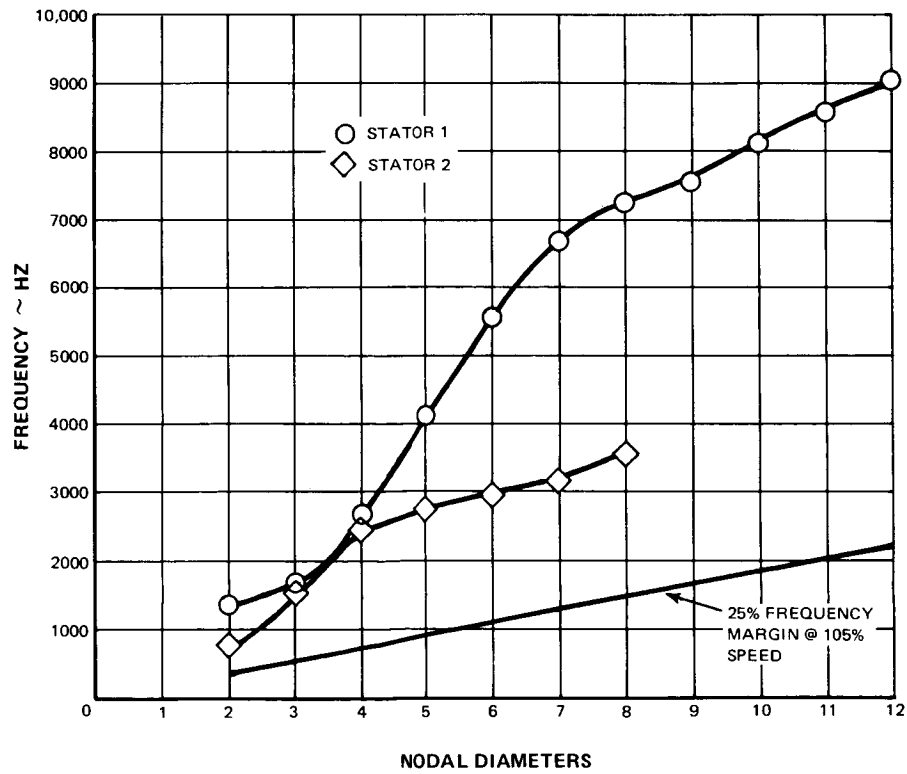


Figure 55 Stator Sideplate Seal Resonance

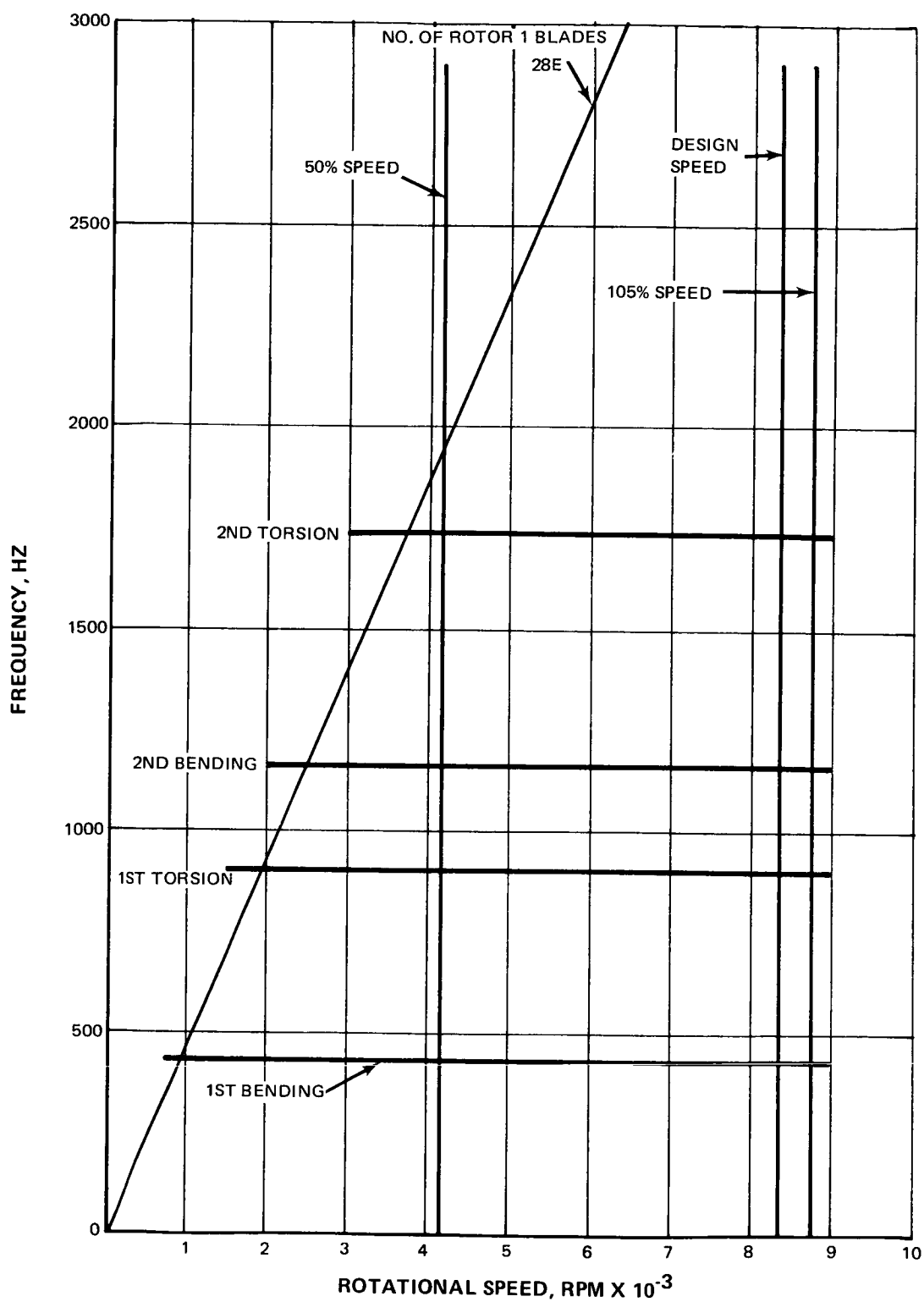
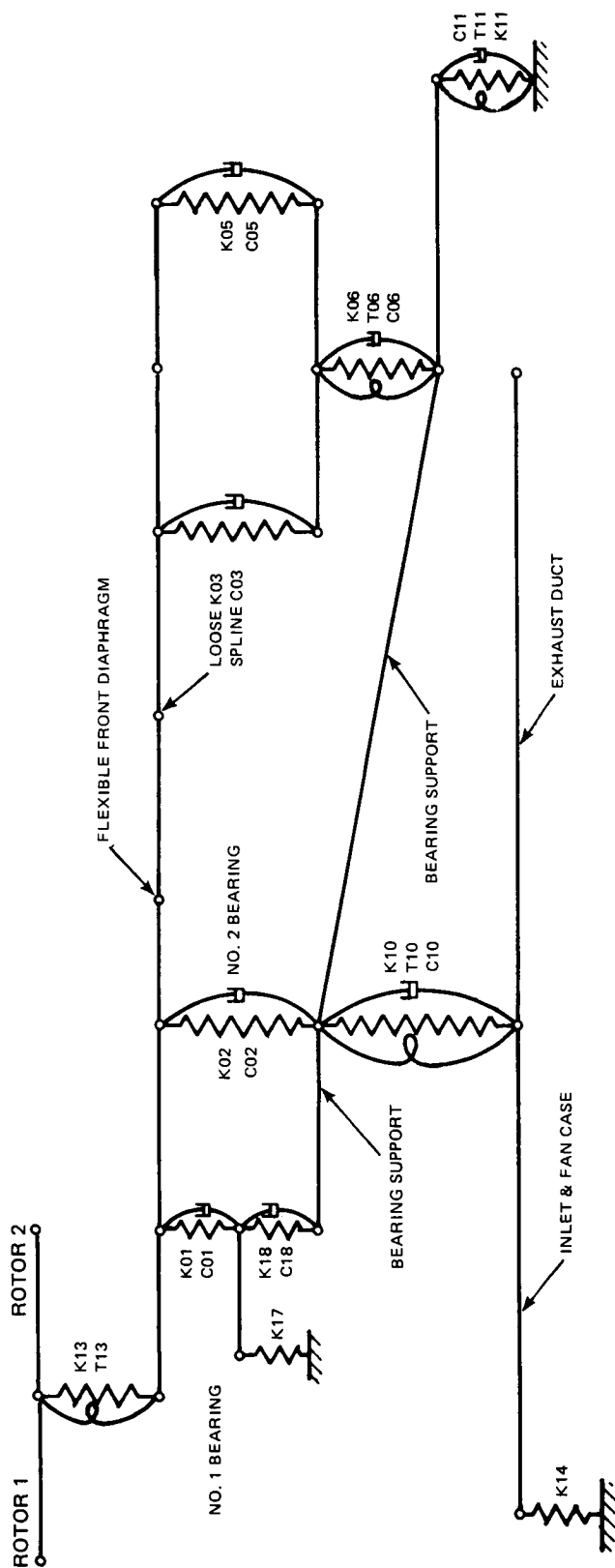


Figure 56 Sonic Inlet Support Struts, Campbell Diagram



# STRUCTURAL DAMPING COEFFICIENTS

lb/in. -sec	(N/m - sec x 10 <sup>-3</sup> )
C01 = 10	1.75
C02 = 10	1.75
C03 = 10	1.75
C05 = 10	1.75
C06 = 100	17.5
C10 = 100	17.5
C11 = 200	35.0
C18 = 400	70.0

# TORSIONAL SPRING RATES

in-lbf/deg x 10 <sup>-8</sup>	(m-N/rad x 10 <sup>-9</sup> )
T06 = 4.0	2.6
T010 = 10.0	6.5
T011 = 50.0	32.5
T013 = 10.0	6.5

# LINEAR SPRING RATES

lb/in.	(N/m x 10 <sup>-8</sup> )
K01 = 0.5	0.9
K02 = 2.0	3.5
K03 = 2.0	3.5
K05 = 2.0	3.5
K06 = 10.0	17.5
K10 = 10.0	17.5
K11 = 1.0	1.8
K13 = 10.0	17.5
K14 = 0.00045	0.0008
K17 = 1.0	1.8
K18 = 0.4	0.6

Figure 57 Spring-Mass Model for Critical Speed Analysis - Standard Inlet

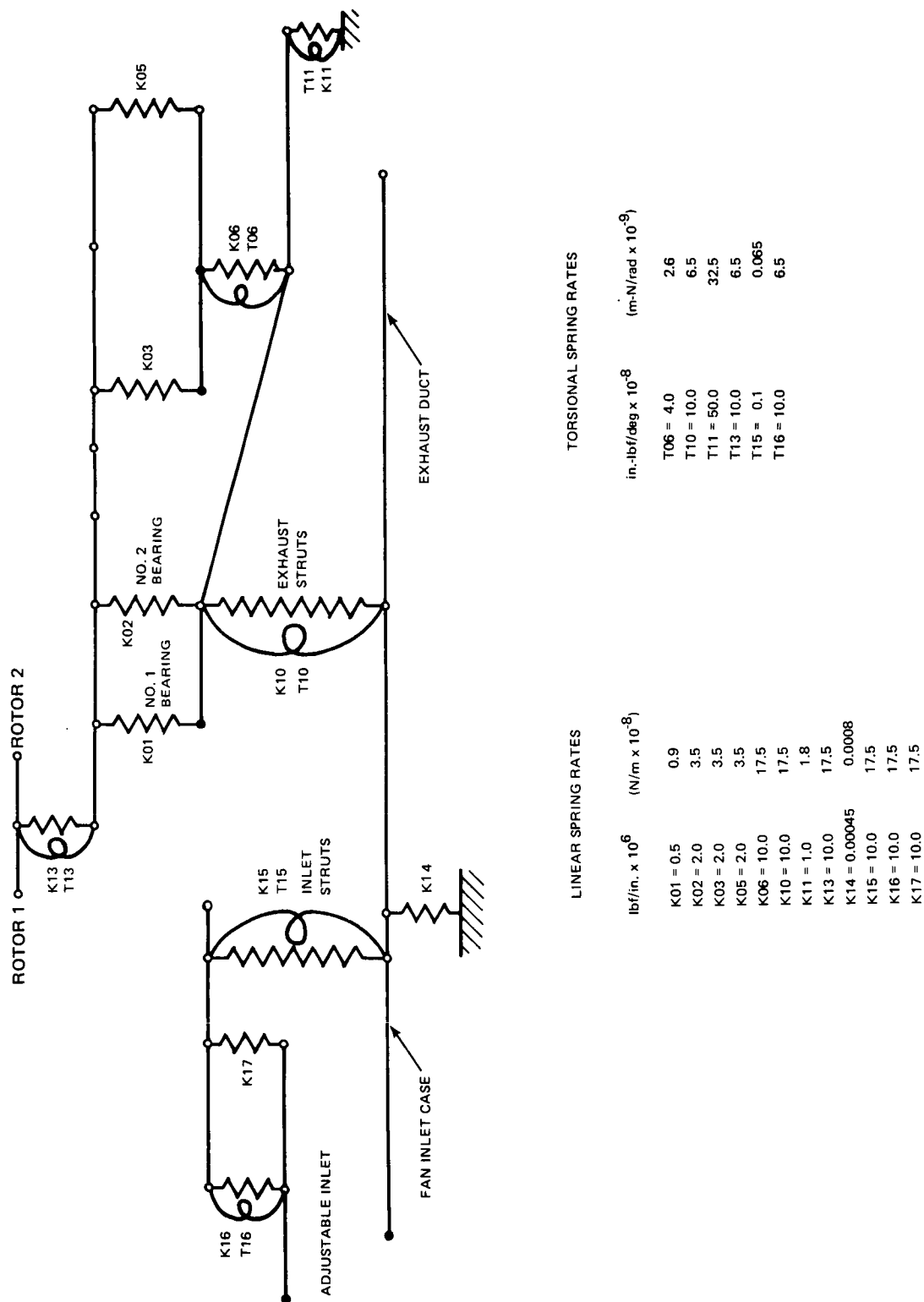


Figure 58 Spring-Mass Model for Critical Speed Analysis - Sonic Inlet

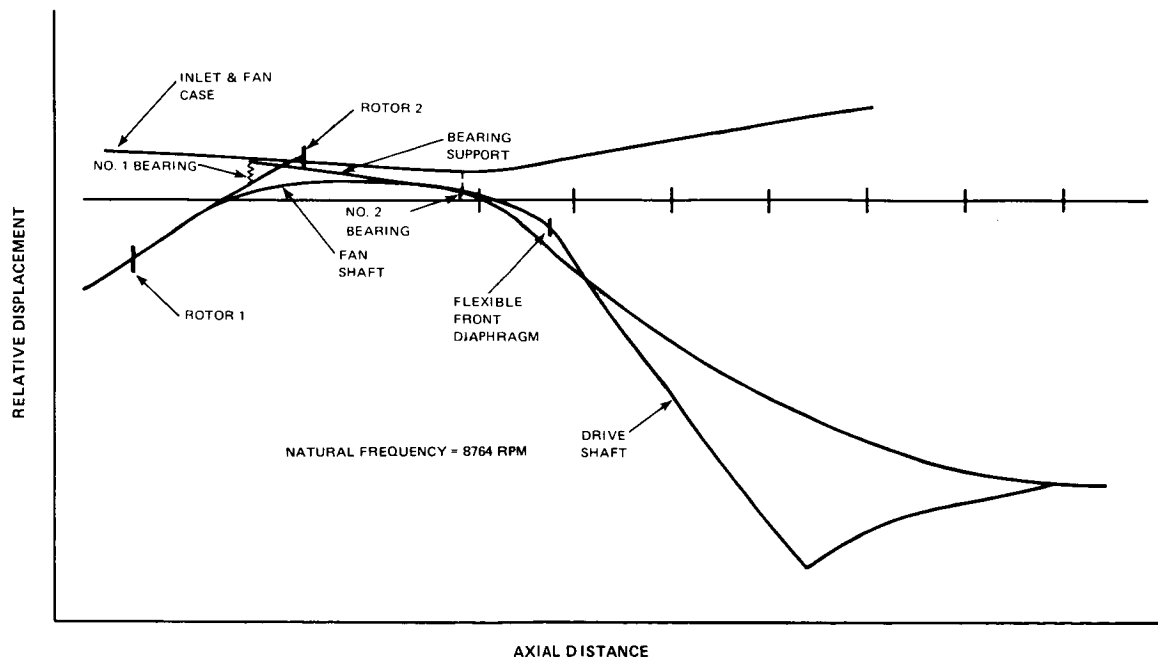
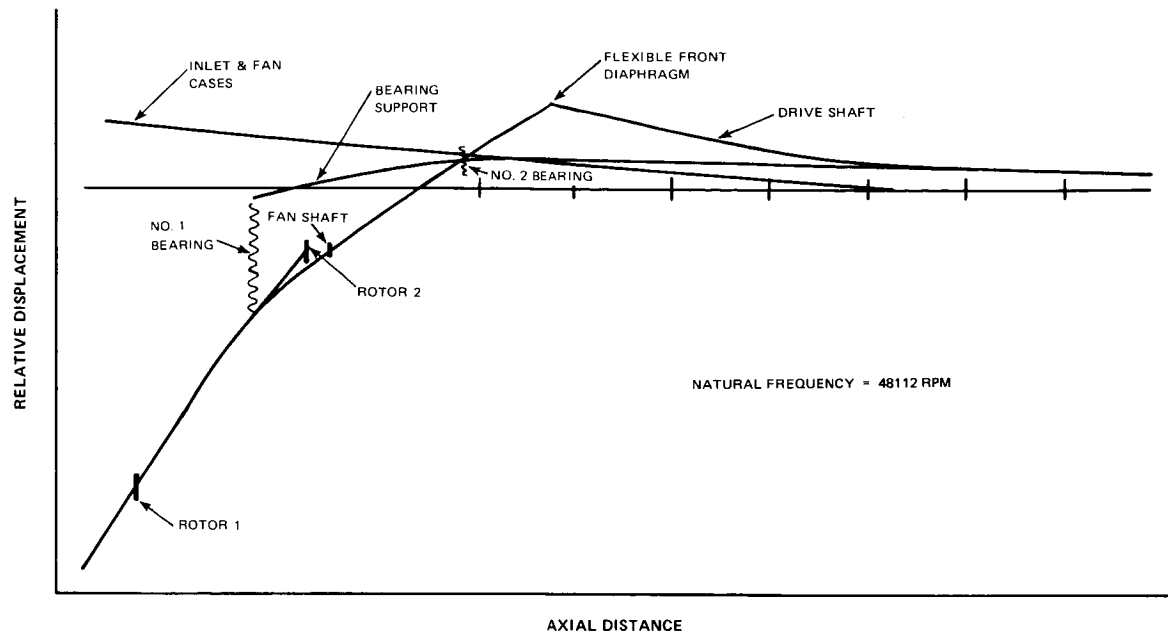


Figure 59 Critical Speed Mode Shapes

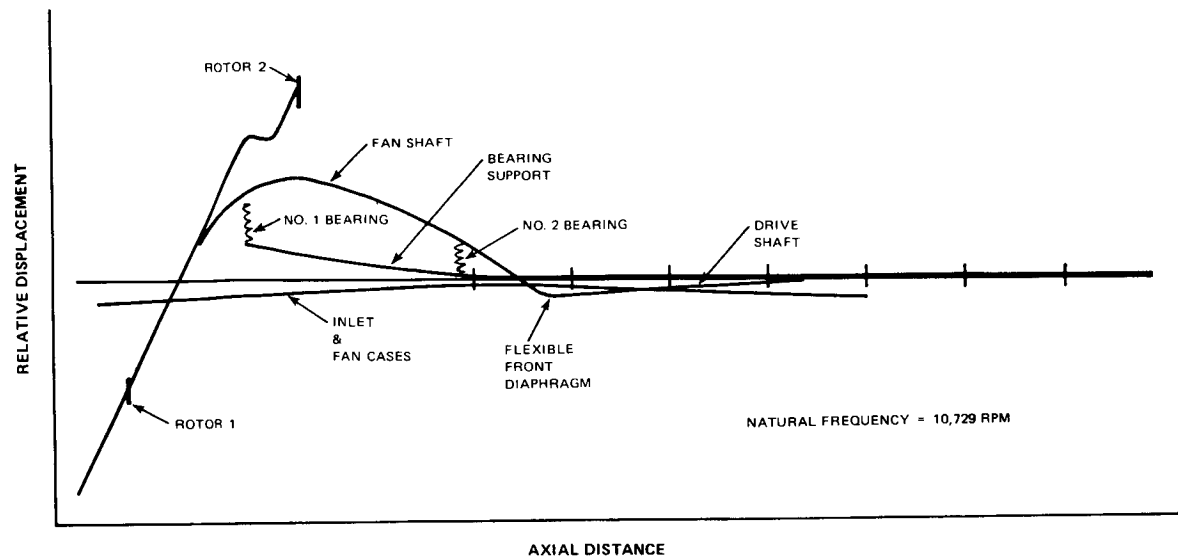


Figure 59 (Cont'd) Critical Speed Mode Shapes

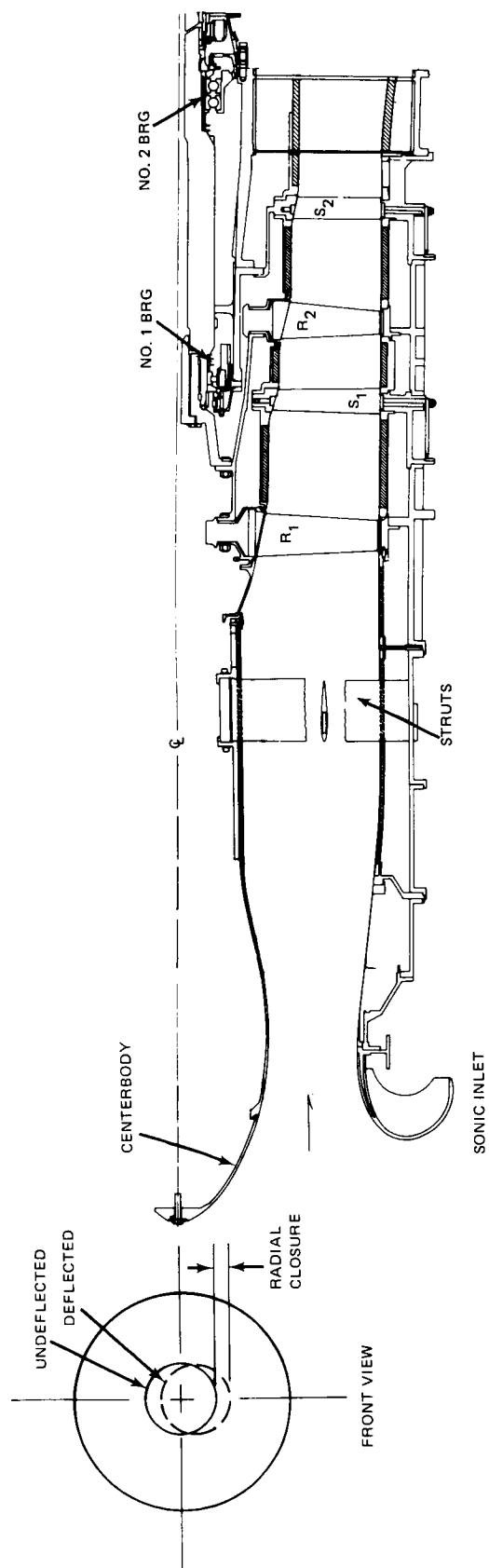


Figure 60 Schematic of Sonic Inlet Configuration

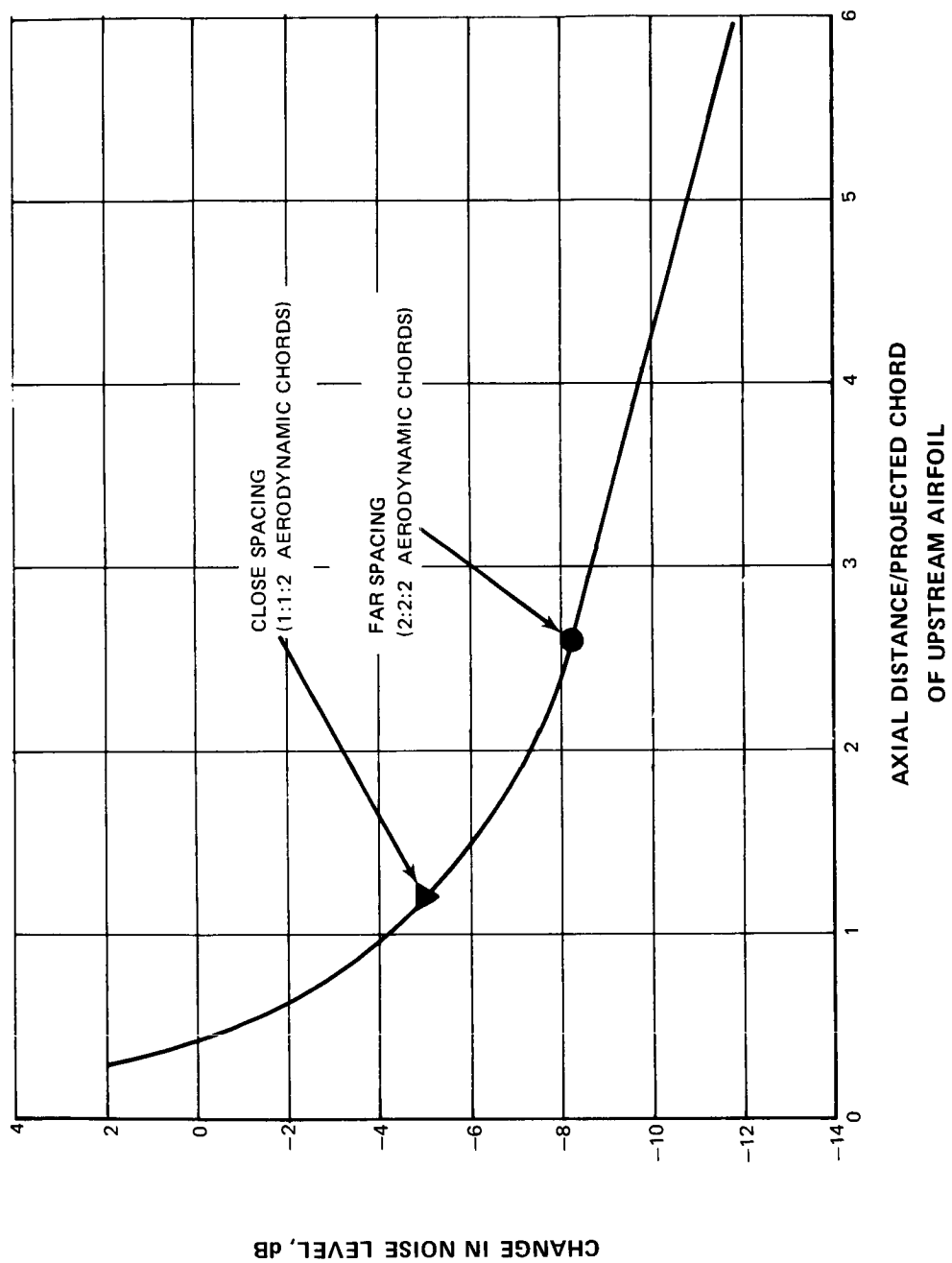


Figure 61 Effect of Rotor-Stator Spacing on Blade-Passing Frequency Noise Level

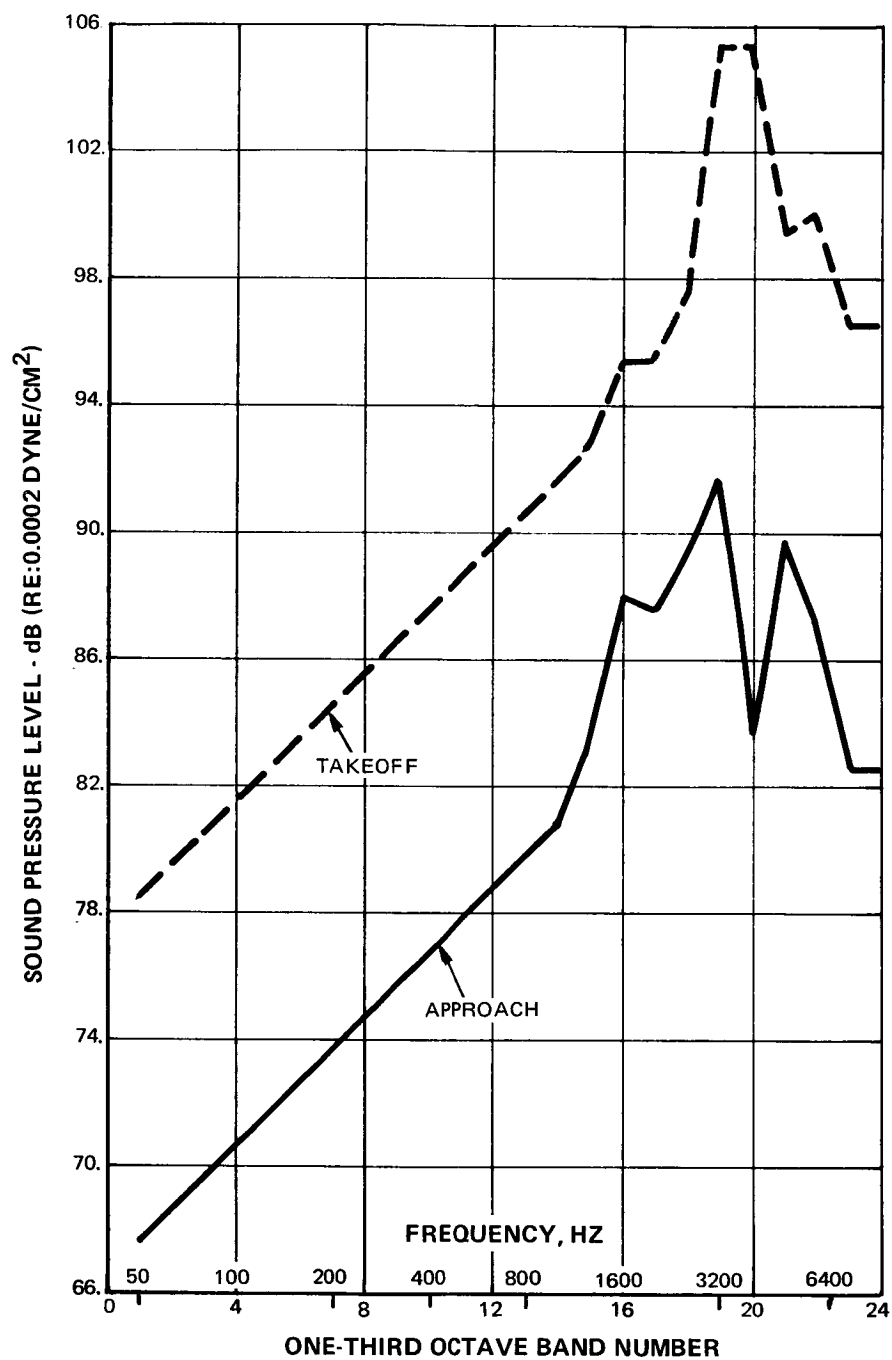


Figure 62 Fan Aft One-Third Octave Spectra – Untreated

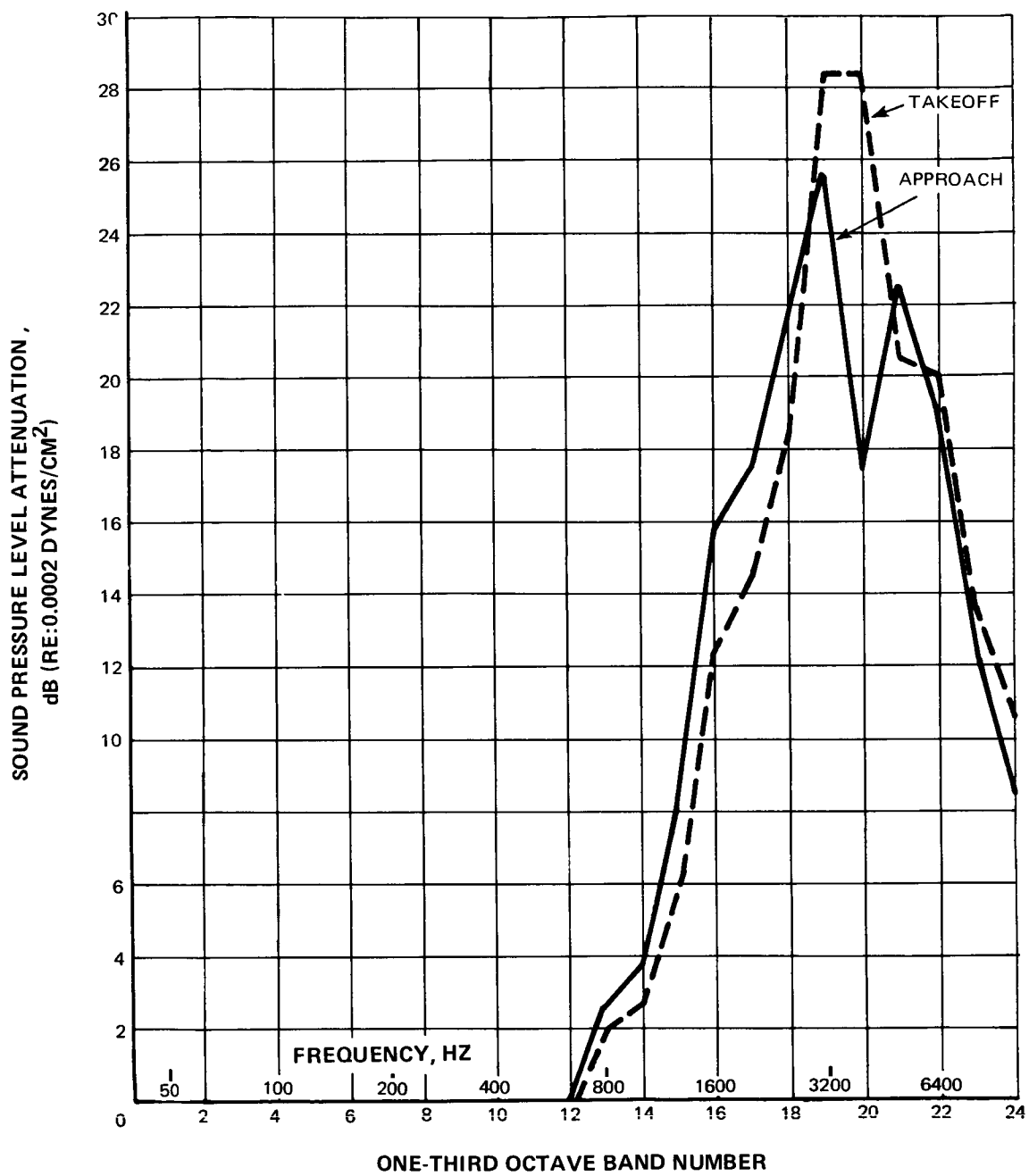


Figure 63 Fan Aft Noise Attenuation Targets

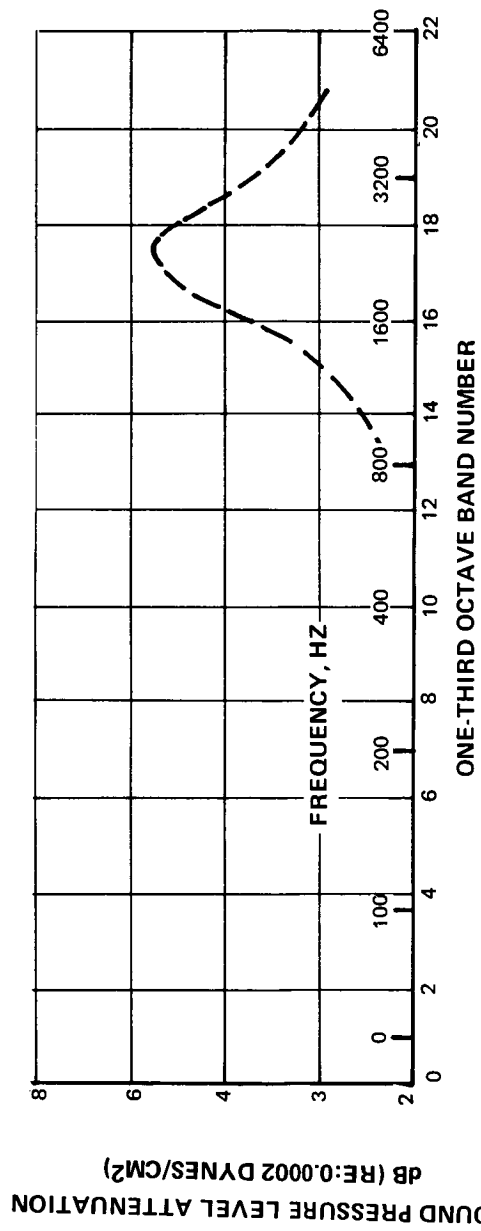


Figure 64 Inlet Estimated Attenuation Due to Wall Treatment — Approach

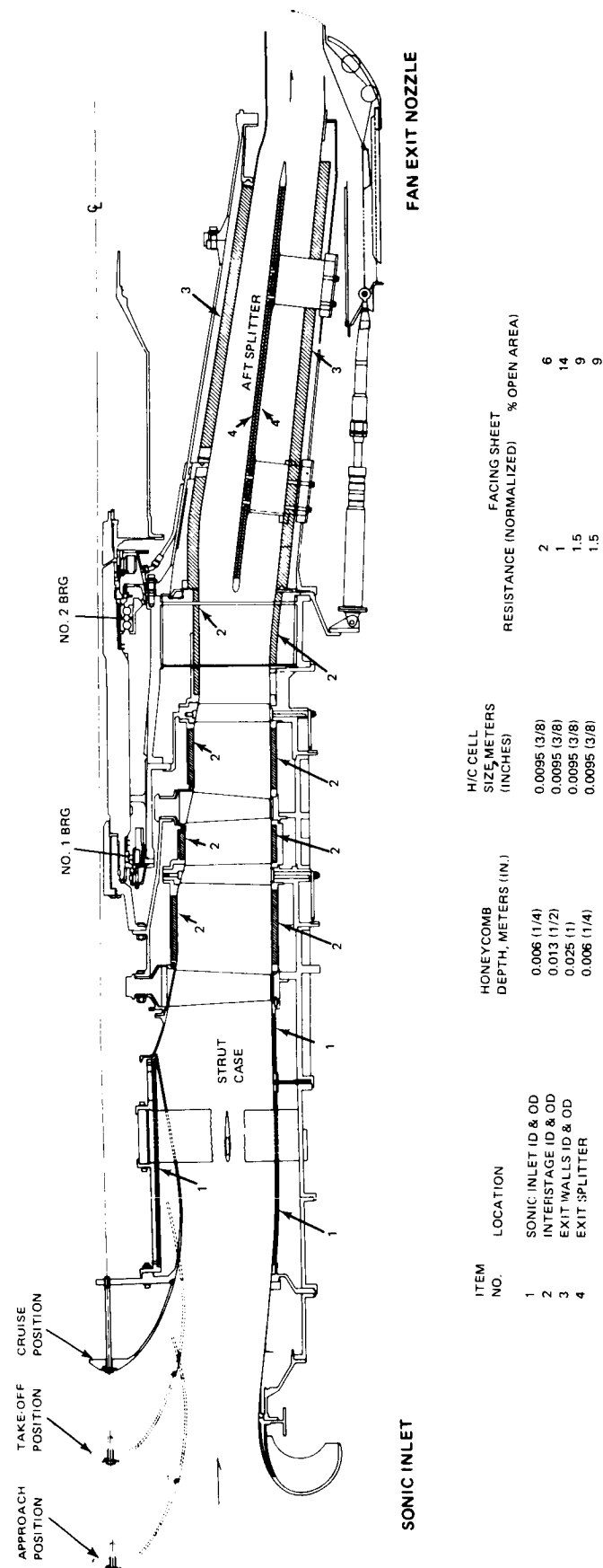


Figure 65 Summary of Fan Acoustic Treatments

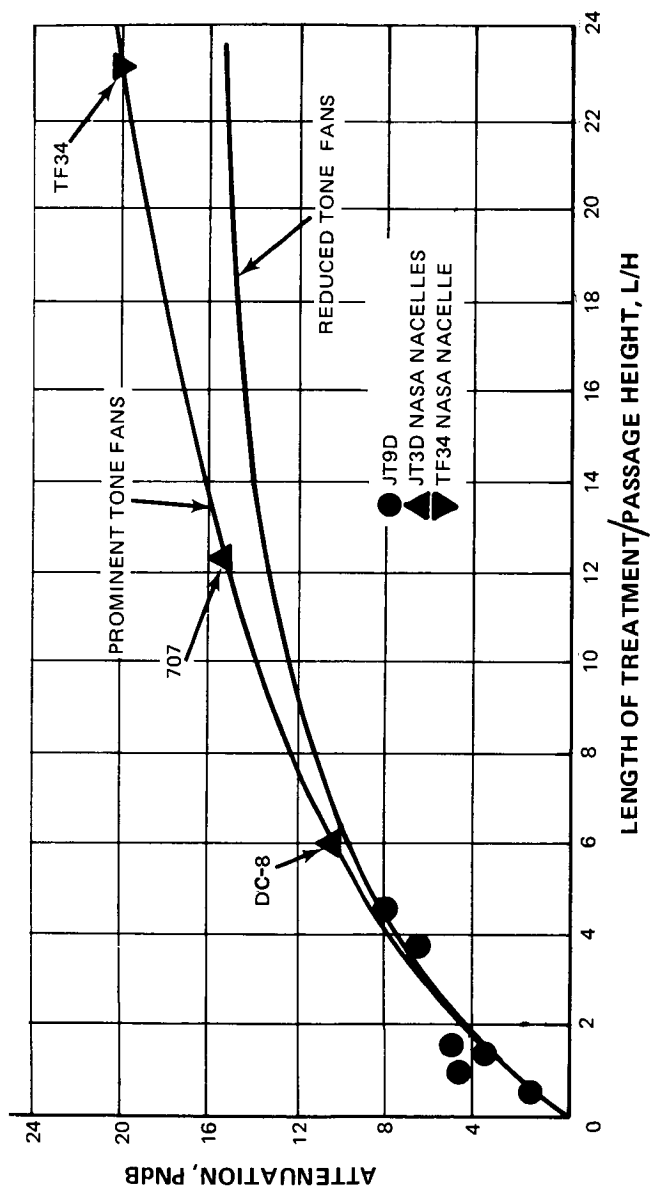


Figure 66 Treatment Attenuation – Fan Discharge Ducts

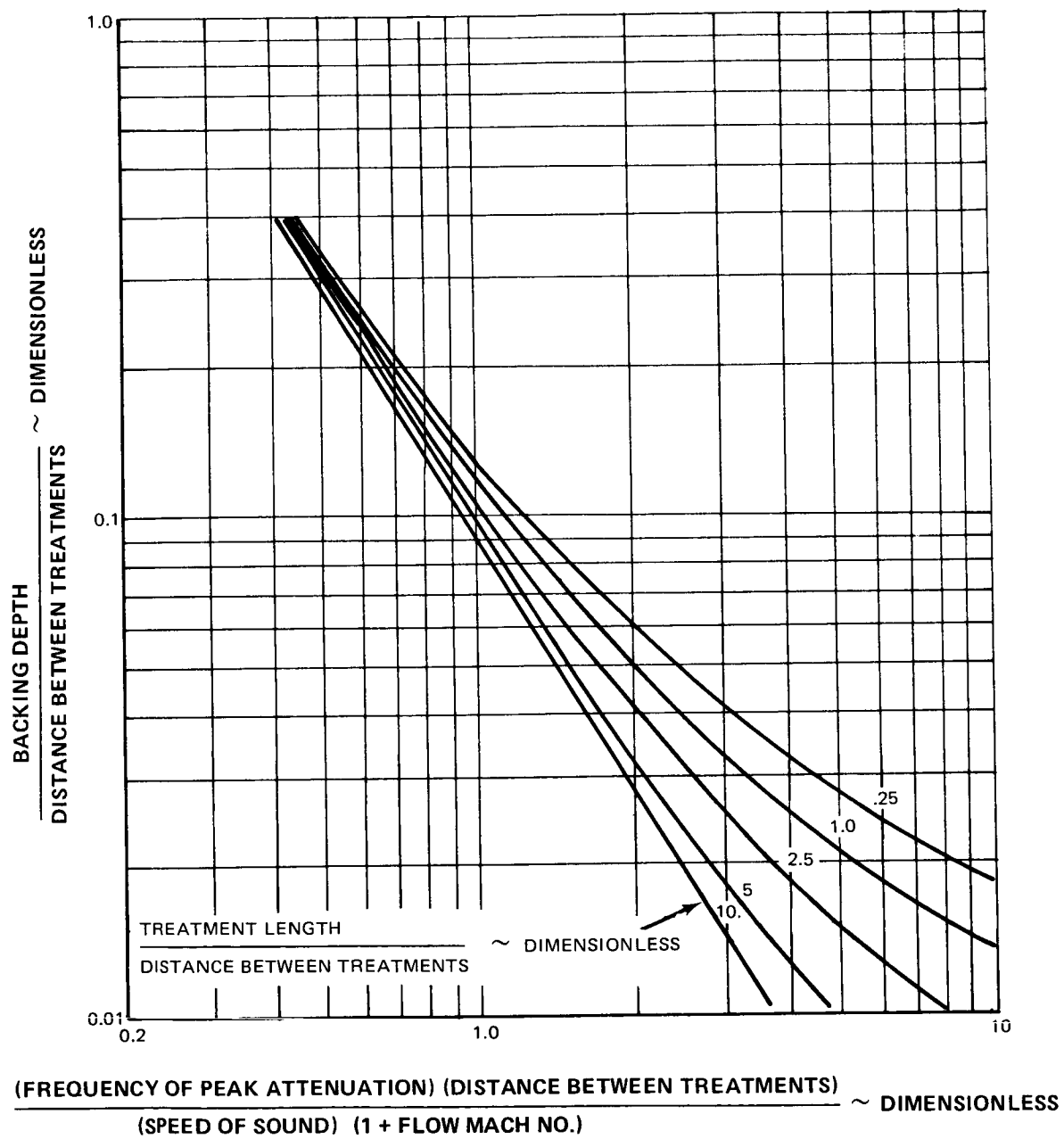


Figure 67 Tuning Curves

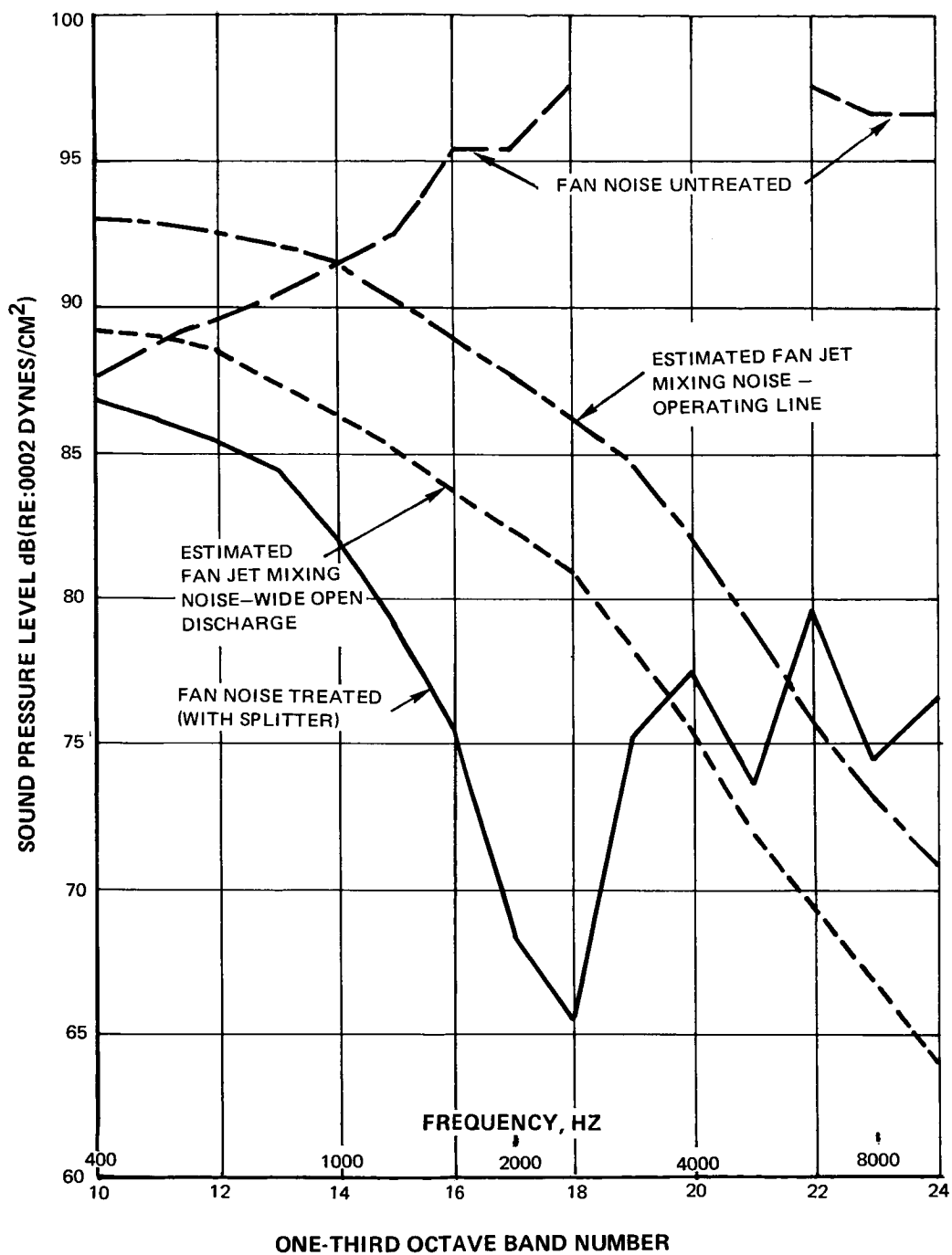


Figure 68 Analytically Predicted Attenuation of Aft Fan Noise at Takeoff

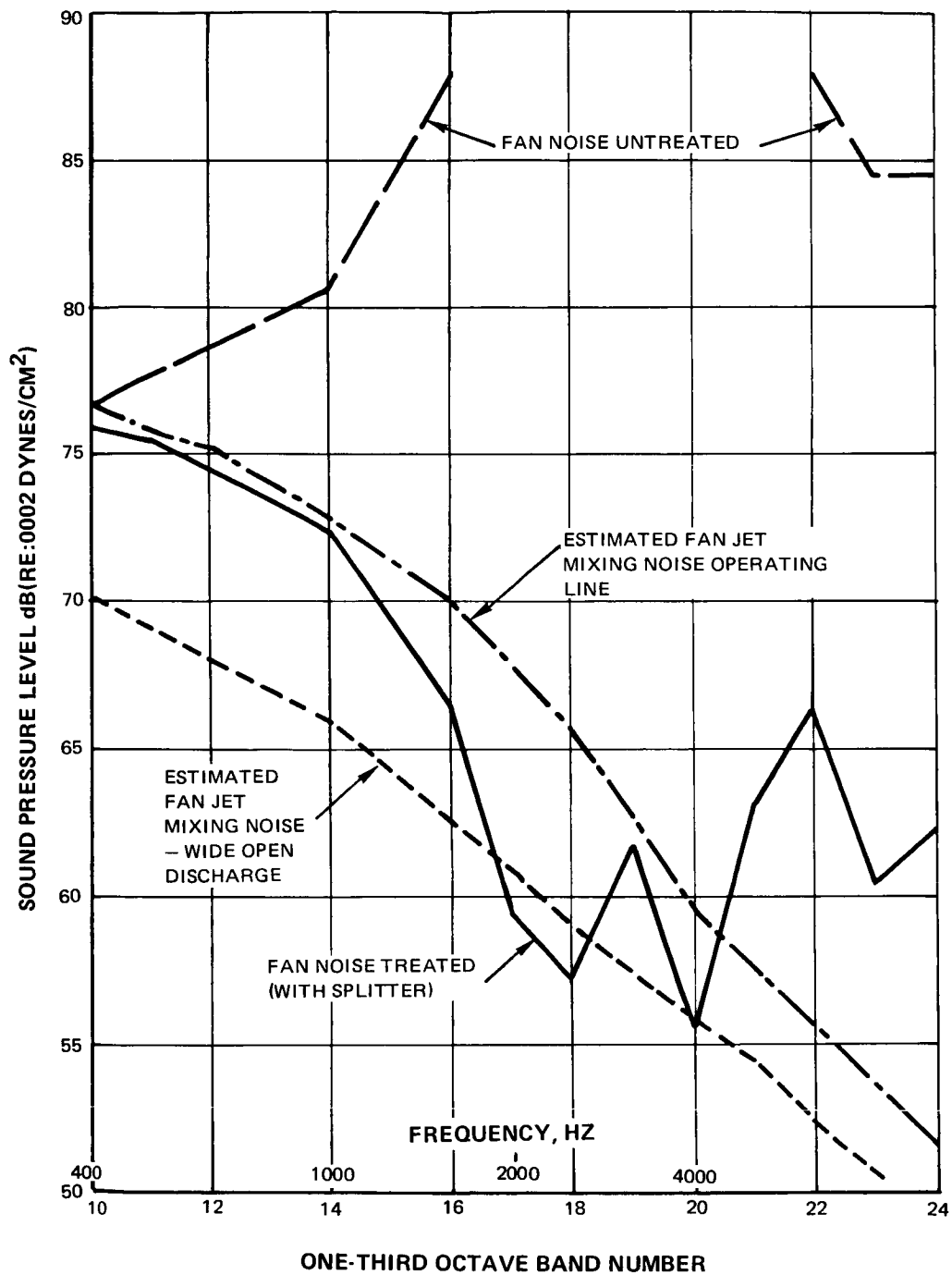


Figure 69 Predicted Jet and Treated Fan Noise Levels – Approach

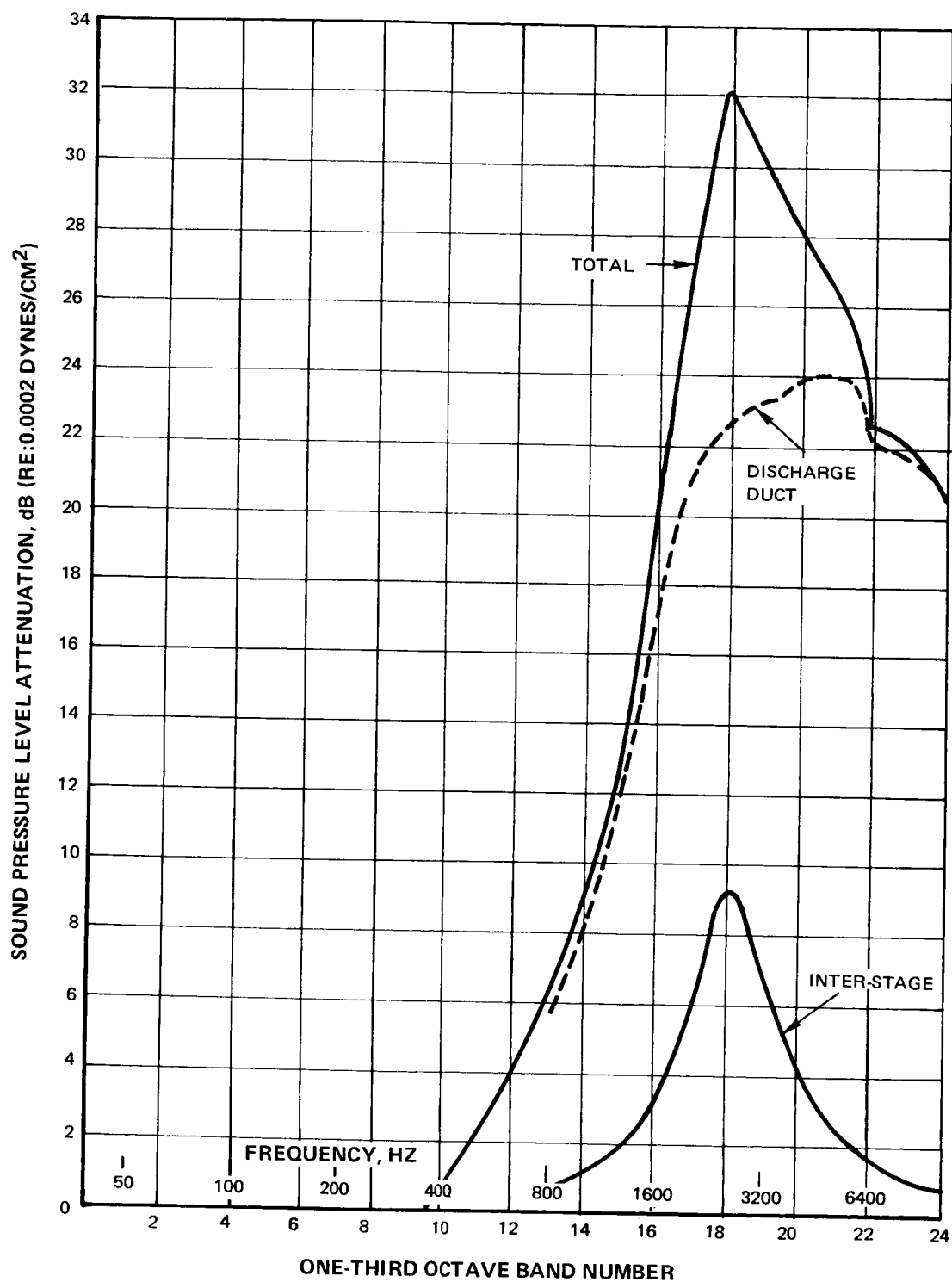


Figure 70 Predicted Jet and Treated Fan Noise Levels – Takeoff

## APPENDIX A

## SYMBOLS AND DEFINITIONS

A	area - meters <sup>2</sup> (feet <sup>2</sup> )
A/A*	ratio of actual-area to critical-area (where local Mach number is 1.0)
a	distance along chord from leading edge of airfoil to point of maximum elevation of airfoil above chord line - meters (inches)
a'	a point on the suction surface of a blade halfway between the leading edge and the point from which a Mach wave emanates that meets the leading edge of the following blade
C	structural damping coefficient - N/m-sec (lbf/in.-sec)
c	Chord (aerodynamic on flow surface) - meters (inches)
D	diffusion factor, $\text{for rotor} = 1 - V'_2/V'_1 + \frac{r_2 V_{\theta 2} - r_1 V_{\theta 1}}{(r_1 + r_2) V' \sigma}$ $\text{for stator} = 1 - V_3/V_2 + \frac{r_2 V_{\theta 2} - r_3 V_{\theta 3}}{(r_2 + r_3) V_2 \sigma}$
d	displacement in the direction normal to the minimum moment of inertia axis - meters (inches)
E	epse, the angle between rays drawn to a conical design surface, one ray to the leading edge of an airfoil section, the second to some other point on the airfoil - degrees; excitations per rotor revolution
G	gravitational force
H	{ boundary layer shape factor passage height
I	moment of inertia about minor axis - meters <sup>4</sup> (inches <sup>4</sup> )
ID	inner diameter of casing - meters (inches)
i	incidence angle, inlet air angle minus blade metal angle - degrees
K	blockage factor; linear spring constant - N/m (lbf/in.)

## SYMBOLS AND DEFINITIONS (Cont'd)

L	length of inlet - meters (inches) length of acoustic treatment
L.E.	leading edge of blade row
M	Mach number
MCA	multiple-circular-arc
N	rotor speed (rpm)
OD	outer diameter of casing - meters (inches)
p	static pressure - $\text{N/m}^2$ (lbf/in. <sup>2</sup> )
P	total or stagnation pressure - $\text{N/m}^2$ (lbf/in. <sup>2</sup> )
PNL	perceived noise level (dB)
RLE	leading edge airfoil radius - meters (inches)
RPM	revolutions per minute
RTE	trailing edge airfoil radius - meters (inches)
r	radius measured from rig centerline - meters (inches); number of rotor blades
R	rotor
r, $\theta$ , z	cylindrical coordinate system, with z axis as rig centerline
S	stator
s	blade spacing - meters (inches); number of stator vanes
SPL	sound pressure level (dB)
T	total temperature - $^{\circ}\text{K}$ ( $^{\circ}\text{R}$ ); torsional spring constant - m-N/rad (in. - lbf/deg)
T. E.	trailing edge of airfoil
t	{ blade maximum thickness - meters (inches) throat
U	rotor speed - m/sec (ft/sec)

## SYMBOLS AND DEFINITIONS (Cont'd)

$V$	air velocity - m/sec (ft/sec)
$W$	weight flow - kg/sec (lbm/sec)
$Z^*$ ratio	$(l/C)_{\text{shroud cross-section}} / (l/C)_{\text{airfoil cross-section above shroud}}$
$z$	axial distance - meters (inches)
$\beta$	absolute air angle $[\cot^{-1} (V_m/V_\theta)]$ - degrees
$\Phi$	vibratory twist deflection - degrees
$\beta'$	relative air angle $[\cot^{-1} (V_m/V'_\theta)]$ - degrees
$\beta^*$	metal angle, on conical surface, between tangent to mean camber line and meridional direction at leading and trailing edge - degrees
$\Delta \beta$	air turning angle - degrees
$\gamma$	blade chord angle, angle between a chord line and axial direction (measured in a plane parallel to z-axis) - degrees; ratio of specific heats for air
$\delta$	ratio of total pressure to standard pressure of $1.01 \times 10^5 \text{ N/m}^2$ ( $2116 \text{ lbf/ft}^2$ )
$\delta^\circ$	deviation angle, exit air angle minus tangent to blade mean camber line at trailing edge - degrees
$\epsilon$	angle between tangent to streamline projected on meridional plane and axial direction - degrees
$\eta$	efficiency (percent)
$\theta$	ratio of total temperature to standard temperature of $518.7^\circ \text{R}$
$\rho$	mass density - $\text{kg/m}^3$ ( $\text{lbm/ft}^3$ )
$\sigma$	solidity, ratio of aerodynamic chord to gap between blades
$\phi$	blade camber angle, difference between blade angles at leading and trailing edges on conical surface, $\beta'^*_1 - \beta'^*_2$ for rotors and $\beta^*_2 - \beta^*_3$ for stators - degrees
$\phi E$	blade camber angle on plane of "unwrapped" conical surface $\beta'^*_1 - \beta'^*_2 - E_{\text{TE}}$ for rotors and $\beta^*_2 - \beta^*_3 - E_{\text{TE}}$ for stators - degrees
$\psi$	amplitude of torsional vibration (radians)

## SYMBOLS AND DEFINITIONS (Cont'd)

$$\bar{\omega} \quad \text{total pressure loss coefficient,} \quad \frac{P'_1 \left[ \frac{T'_2}{T'_1} \right]^{\frac{\gamma}{\gamma-1}} - P'_2}{P'_1 - p_1} \quad (\text{rotors})$$

$$\frac{P_2 - P_3}{P_2 - p_2} \quad (\text{stators})$$

$\omega_b$  bending vibrational frequency (Hz)

$\omega_t$  torsional vibrational frequency (rad/sec)

## Subscripts

ad adiabatic

f front

Ef refers to front camber definitions which include epse angle E

in inlet

LE leading edge

m meridional (velocity); mean camber line (angle)

p profile (loss); polytropic (efficiency)

ss suction surface

st stage

t transition, throat

TE trailing edge

z axial component

$\theta$  tangential component

o plenum chamber

## SYMBOLS AND DEFINITIONS (Cont'd)

1	station into rotor
2	station out of rotor or into stator
3	station out of stator
Superscripts	
'	relative to rotor
*	blade metal (angle); critical, at Mach number unity (area)



# APPENDIX B AERODYNAMIC SUMMARY

TABLE XIV

## IDENTIFICATION OF AERODYNAMIC SUMMARY TABLE HEADINGS

ROTOR																		
SL	EPSI-1 DEGREE	EPSI-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	Vθ-1 FT/SEC	Vθ-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	M-1	M-2	U-1 FT/SEC	U-2 FT/SEC	M'-1	M'-2	V'-1 FT/SEC	V'-2 FT/SEC
*	ε <sub>1</sub>	ε <sub>2</sub>	V <sub>1</sub>	V <sub>2</sub>	V <sub>m1</sub>	V <sub>m2</sub>	V <sub>θ1</sub>	V <sub>θ2</sub>	β <sub>1</sub>	β <sub>2</sub>	M <sub>1</sub>	M <sub>2</sub>	U <sub>1</sub>	U <sub>2</sub>	M' <sub>1</sub>	M' <sub>2</sub>	V' <sub>1</sub>	V' <sub>2</sub>
SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B TOTAL	LOSS-P TOTAL	PO2/ PO1	%EFF-P TOT	%EFF-A TOT	B'-1 DEGREE	B'-2 DEGREE	Vθ'-1 FT/SEC	Vθ'-2 FT/SEC	PO/PO INLET	
*	i <sub>s1</sub>	i <sub>m1</sub>	δ° <sub>2</sub>	Δβ	ρ <sub>1</sub> V <sub>1m1</sub>	ρ <sub>2</sub> V <sub>m2</sub>	D	Ω̄	Ω̄cosβ' <sub>2</sub> 2θ	P <sub>2</sub> P <sub>1</sub>	η <sub>p</sub>	η <sub>ad</sub>	β' <sub>1</sub>	β' <sub>2</sub>	V' <sub>θ1</sub>	V' <sub>θ2</sub>	P <sub>2</sub> P <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>1</sub>	η <sub>ad2</sub>	η <sub>p2</sub>					
										WC1/A1 LBM/SEC SQFT	WC1/A1 LBM/SEC SQFT	WC1/A1 LBM/SEC SQFT	WC1/A1 LBM/SEC SQFT					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					
										T <sub>2</sub> T <sub>0</sub>	P <sub>2</sub> P <sub>0</sub>	η <sub>ad</sub>	η <sub>p</sub>					
										TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %					

TABLE XV  
IDENTIFICATION OF SPANS AND DIAMETERS FOR BLADE ELEMENT DATA

SL	ROTOR 1 INLET		ROTOR 1 EXIT		STATOR 1 INLET		STATOR 1 EXIT	
	DIA. (in.)	SPAN (%)	DIA. (in.)	SPAN (%)	DIA. (in.)	SPAN (%)	DIA. (in.)	SPAN (%)
1	13.16	0.0	14.60	0.0	15.48	0.0	16.46	0.0
2	14.15	5.0	15.52	5.0	16.41	5.3	17.16	4.2
3	15.19	10.3	16.43	10.0	17.30	10.5	17.90	8.8
4	16.23	15.6	17.35	15.0	18.19	15.6	18.67	13.5
5	17.28	20.9	18.26	20.0	19.07	20.6	19.47	18.3
6	19.34	31.3	20.09	30.0	20.81	30.6	21.08	28.1
7	21.38	41.6	21.93	40.0	22.56	40.6	22.75	38.2
8	23.38	51.8	23.76	50.1	24.29	50.6	24.43	48.5
9	25.32	61.6	25.57	59.9	25.99	60.4	26.10	58.6
10	26.30	66.6	26.49	65.0	26.86	65.3	26.96	63.9
11	27.27	71.5	27.41	70.0	27.73	70.3	27.81	69.0
12	29.20	81.2	29.24	80.0	29.45	80.2	29.52	79.4
13	30.15	86.1	30.16	85.0	30.32	85.2	30.38	84.7
14	31.09	90.8	31.07	90.0	31.18	90.1	31.23	89.9
15	32.01	95.5	31.99	95.0	32.04	95.1	32.08	95.0
16	32.90	100.0	32.90	100.0	32.90	100.0	32.90	100.0

SL	ROTOR 2 INLET		ROTOR 2 EXIT		STATOR 2 INLET		STATOR 2 EXIT	
	DIA. (in.)	SPAN (%)	DIA. (in.)	SPAN (%)	DIA. (in.)	SPAN (%)	DIA. (in.)	SPAN (%)
1	16.89	0.0	18.28	0.0	18.55	0.0	19.30	0.0
2	17.66	4.8	18.85	3.9	19.19	4.5	19.82	3.8
3	18.44	9.7	19.45	8.0	19.84	9.0	20.37	7.9
4	19.22	14.6	20.08	12.3	20.50	13.6	20.95	12.1
5	20.01	19.5	20.73	16.8	21.17	18.2	21.55	16.5
6	21.59	29.3	22.08	26.0	22.52	27.6	22.78	25.6
7	23.18	39.3	22.49	35.6	23.90	37.3	24.08	35.2
8	24.78	49.3	24.96	45.7	25.32	47.2	25.43	45.1
9	26.38	59.3	26.45	55.9	26.75	57.1	26.82	55.3
10	27.19	64.4	27.22	61.2	27.49	62.3	27.54	60.6
11	28.01	69.4	28.00	66.5	28.23	67.5	28.27	66.0
12	29.64	79.7	29.59	77.4	29.75	78.0	29.77	77.0
13	30.47	84.8	30.40	82.9	30.52	83.4	30.54	82.7
14	31.29	90.0	31.23	88.6	31.31	88.9	31.33	88.4
15	32.11	95.0	32.07	94.3	32.11	94.5	32.11	94.2
16	32.90	100.0	32.90	100.0	32.90	100.0	32.90	100.0

TABLE XVI

AERODYNAMIC SUMMARY — ROTOR 1  
S1 Units)

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	R-1	R-2	M-1	M-2	U-1	U-2	U-3	U-4	U-5	U-6	U-7	U-8	U-9	U-10	U-11	U-12	U-13	U-14	U-15	U-16	U-17	U-18	U-19	U-20	U-21	U-22	U-23	U-24	U-25	U-26	U-27	U-28	U-29	U-30	U-31	U-32	U-33	U-34	U-35	U-36	U-37	U-38	U-39	U-40	U-41	U-42	U-43	U-44	U-45	U-46	U-47	U-48	U-49	U-50	U-51	U-52	U-53	U-54	U-55	U-56	U-57	U-58	U-59	U-60	U-61	U-62	U-63	U-64	U-65	U-66	U-67	U-68	U-69	U-70	U-71	U-72	U-73	U-74	U-75	U-76	U-77	U-78	U-79	U-80	U-81	U-82	U-83	U-84	U-85	U-86	U-87	U-88	U-89	U-90	U-91	U-92	U-93	U-94	U-95	U-96	U-97	U-98	U-99	U-100	U-101	U-102	U-103	U-104	U-105	U-106	U-107	U-108	U-109	U-110	U-111	U-112	U-113	U-114	U-115	U-116	U-117	U-118	U-119	U-120	U-121	U-122	U-123	U-124	U-125	U-126	U-127	U-128	U-129	U-130	U-131	U-132	U-133	U-134	U-135	U-136	U-137	U-138	U-139	U-140	U-141	U-142	U-143	U-144	U-145	U-146	U-147	U-148	U-149	U-150	U-151	U-152	U-153	U-154	U-155	U-156	U-157	U-158	U-159	U-160	U-161	U-162	U-163	U-164	U-165	U-166	U-167	U-168	U-169	U-170	U-171	U-172	U-173	U-174	U-175	U-176	U-177	U-178	U-179	U-180	U-181	U-182	U-183	U-184	U-185	U-186	U-187	U-188	U-189	U-190	U-191	U-192	U-193	U-194	U-195	U-196	U-197	U-198	U-199	U-200	U-201	U-202	U-203	U-204	U-205	U-206	U-207	U-208	U-209	U-210	U-211	U-212	U-213	U-214	U-215	U-216	U-217	U-218	U-219	U-220	U-221	U-222	U-223	U-224	U-225	U-226	U-227	U-228	U-229	U-230	U-231	U-232	U-233	U-234	U-235	U-236	U-237	U-238	U-239	U-240	U-241	U-242	U-243	U-244	U-245	U-246	U-247	U-248	U-249	U-250	U-251	U-252	U-253	U-254	U-255	U-256	U-257	U-258	U-259	U-260	U-261	U-262	U-263	U-264	U-265	U-266	U-267	U-268	U-269	U-270	U-271	U-272	U-273	U-274	U-275	U-276	U-277	U-278	U-279	U-280	U-281	U-282	U-283	U-284	U-285	U-286	U-287	U-288	U-289	U-290	U-291	U-292	U-293	U-294	U-295	U-296	U-297	U-298	U-299	U-300	U-301	U-302	U-303	U-304	U-305	U-306	U-307	U-308	U-309	U-310	U-311	U-312	U-313	U-314	U-315	U-316	U-317	U-318	U-319	U-320	U-321	U-322	U-323	U-324	U-325	U-326	U-327	U-328	U-329	U-330	U-331	U-332	U-333	U-334	U-335	U-336	U-337	U-338	U-339	U-340	U-341	U-342	U-343	U-344	U-345	U-346	U-347	U-348	U-349	U-350	U-351	U-352	U-353	U-354	U-355	U-356	U-357	U-358	U-359	U-360	U-361	U-362	U-363	U-364	U-365	U-366	U-367	U-368	U-369	U-370	U-371	U-372	U-373	U-374	U-375	U-376	U-377	U-378	U-379	U-380	U-381	U-382	U-383	U-384	U-385	U-386	U-387	U-388	U-389	U-390	U-391	U-392	U-393	U-394	U-395	U-396	U-397	U-398	U-399	U-400	U-401	U-402	U-403	U-404	U-405	U-406	U-407	U-408	U-409	U-410	U-411	U-412	U-413	U-414	U-415	U-416	U-417	U-418	U-419	U-420	U-421	U-422	U-423	U-424	U-425	U-426	U-427	U-428	U-429	U-430	U-431	U-432	U-433	U-434	U-435	U-436	U-437	U-438	U-439	U-440	U-441	U-442	U-443	U-444	U-445	U-446	U-447	U-448	U-449	U-450	U-451	U-452	U-453	U-454	U-455	U-456	U-457	U-458	U-459	U-460	U-461	U-462	U-463	U-464	U-465	U-466	U-467	U-468	U-469	U-470	U-471	U-472	U-473	U-474	U-475	U-476	U-477	U-478	U-479	U-480	U-481	U-482	U-483	U-484	U-485	U-486	U-487	U-488	U-489	U-490	U-491	U-492	U-493	U-494	U-495	U-496	U-497	U-498	U-499	U-500	U-501	U-502	U-503	U-504	U-505	U-506	U-507	U-508	U-509	U-510	U-511	U-512	U-513	U-514	U-515	U-516	U-517	U-518	U-519	U-520	U-521	U-522	U-523	U-524	U-525	U-526	U-527	U-528	U-529	U-530	U-531	U-532	U-533	U-534	U-535	U-536	U-537	U-538	U-539	U-540	U-541	U-542	U-543	U-544	U-545	U-546	U-547	U-548	U-549	U-550	U-551	U-552	U-553	U-554	U-555	U-556	U-557	U-558	U-559	U-560	U-561	U-562	U-563	U-564	U-565	U-566	U-567	U-568	U-569	U-570	U-571	U-572	U-573	U-574	U-575	U-576	U-577	U-578	U-579	U-580	U-581	U-582	U-583	U-584	U-585	U-586	U-587	U-588	U-589	U-590	U-591	U-592	U-593	U-594	U-595	U-596	U-597	U-598	U-599	U-600	U-601	U-602	U-603	U-604	U-605	U-606	U-607	U-608	U-609	U-610	U-611	U-612	U-613	U-614	U-615	U-616	U-617	U-618	U-619	U-620	U-621	U-622	U-623	U-624	U-625	U-626	U-627	U-628	U-629	U-630	U-631	U-632	U-633	U-634	U-635	U-636	U-637	U-638	U-639	U-640	U-641	U-642	U-643	U-644	U-645	U-646	U-647	U-648	U-649	U-650	U-651	U-652	U-653	U-654	U-655	U-656	U-657	U-658	U-659	U-660	U-661	U-662	U-663	U-664	U-665	U-666	U-667	U-668	U-669	U-670	U-671	U-672	U-673	U-674	U-675	U-676	U-677	U-678	U-679	U-680	U-681	U-682	U-683	U-684	U-685	U-686	U-687	U-688	U-689	U-690	U-691	U-692	U-693	U-694	U-695	U-696	U-697	U-698	U-699	U-700	U-701	U-702	U-703	U-704	U-705	U-706	U-707	U-708	U-709	U-710	U-711	U-712	U-713	U-714	U-715	U-716	U-717	U-718	U-719	U-720	U-721	U-722	U-723	U-724	U-725	U-726	U-727	U-728	U-729	U-730	U-731	U-732	U-733	U-734	U-735	U-736	U-737	U-738	U-739	U-740	U-741	U-742	U-743	U-744	U-745	U-746	U-747	U-748	U-749	U-750	U-751	U-752	U-753	U-754	U-755	U-756	U-757	U-758	U-759	U-760	U-761	U-762	U-763	U-764	U-765	U-766	U-767	U-768	U-769	U-770	U-771	U-772	U-773	U-774	U-775	U-776	U-777	U-778	U-779	U-780	U-781	U-782	U-783	U-784	U-785	U-786	U-787	U-788	U-789	U-790	U-791	U-792	U-793	U-794	U-795	U-796	U-797	U-798	U-799	U-800	U-801	U-802	U-803	U-804	U-805	U-806	U-807	U-808	U-809	U-810	U-811	U-812	U-813	U-814	U-815	U-816	U-817	U-818	U-819	U-820	U-821	U-822	U-823	U-824	U-825	U-826	U-827	U-828	U-829	U-830	U-831	U-832	U-833	U-834	U-835	U-836	U-837	U-838	U-839	U-840	U-841	U-842	U-843	U-844	U-845	U-846	U-847	U-848	U-849	U-850	U-851	U-852	U-853	U-854	U-855	U-856	U-857	U-858	U-859	U-860	U-861	U-862	U-863	U-864	U-865	U-866	U-867	U-868	U-869	U-870	U-871	U-872	U-873	U-874	U-875	U-876	U-877	U-878	U-879	U-880	U-881	U-882	U-883	U-884	U-885	U-886	U-887	U-888	U-889	U-890	U-891	U-892	U-893	U-894	U-895	U-896	U-897	U-898	U-899	U-900	U-901	U-902	U-903	U-904	U-905	U-906	U-907	U-908	U-909	U-910	U-911	U-912	U-913	U-914	U-915	U-916	U-917	U-918	U-919	U-920	U-921	U-922	U-923	U-924	U-925	U-926	U-927	U-928	U-929	U-930	U-931	U-932	U-933	U-934	U-935	U-936	U-937	U-938	U-939	U-940	U-941	U-942	U-943	U-944	U-945	U-946	U-947	U-948	U-949	U-950	U-951	U-952	U-953	U-954	U-955	U-956	U-957	U-958	U-959	U-960	U-961	U-962	U-963	U-964	U-965	U-966	U-967	U-968	U-969	U-970	U-971	U-972	U-973	U-974	U-975	U-976	U-977	U-978	U-979	U-980	U-981	U-982	U-983	U-984	U-985	U-986	U-987	U-988	U-989	U-990	U-991	U-992	U-993	U-994	U-995	U-996	U-997	U-998	U-999	U-1000	U-1001	U-1002	U-1003	U-1004	U-1005	U-1006	U-1007	U-1008	U-1009	U-1010	U-1011	U-1012	U-1013	U-1014	U-1015	U-1016	U-1017	U-1018	U-1019	U-1020	U-1021	U-1022	U-1023	U-1024	U-1025	U-1026	U-1027	U-1028	U-1029	U-1030	U-1031	U-1032	U-1033	U-1034	U-1035	U-1036	U-1037	U-1038	U-1039	U-1040	U-1041	U-1042	U-1043	U-1044	U-1045	U-1046	U-1047	U-1048	U-1049	U-1050	U-1051	U-1052	U-1053	U-1054	U-1055	U-1056	U-1057	U-1058	U-1059	U-1060	U-1061	U-1062	U-1063	U-1064	U-1065	U-1066	U-1067	U-1068	U-1069	U-1070	U-1071	U-1072	U-1073	U-1074	U-1075	U-1076	U-1077	U-1078	U-1079	U-1080	U-1081	U-1082	U-1083	U-1084	U-1085	U-1086	U-1087	U-1088	U-1089	U-1090	U-1091	U-1092	U-1093	U-1094	U-1095	U-1096	U-1097	U-1098	U-1099	U-1100	U-1101	U-1102	U-1103	U-1104	U-1105	U-1106	U-1107	U-1108	U-1109	U-1110	U-1111	U-1112	U-1113	U-1114	U-1115	U-1116	U-1117	U-1118	U-1119	U-1120	U-1121	U-1122	U-1123	U-1124	U-1125	U-1126	U-1127	U-1128	U-1129	U-1130	U-1131	U-1132	U-1133	U-1134	U-1135	U-1136	U-1137	U-1138	U-1139	U-1140	U-1141	U-1142	U-1143	U-1144	U-1145	U-1146	U-1147	U-1148	U-1149	U-1150	U-1151	U-1152	U-1153	U-1154	U-1155	U-1156	U-1157	U-1158	U-1159	U-1160	U-1161	U-1162	U-1163	U-1164	U-1165	U-1166	U-1167	U-1168	U-1169	U-1170	U-1171	U-1172	U-1173	U-1174	U-1175	U-1176	U-1177	U-1178	U-1179	U-1180	U-1181	U-1182	U-1183	U-1184	U-1185	U-1186	U-1187	U-1188	U-1189	U-1190	U-1191	U-1192	U-1193	U-1194	U-1195	U-1196	U-1197	U-1198	U-1199	U-1200	U-1201	U-1202	U-1203	U-1204	
----	--------	--------	-----	-----	------	------	------	------	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--

TABLE XVI (Cont'd)

AERODYNAMIC SUMMARY – ROTOR 1  
(English Units)

SL	EPIS-1	EPIS-2	V-1	V-2	VM-1	VM-2	V9-1	V9-2	P-1	R-2	M-1	M-2	U-1	U-2	O <sub>1</sub> POINT NO.	0	M-1	M-2	V-1	V-2
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC			FT/SEC	FT/SEC	FT/SEC	FT/SEC
1	12.666	11.135	703.6	1060.6	703.6	607.4	0.0	869.4	0.0	55.0	0.6567	0.9056	480.4	533.0	0.7952	0.6322	851.9	694.4	675.6	694.4
2	12.175	9.481	707.7	1001.2	707.7	645.7	0.0	765.2	0.0	49.7	0.6609	0.9068	516.6	566.4	0.8183	0.6119	876.2	675.6	675.6	675.6
3	11.371	8.143	711.6	952.6	711.6	650.6	0.0	695.8	0.0	46.8	0.6648	0.8584	554.3	599.8	0.8847	0.5926	902.0	657.6	645.5	645.5
4	10.424	7.044	715.2	911.6	715.2	646.5	0.0	642.7	0.0	44.1	0.6685	0.8177	592.5	633.2	0.8681	0.5800	928.7	645.5	645.5	645.5
5	9.426	6.148	718.3	876.8	718.3	636.9	0.0	602.6	0.0	43.3	0.6717	0.7833	630.8	666.6	0.8939	0.5718	955.9	645.5	645.5	645.5
6	8.424	5.250	722.7	837.9	722.7	617.9	0.0	537.9	0.0	41.0	0.6762	0.7271	706.1	733.3	0.9453	0.5751	1010.4	648.1	648.1	648.1
7	7.424	4.353	725.1	795.5	725.1	600.8	0.0	490.4	0.0	39.2	0.6786	0.6847	780.5	807.4	0.9970	0.5969	1085.3	676.0	676.0	676.0
8	6.424	3.456	728.7	742.0	728.7	588.2	0.0	442.3	0.0	37.5	0.6792	0.6526	853.4	867.3	1.0485	0.6331	1120.2	719.9	719.9	719.9
9	5.424	2.559	732.0	694.5	732.0	539.2	0.0	423.8	0.0	36.2	0.6785	0.6291	924.3	933.4	1.0994	0.6763	1174.7	771.5	771.5	771.5
10	4.424	1.662	735.4	646.8	735.4	491.5	0.0	411.2	0.0	35.5	0.6781	0.6191	960.1	967.1	1.1257	0.7003	1202.9	800.1	800.1	800.1
11	3.424	0.765	738.8	599.1	738.8	444.8	0.0	400.5	0.0	35.0	0.6779	0.6105	995.6	1000.5	1.1522	0.7247	1231.2	829.1	829.1	829.1
12	2.424	-0.132	742.2	551.4	742.2	397.1	0.0	387.1	0.0	34.4	0.6767	0.5963	1065.8	1067.3	1.2052	0.7701	1286.0	884.0	884.0	884.0
13	1.424	-0.831	745.6	503.7	745.6	349.4	0.0	373.9	0.0	34.4	0.6757	0.5906	1100.7	1100.9	1.2317	0.7912	1316.5	910.0	910.0	910.0
14	0.424	-1.529	749.0	456.0	749.0	301.7	0.0	360.3	0.0	35.9	0.6746	0.5875	1134.5	1134.3	1.2579	0.7945	1344.7	918.6	918.6	918.6
15	-0.576	-2.227	752.4	408.3	752.4	254.0	0.0	346.6	0.0	37.7	0.6737	0.5841	1168.5	1167.7	1.2839	0.7966	1372.6	924.8	924.8	924.8
16	-1.274	-2.925	755.8	360.6	755.8	206.5	0.0	332.9	0.0	40.7	0.6732	0.5853	1201.0	1201.0	1.3095	0.7830	1400.2	915.4	915.4	915.4

TABLE XVII

AERODYNAMIC SUMMARY — STATOR 1  
(SI Units)

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	R-1	R-2	M-1	M-2	0, SPEED CODE	TO/TO	PO/PO	STAGE	TO/PO	TO2/ TO1
	RADIAN	RADIAN	M/SEC	M/SEC	M/SEC	M/SEC	M/SEC	M/SEC	RADIAN	RADIAN				INLET	INLET		INLET	T01
1	0.2738	0.1833	287.0	182.8	141.2	181.3	249.9	23.5	1.0546	0.1255	0.8410	0.5145	1.4181	1.4187	1.4181	1.4181	1.4181	1.4181
2	0.2037	0.1404	275.7	181.0	165.3	179.5	220.6	23.4	0.9265	0.1279	0.8071	0.5115	1.4356	1.4391	1.4356	1.4356	1.4356	1.4391
3	0.1603	0.1141	267.3	181.0	175.6	179.4	201.4	23.5	0.8526	0.1291	0.7816	0.5125	1.4517	1.4340	1.4517	1.4517	1.4340	1.4340
4	0.1289	0.0950	260.4	179.9	181.5	178.3	186.8	23.4	0.7996	0.1298	0.7604	0.5100	1.4603	1.4306	1.4603	1.4603	1.4306	1.4306
5	0.1065	0.0813	254.6	179.2	184.1	177.7	175.9	23.3	0.7626	0.1301	0.7420	0.5084	1.4665	1.4290	1.4665	1.4665	1.4290	1.4290
6	0.0724	0.0612	244.1	177.2	185.9	175.7	158.2	23.1	0.7053	0.1306	0.7091	0.5030	1.4700	1.4266	1.4700	1.4700	1.4266	1.4266
7	0.0507	0.0478	235.4	175.8	185.3	174.3	145.3	22.9	0.6651	0.1307	0.6817	0.4989	1.4689	1.4250	1.4689	1.4689	1.4250	1.4250
8	0.0367	0.0380	228.3	174.9	184.2	173.4	134.9	22.8	0.6321	0.1308	0.6591	0.4964	1.4670	1.4259	1.4670	1.4670	1.4259	1.4259
9	0.0269	0.0304	222.8	174.6	183.0	173.1	127.1	22.8	0.6068	0.1309	0.6417	0.4952	1.4657	1.4270	1.4657	1.4657	1.4270	1.4270
10	0.0232	0.0270	220.4	174.2	182.4	172.7	123.6	22.7	0.5954	0.1309	0.6339	0.4938	1.4643	1.4277	1.4643	1.4643	1.4277	1.4277
11	0.0200	0.0238	218.3	173.8	181.9	172.4	120.7	22.7	0.5858	0.1309	0.6272	0.4925	1.4633	1.4286	1.4633	1.4633	1.4286	1.4286
12	0.0143	0.0177	214.9	172.6	180.2	171.1	117.1	22.5	0.5762	0.1309	0.6157	0.4879	1.4598	1.4326	1.4598	1.4598	1.4326	1.4326
13	0.0118	0.0148	213.6	171.4	179.2	170.0	116.4	22.4	0.5761	0.1309	0.6108	0.4838	1.4567	1.4357	1.4567	1.4567	1.4357	1.4357
14	0.0090	0.0112	213.7	171.6	176.2	170.1	121.0	22.4	0.6017	0.1309	0.6083	0.4821	1.4560	1.4450	1.4560	1.4560	1.4450	1.4450
15	0.0053	0.0065	213.8	170.4	172.6	169.4	126.1	22.3	0.6311	0.1309	0.6056	0.4779	1.4530	1.4554	1.4530	1.4530	1.4554	1.4554
16	0.0000	0.0000	215.8	173.0	167.5	171.5	136.1	22.6	0.6824	0.1309	0.6071	0.4804	1.4556	1.4721	1.4556	1.4556	1.4721	1.4721

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-8	LOSS-P	P02/	%EFF-P	%EFF-A	%EFF-P	%EFF-A	%EFF-P	%EFF-A
	RADIAN	RADIAN	RADIAN	RADIAN				TOTAL	TOTAL	P01	STAGE-ST	TOT-INLET	TOT-INLET	TOT-STG	TOT-STG	
1	0.0212	0.0968	0.2807	0.9291	33.79	49.37	0.5152	0.1892	0.0376	0.9299	74.27	70.57	71.98	70.57	71.98	
2	0.0096	0.0718	0.2311	0.7986	40.71	49.98	0.4883	0.1556	0.0323	0.9457	77.69	78.25	79.33	78.25	79.33	
3	0.0067	0.0796	0.1879	0.7236	44.06	50.72	0.4644	0.1182	0.0256	0.9607	82.14	83.89	84.71	83.89	84.71	
4	0.0160	0.0742	0.1672	0.6698	46.11	50.91	0.4487	0.0934	0.0211	0.9703	85.31	87.46	88.12	87.46	88.12	
5	0.0323	0.0612	0.1586	0.6325	47.26	51.06	0.4347	0.0730	0.0171	0.9777	88.05	89.66	90.20	89.66	90.20	
6	0.0562	0.0436	0.1457	0.5747	48.56	50.85	0.4122	0.0483	0.0122	0.9862	91.45	91.91	92.34	91.91	92.34	
7	0.0807	0.0252	0.1395	0.5344	49.05	50.52	0.3926	0.0372	0.0101	0.9900	92.87	92.18	92.59	92.18	92.59	
8	0.1051	0.0066	0.1341	0.5013	49.29	50.28	0.3739	0.0321	0.0093	0.9919	93.32	91.89	92.32	91.89	92.32	
9	0.1285	0.0110	0.1278	0.4760	49.58	50.12	0.3584	0.0316	0.0097	0.9924	92.91	90.91	91.39	90.91	91.39	
10	0.1407	0.0202	0.1257	0.4646	49.89	49.96	0.3527	0.0334	0.0105	0.9921	92.26	90.21	90.72	90.21	90.72	
11	0.1524	0.0290	0.1241	0.4549	49.38	49.81	0.3480	0.0359	0.0116	0.9917	91.47	89.34	89.89	89.34	89.89	
12	0.1744	0.0458	0.1231	0.4453	49.08	49.26	0.3465	0.0467	0.0159	0.9895	88.51	86.09	86.81	86.09	86.81	
13	0.1890	0.0577	0.1249	0.4452	48.79	48.79	0.3510	0.0572	0.0199	0.9873	85.94	83.64	84.49	83.64	84.49	
14	0.1989	0.0656	0.1347	0.4708	47.75	48.44	0.3622	0.0681	0.0243	0.9849	83.18	78.15	79.28	78.15	79.28	
15	0.2108	0.0760	0.1711	0.5002	46.51	47.82	0.3785	0.0867	0.0316	0.9810	78.86	72.50	73.91	72.50	73.91	
16	0.2180	0.0821	0.2321	0.5515	44.73	47.74	0.3960	0.1050	0.0391	0.9769	74.18	65.78	67.53	65.78	67.53	

NCORR	WCORR	TO/TO	PO/PO	EFF-AD	EFF-P	EFF-AD	EFF-P
RAD/SEC	KG/SEC	INLET	INLET	%	%	%	%
875.19	96.372	1.1336	1.4611	85.66	86.41	1.1336	85.66
							261.44

TABLE XVII (Cont'd)

AERODYNAMIC SUMMARY - STATOR 1  
(English Units)

SL	EPI-1	EPI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	O <sub>2</sub> SPEED CODE		PO/PO	TO/TO	PO/PO	TOT-1	TOT-2	TOT-3	TOT-4	TOT-5	TOT-6	TOT-7	TOT-8	TOT-9	TOT-10	TOT-11	TOT-12	TOT-13	TOT-14	TOT-15	TOT-16	TOT-17	TOT-18	TOT-19	TOT-20	TOT-21	TOT-22	TOT-23	TOT-24	TOT-25	TOT-26	TOT-27	TOT-28	TOT-29	TOT-30	TOT-31	TOT-32	TOT-33	TOT-34	TOT-35	TOT-36	TOT-37	TOT-38	TOT-39	TOT-40	TOT-41	TOT-42	TOT-43	TOT-44	TOT-45	TOT-46	TOT-47	TOT-48	TOT-49	TOT-50	TOT-51	TOT-52	TOT-53	TOT-54	TOT-55	TOT-56	TOT-57	TOT-58	TOT-59	TOT-60	TOT-61	TOT-62	TOT-63	TOT-64	TOT-65	TOT-66	TOT-67	TOT-68	TOT-69	TOT-70	TOT-71	TOT-72	TOT-73	TOT-74	TOT-75	TOT-76	TOT-77	TOT-78	TOT-79	TOT-80	TOT-81	TOT-82	TOT-83	TOT-84	TOT-85	TOT-86	TOT-87	TOT-88	TOT-89	TOT-90	TOT-91	TOT-92	TOT-93	TOT-94	TOT-95	TOT-96	TOT-97	TOT-98	TOT-99	TOT-100	TOT-101	TOT-102	TOT-103	TOT-104	TOT-105	TOT-106	TOT-107	TOT-108	TOT-109	TOT-110	TOT-111	TOT-112	TOT-113	TOT-114	TOT-115	TOT-116	TOT-117	TOT-118	TOT-119	TOT-120	TOT-121	TOT-122	TOT-123	TOT-124	TOT-125	TOT-126	TOT-127	TOT-128	TOT-129	TOT-130	TOT-131	TOT-132	TOT-133	TOT-134	TOT-135	TOT-136	TOT-137	TOT-138	TOT-139	TOT-140	TOT-141	TOT-142	TOT-143	TOT-144	TOT-145	TOT-146	TOT-147	TOT-148	TOT-149	TOT-150	TOT-151	TOT-152	TOT-153	TOT-154	TOT-155	TOT-156	TOT-157	TOT-158	TOT-159	TOT-160	TOT-161	TOT-162	TOT-163	TOT-164	TOT-165	TOT-166	TOT-167	TOT-168	TOT-169	TOT-170	TOT-171	TOT-172	TOT-173	TOT-174	TOT-175	TOT-176	TOT-177	TOT-178	TOT-179	TOT-180	TOT-181	TOT-182	TOT-183	TOT-184	TOT-185	TOT-186	TOT-187	TOT-188	TOT-189	TOT-190	TOT-191	TOT-192	TOT-193	TOT-194	TOT-195	TOT-196	TOT-197	TOT-198	TOT-199	TOT-200	TOT-201	TOT-202	TOT-203	TOT-204	TOT-205	TOT-206	TOT-207	TOT-208	TOT-209	TOT-210	TOT-211	TOT-212	TOT-213	TOT-214	TOT-215	TOT-216	TOT-217	TOT-218	TOT-219	TOT-220	TOT-221	TOT-222	TOT-223	TOT-224	TOT-225	TOT-226	TOT-227	TOT-228	TOT-229	TOT-230	TOT-231	TOT-232	TOT-233	TOT-234	TOT-235	TOT-236	TOT-237	TOT-238	TOT-239	TOT-240	TOT-241	TOT-242	TOT-243	TOT-244	TOT-245	TOT-246	TOT-247	TOT-248	TOT-249	TOT-250	TOT-251	TOT-252	TOT-253	TOT-254	TOT-255	TOT-256	TOT-257	TOT-258	TOT-259	TOT-260	TOT-261	TOT-262	TOT-263	TOT-264	TOT-265	TOT-266	TOT-267	TOT-268	TOT-269	TOT-270	TOT-271	TOT-272	TOT-273	TOT-274	TOT-275	TOT-276	TOT-277	TOT-278	TOT-279	TOT-280	TOT-281	TOT-282	TOT-283	TOT-284	TOT-285	TOT-286	TOT-287	TOT-288	TOT-289	TOT-290	TOT-291	TOT-292	TOT-293	TOT-294	TOT-295	TOT-296	TOT-297	TOT-298	TOT-299	TOT-300	TOT-301	TOT-302	TOT-303	TOT-304	TOT-305	TOT-306	TOT-307	TOT-308	TOT-309	TOT-310	TOT-311	TOT-312	TOT-313	TOT-314	TOT-315	TOT-316	TOT-317	TOT-318	TOT-319	TOT-320	TOT-321	TOT-322	TOT-323	TOT-324	TOT-325	TOT-326	TOT-327	TOT-328	TOT-329	TOT-330	TOT-331	TOT-332	TOT-333	TOT-334	TOT-335	TOT-336	TOT-337	TOT-338	TOT-339	TOT-340	TOT-341	TOT-342	TOT-343	TOT-344	TOT-345	TOT-346	TOT-347	TOT-348	TOT-349	TOT-350	TOT-351	TOT-352	TOT-353	TOT-354	TOT-355	TOT-356	TOT-357	TOT-358	TOT-359	TOT-360	TOT-361	TOT-362	TOT-363	TOT-364	TOT-365	TOT-366	TOT-367	TOT-368	TOT-369	TOT-370	TOT-371	TOT-372	TOT-373	TOT-374	TOT-375	TOT-376	TOT-377	TOT-378	TOT-379	TOT-380	TOT-381	TOT-382	TOT-383	TOT-384	TOT-385	TOT-386	TOT-387	TOT-388	TOT-389	TOT-390	TOT-391	TOT-392	TOT-393	TOT-394	TOT-395	TOT-396	TOT-397	TOT-398	TOT-399	TOT-400	TOT-401	TOT-402	TOT-403	TOT-404	TOT-405	TOT-406	TOT-407	TOT-408	TOT-409	TOT-410	TOT-411	TOT-412	TOT-413	TOT-414	TOT-415	TOT-416	TOT-417	TOT-418	TOT-419	TOT-420	TOT-421	TOT-422	TOT-423	TOT-424	TOT-425	TOT-426	TOT-427	TOT-428	TOT-429	TOT-430	TOT-431	TOT-432	TOT-433	TOT-434	TOT-435	TOT-436	TOT-437	TOT-438	TOT-439	TOT-440	TOT-441	TOT-442	TOT-443	TOT-444	TOT-445	TOT-446	TOT-447	TOT-448	TOT-449	TOT-450	TOT-451	TOT-452	TOT-453	TOT-454	TOT-455	TOT-456	TOT-457	TOT-458	TOT-459	TOT-460	TOT-461	TOT-462	TOT-463	TOT-464	TOT-465	TOT-466	TOT-467	TOT-468	TOT-469	TOT-470	TOT-471	TOT-472	TOT-473	TOT-474	TOT-475	TOT-476	TOT-477	TOT-478	TOT-479	TOT-480	TOT-481	TOT-482	TOT-483	TOT-484	TOT-485	TOT-486	TOT-487	TOT-488	TOT-489	TOT-490	TOT-491	TOT-492	TOT-493	TOT-494	TOT-495	TOT-496	TOT-497	TOT-498	TOT-499	TOT-500	TOT-501	TOT-502	TOT-503	TOT-504	TOT-505	TOT-506	TOT-507	TOT-508	TOT-509	TOT-510	TOT-511	TOT-512	TOT-513	TOT-514	TOT-515	TOT-516	TOT-517	TOT-518	TOT-519	TOT-520	TOT-521	TOT-522	TOT-523	TOT-524	TOT-525	TOT-526	TOT-527	TOT-528	TOT-529	TOT-530	TOT-531	TOT-532	TOT-533	TOT-534	TOT-535	TOT-536	TOT-537	TOT-538	TOT-539	TOT-540	TOT-541	TOT-542	TOT-543	TOT-544	TOT-545	TOT-546	TOT-547	TOT-548	TOT-549	TOT-550	TOT-551	TOT-552	TOT-553	TOT-554	TOT-555	TOT-556	TOT-557	TOT-558	TOT-559	TOT-560	TOT-561	TOT-562	TOT-563	TOT-564	TOT-565	TOT-566	TOT-567	TOT-568	TOT-569	TOT-570	TOT-571	TOT-572	TOT-573	TOT-574	TOT-575	TOT-576	TOT-577	TOT-578	TOT-579	TOT-580	TOT-581	TOT-582	TOT-583	TOT-584	TOT-585	TOT-586	TOT-587	TOT-588	TOT-589	TOT-590	TOT-591	TOT-592	TOT-593	TOT-594	TOT-595	TOT-596	TOT-597	TOT-598	TOT-599	TOT-600	TOT-601	TOT-602	TOT-603	TOT-604	TOT-605	TOT-606	TOT-607	TOT-608	TOT-609	TOT-610	TOT-611	TOT-612	TOT-613	TOT-614	TOT-615	TOT-616	TOT-617	TOT-618	TOT-619	TOT-620	TOT-621	TOT-622	TOT-623	TOT-624	TOT-625	TOT-626	TOT-627	TOT-628	TOT-629	TOT-630	TOT-631	TOT-632	TOT-633	TOT-634	TOT-635	TOT-636	TOT-637	TOT-638	TOT-639	TOT-640	TOT-641	TOT-642	TOT-643	TOT-644	TOT-645	TOT-646	TOT-647	TOT-648	TOT-649	TOT-650	TOT-651	TOT-652	TOT-653	TOT-654	TOT-655	TOT-656	TOT-657	TOT-658	TOT-659	TOT-660	TOT-661	TOT-662	TOT-663	TOT-664	TOT-665	TOT-666	TOT-667	TOT-668	TOT-669	TOT-670	TOT-671	TOT-672	TOT-673	TOT-674	TOT-675	TOT-676	TOT-677	TOT-678	TOT-679	TOT-680	TOT-681	TOT-682	TOT-683	TOT-684	TOT-685	TOT-686	TOT-687	TOT-688	TOT-689	TOT-690	TOT-691	TOT-692	TOT-693	TOT-694	TOT-695	TOT-696	TOT-697	TOT-698	TOT-699	TOT-700	TOT-701	TOT-702	TOT-703	TOT-704	TOT-705	TOT-706	TOT-707	TOT-708	TOT-709	TOT-710	TOT-711	TOT-712	TOT-713	TOT-714	TOT-715	TOT-716	TOT-717	TOT-718	TOT-719	TOT-720	TOT-721	TOT-722	TOT-723	TOT-724	TOT-725	TOT-726	TOT-727	TOT-728	TOT-729	TOT-730	TOT-731	TOT-732	TOT-733	TOT-734	TOT-735	TOT-736	TOT-737	TOT-738	TOT-739	TOT-740	TOT-741	TOT-742	TOT-743	TOT-744	TOT-745	TOT-746	TOT-747	TOT-748	TOT-749	TOT-750	TOT-751	TOT-752	TOT-753	TOT-754	TOT-755	TOT-756	TOT-757	TOT-758	TOT-759	TOT-760	TOT-761	TOT-762	TOT-763	TOT-764	TOT-765	TOT-766	TOT-767	TOT-768	TOT-769	TOT-770	TOT-771	TOT-772	TOT-773	TOT-774	TOT-775	TOT-776	TOT-777	TOT-778	TOT-779	TOT-780	TOT-781	TOT-782	TOT-783	TOT-784	TOT-785	TOT-786	TOT-787	TOT-788	TOT-789	TOT-790	TOT-791	TOT-792	TOT-793	TOT-794	TOT-795	TOT-796	TOT-797	TOT-798	TOT-799	TOT-800	TOT-801	TOT-802	TOT-803	TOT-804	TOT-805	TOT-806	TOT-807	TOT-808	TOT-809	TOT-810	TOT-811	TOT-812	TOT-813	TOT-814	TOT-815	TOT-816	TOT-817	TOT-818	TOT-819	TOT-820	TOT-821	TOT-822	TOT-823	TOT-824	TOT-825	TOT-826	TOT-827	TOT-828	TOT-829	TOT-830	TOT-831	TOT-832	TOT-833	TOT-834	TOT-835	TOT-836	TOT-837	TOT-838	TOT-839	TOT-840	TOT-841	TOT-842	TOT-843	TOT-844	TOT-845	TOT-846	TOT-847	TOT-848	TOT-849	TOT-850	TOT-851	TOT-852	TOT-853	TOT-854	TOT-855	TOT-856	TOT-857	TOT-858	TOT-859	TOT-860	TOT-861	TOT-862	TOT-863	TOT-864	TOT-865	TOT-866	TOT-867	TOT-868	TOT-869	TOT-870	TOT-871	TOT-872	TOT-873	TOT-874	TOT-875	TOT-876	TOT-877	TOT-878	TOT-879	TOT-880	TOT-881	TOT-882	TOT-883	TOT-884	TOT-885	TOT-886	TOT-887	TOT-888	TOT-889	TOT-890	TOT-891	TOT-892	TOT-893	TOT-894	TOT-895	TOT-896	TOT-897	TOT-898	TOT-899	TOT-900	TOT-901	TOT-902	TOT-903	TOT-904	TOT-905	TOT-906	TOT-907	TOT-908	TOT-909	TOT-910	TOT-911	TOT-912	TOT-913	TOT-914	TOT-915	TOT-916	TOT-917	TOT-918	TOT-919	TOT-920	TOT-921	TOT-922	TOT-923	TOT-924	TOT-925	TOT-926	TOT-927	TOT-928	TOT-929	TOT-930	TOT-931	TOT-932	TOT-933	TOT-934	TOT-935	TOT-936	TOT-937	TOT-938	TOT-939	TOT-940	TOT-941	TOT-942	TOT-943	TOT-944	TOT-945	TOT-946	TOT-947	TOT-948	TOT-949	TOT-950	TOT-951	TOT-952	TOT-953	TOT-954	TOT-955	TOT-956	TOT-957	TOT-958	TOT-959	TOT-960	TOT-961	TOT-962	TOT-963	TOT-964	TOT-965	TOT-966	TOT-967	TOT-968	TOT-969	TOT-970	TOT-971	TOT-972	TOT-973	TOT-974	TOT-975	TOT-976	TOT-977	TOT-978	TOT-979	TOT-980	TOT-981	TOT-982	TOT-983	TOT-984	TOT-985	TOT-986	TOT-987	TOT-988	TOT-989	TOT-990	TOT-991	TOT-992	TOT-993	TOT-994	TOT-995	TOT-996	TOT-997	TOT-998	TOT-999	TOT-1000	TOT-1001	TOT-1002	TOT-1003	TOT-1004	TOT-1005	TOT-1006	TOT-1007	TOT-1008	TOT-1009	TOT-1010	TOT-1011	TOT-1012	TOT-1013	TOT-1014	TOT-1015	TOT-1016	TOT-1017	TOT-1018	TOT-1019	TOT-1020	TOT-1021	TOT-1022	TOT-1023	TOT-1024	TOT-1025	TOT-1026	TOT-1027	TOT-1028	TOT-1029	TOT-1030	TOT-1031	TOT-1032	TOT-1033	TOT-1034	TOT-1035	TOT-1036	TOT-1037	TOT-1038	TOT-1039	TOT-1040	TOT-1041	TOT-1042	TOT-1043	TOT-1044	TOT-1045	TOT-1046	TOT-1047	TOT-1048	TOT-1049	TOT-1050	TOT-1051	TOT-1052	TOT-1053	TOT-1054	TOT-1055	TOT-1056	TOT-1057	TOT-1058	TOT-1059	TOT-1060	TOT-1061	TOT-1062	TOT-1063	TOT-1064	TOT-1065	TOT-1066	TOT-1067	TOT-1068	TOT-1069	TOT-1070	TOT-1071	TOT-1072	TOT-1073	TOT-1074	TOT-1075	TOT-1076	TOT-1077	TOT-1078	TOT-1079	TOT-1080	TOT-1081	TOT-1082	TOT-1083	TOT-1084	TOT-1085	TOT-1086	TOT-1087	TOT-1088	TOT-1089	TOT-1090	TOT-1091	TOT-1092	TOT-1093	TOT-1094	TOT-1095	TOT-1096	TOT-1097	TOT-1098	TOT-1099	TOT-1100	TOT-1101	TOT-1102	TOT-1103	TOT-1104	TOT-1105	TOT-1106	TOT-1107	TOT-1108	TOT-1109	TOT-1110	TOT-1111	TOT-1112	TOT-1113	TOT-1114	TOT-1115	TOT-1116	TOT-1117	TOT-1118	TOT-1119	TOT-1120	TOT-1121	TOT-1122	TOT-1123	TOT-1124	TOT-1125	TOT-1126	TOT-1127	TOT-1128	TOT-1129	TOT-1130	TOT-1131	TOT-1132	TOT-1133	TOT-1134	TOT-1135	TOT-1136	TOT-1137	TOT-1138	TOT-1139	TOT-1140	TOT-1141	TOT-1142	TOT-1143	TOT-1144	TOT-1145	TOT-1146	TOT-1147	TOT-1148	TOT-1149	TOT-1150	TOT-1151	TOT-1152	TOT-1153	TOT-1154	TOT-1155	TOT-1156	TOT-1157	TOT-1158	TOT-1159	TOT-1160	TOT-1161	TOT-1162	TOT-1163	TOT-1164	TOT-1165	TOT-1166	TOT-1167	TOT-1168	TOT-1169	TOT-1170	TOT-1171	TOT-1172	TOT-1173	TOT-1174	TOT-1175	TOT-1176	TOT-1177	TOT-1178	TOT-1179	TOT-1180	TOT-1181	TOT-1182	TOT-1183	TOT-1184	TOT-1185	TOT-1186	TOT-1187	TOT-1188	TOT-1189	TOT-1190	TOT-1191	TOT-1192	TOT-1193	TOT-1194	TOT-1195	TOT-1196	TOT-1197	TOT-1198	TOT-1199	TOT-1200	TOT-1201	TOT-1202	TOT-1203	TOT-1204	TOT-1205	TOT-1206	TOT-1207	TOT-1208	TOT-1209	TOT-1210	TOT-1211	TOT-1212	TOT-1213	TOT-12
----	-------	-------	-----	-----	------	------	------	------	-----	-----	-----	-----	---------------------------	--	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	--------

TABLE XVIII

AERODYNAMIC SUMMARY — ROTOR 2  
(SI Units)

SL	EP51-1	EP51-2	V-1	V-2	VM-1	VM-2	VO-1	VO-2	R-1	R-2	M-1	M-2	U-1	U-2	O, POINT NO. 0	V1-1	V1-2
	RADIAN	RADIAN	M/SEC	M/SEC	M/SEC	M/SEC	M/SEC	M/SEC	RADIAN	RADIAN	M/SEC	M/SEC	M/SEC	M/SEC		M/SEC	M/SEC
1	0.1805	0.1249	149.8	268.6	148.1	184.5	22.9	195.3	0.1521	0.8050	0.4180	0.7378	187.9	203.4	0.6186	0.5072	221.7
2	0.1638	0.1138	141.0	260.1	159.4	186.4	22.7	181.4	0.1409	0.7654	0.4523	0.7189	196.4	209.7	0.6623	0.5197	235.7
3	0.1429	0.1017	170.5	251.8	169.6	187.9	22.8	167.7	0.1335	0.7240	0.4814	0.6953	205.1	216.4	0.7019	0.5360	248.6
4	0.1255	0.0906	176.4	244.3	174.9	186.9	22.7	157.3	0.1287	0.6963	0.4996	0.6750	213.9	223.4	0.7339	0.5478	259.1
5	0.1106	0.0805	180.8	238.7	179.4	185.5	22.7	150.2	0.1255	0.6783	0.5132	0.6594	222.6	230.7	0.7624	0.5586	268.6
6	0.0844	0.0614	185.0	227.9	183.7	180.4	22.5	139.3	0.1221	0.6567	0.5264	0.6286	240.2	245.6	0.8102	0.5775	284.8
7	0.0621	0.0447	186.2	218.4	184.8	174.6	22.5	131.2	0.1211	0.6438	0.5300	0.6009	257.2	261.4	0.8520	0.5993	299.3
8	0.0427	0.0294	185.8	210.2	184.5	169.7	22.5	124.0	0.1214	0.6311	0.5290	0.5770	275.7	277.6	0.8919	0.6284	313.3
9	0.0242	0.0160	185.0	203.4	183.6	165.8	22.5	117.8	0.1227	0.6178	0.5262	0.5570	293.5	294.2	0.9309	0.6631	327.3
10	0.0185	0.0098	184.1	199.4	182.8	163.7	22.5	114.8	0.1222	0.6115	0.5235	0.5470	302.5	302.9	0.9506	0.6821	344.4
11	0.0113	0.0039	183.3	196.9	181.9	161.9	22.5	111.9	0.1232	0.6049	0.5208	0.5379	311.6	311.5	0.9703	0.7023	341.6
12	0.0068	0.0021	181.0	190.9	179.6	158.2	22.4	106.8	0.1242	0.5936	0.5130	0.5199	329.8	329.8	1.0089	0.7434	356.0
13	0.0052	0.0010	179.4	187.6	178.0	154.5	22.3	106.9	0.1247	0.6051	0.5074	0.5099	339.0	338.3	1.0275	0.7552	363.3
14	0.0069	0.0107	179.1	186.3	177.7	150.3	22.3	110.0	0.1251	0.6317	0.5043	0.5021	348.2	347.5	1.0450	0.7574	371.1
15	0.0052	0.0073	178.2	186.9	176.8	146.7	22.3	115.9	0.1254	0.6687	0.4982	0.4996	357.2	356.8	1.0611	0.7537	378.7
16	0.0000	0.0000	180.1	190.9	178.7	145.4	22.3	123.7	0.1257	0.7050	0.5011	0.5047	366.0	366.0	1.0772	0.7472	387.2

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-R	LOSS-P	PO2/	%EFF-P	%EFF-A	B1-1	B1-2	VR1-1	VR1-2	PO/PO
	RADIAN	RADIAN	RADIAN	RADIAN					TOTAL	PO1	TOT	TOT	RADIAN	RADIAN	M/SEC	M/SEC	INLET
1	0.1009	0.0260	0.2652	0.7926	42.09	55.47	0.3576	0.1124	0.0262	1.3901	92.91	92.57	0.8359	0.0432	-165.0	-8.1	1.9713
2	0.0848	0.0378	0.2506	0.6768	45.59	57.55	0.3695	0.0892	0.0213	1.3733	93.41	93.11	0.8255	0.1487	-173.7	-28.3	1.9715
3	0.0778	0.0385	0.2321	0.5695	48.47	59.26	0.3703	0.0651	0.0158	1.3553	94.42	94.16	0.8213	0.2517	-182.3	-48.8	1.9675
4	0.0684	0.0419	0.2086	0.4901	50.19	59.90	0.3734	0.0495	0.0121	1.3435	95.27	95.06	0.8283	0.3381	-191.1	-66.2	1.9619
5	0.0649	0.0397	0.1960	0.4311	51.43	60.21	0.3775	0.0410	0.0101	1.3374	95.74	95.56	0.8386	0.4076	-199.9	-80.5	1.9613
6	0.0516	0.0420	0.1669	0.3379	52.55	59.61	0.3841	0.0355	0.0088	1.3286	95.83	95.66	0.8696	0.5317	-217.6	-106.3	1.9530
7	0.0423	0.0409	0.1395	0.2651	52.77	58.39	0.3841	0.0373	0.0092	1.3222	95.20	95.01	0.9054	0.6403	-235.4	-130.2	1.9422
8	0.0271	0.0466	0.1168	0.2058	52.63	57.22	0.3751	0.0395	0.0095	1.3166	94.52	94.30	0.9414	0.7356	-253.3	-153.6	1.9314
9	0.0077	0.0569	0.1146	0.1588	52.37	56.20	0.3605	0.0416	0.0098	1.3111	93.79	93.54	0.9753	0.8165	-270.9	-176.4	1.9217
10	0.0047	0.0662	0.1101	0.1381	52.11	55.60	0.3520	0.0428	0.0100	1.3083	93.39	93.13	0.9926	0.8545	-289.0	-188.1	1.9157
11	0.0187	0.0621	0.1086	0.1199	51.86	55.06	0.3427	0.0436	0.0100	1.3055	93.03	92.76	1.0091	0.8892	-280.1	-199.6	1.9103
12	0.0283	0.0670	0.1102	0.0894	51.10	53.78	0.3241	0.0459	0.0102	1.3001	92.21	91.91	1.0419	0.9525	-307.4	-222.4	1.8979
13	0.0330	0.0718	0.1135	0.0766	50.53	52.29	0.3257	0.0639	0.0140	1.2973	89.12	88.71	1.0587	0.9821	-316.7	-231.4	1.8898
14	0.0369	0.0758	0.1174	0.0652	50.08	50.30	0.3381	0.0970	0.0211	1.2943	83.84	83.23	1.0715	1.0063	-325.8	-237.4	1.8847
15	0.0404	0.0793	0.1239	0.0613	49.40	48.39	0.3578	0.1364	0.0296	1.2986	78.39	77.57	1.0851	1.0238	-334.9	-240.9	1.8868
16	0.0318	0.0708	0.1596	0.0607	49.26	47.10	0.3810	0.1773	0.0390	1.3051	73.42	72.39	1.0911	1.0304	-343.5	-242.3	1.8997

TC/TC	PC/PO	EFF-AD	EFF-P	WCI/A1	TC2/TC1	PO2/PO1	EFF-AU	EFF-P	ROTOR	%
INLET	INLET	INLET	INLET	KG/SEC			ROTOR	ROTOR	%	
1.2354	1.9242	87.28	88.39	173.80	1.0898	1.3170	90.92	91.27		

TABLE XVIII (Cont'd)

AERODYNAMIC SUMMARY - ROTOR 2  
(English Units)

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	R-1	R-2	M-1	M-2	U-1	U-2	0, POINT NO	0	V0-1	V0-2
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC			FT/SEC	FT/SEC
1	10.858	7.249	491.6	481.4	485.8	605.4	75.0	640.7	8.7	46.1	0.4180	0.7378	616.6	667.3	0.6186	0.5072	721.5	606.0
2	9.385	6.522	528.2	523.4	522.9	611.7	74.6	595.2	8.1	43.9	0.4523	0.7169	644.5	688.0	0.6623	0.5197	773.4	618.7
3	8.190	5.829	554.5	526.1	554.4	616.4	74.8	590.1	7.6	41.5	0.4814	0.6953	673.0	710.1	0.7019	0.5360	815.6	636.8
4	7.188	5.193	578.7	501.4	573.9	613.2	74.5	516.0	7.4	39.2	0.4996	0.6750	701.7	733.1	0.7339	0.5478	850.1	650.5
5	6.335	4.611	593.2	783.2	588.5	608.7	74.4	492.8	7.2	38.9	0.5132	0.6594	730.4	756.8	0.7624	0.5586	881.3	663.5
6	4.838	3.516	607.1	747.7	602.6	591.8	74.0	457.1	7.0	37.6	0.5264	0.6286	788.1	805.9	0.8102	0.5775	934.4	686.9
7	3.558	2.559	610.8	716.5	606.3	572.9	73.8	430.3	6.9	36.9	0.5300	0.6009	846.2	857.5	0.8520	0.5993	982.0	714.7
8	2.448	1.687	609.7	689.7	605.2	556.8	73.8	407.0	7.0	36.2	0.5290	0.5770	904.7	911.0	0.8919	0.6284	1028.0	751.0
9	1.495	0.916	606.9	667.3	602.4	543.9	74.0	386.5	7.0	35.4	0.5262	0.5470	962.8	965.4	0.9309	0.6631	1075.8	794.3
10	1.058	0.563	604.2	656.0	599.6	537.1	73.9	376.6	7.0	35.0	0.5235	0.5470	992.6	993.7	0.9506	0.6821	1097.1	818.1
11	0.647	0.225	601.5	645.9	596.9	531.3	73.9	367.3	7.1	34.7	0.5208	0.5379	1022.4	1022.2	0.9703	0.7023	1120.7	843.3
12	-0.048	-0.374	594.0	626.3	589.4	519.1	73.6	350.3	7.1	34.0	0.5130	0.5199	1082.1	1080.1	1.0089	0.7434	1168.1	895.6
13	-0.298	-0.577	586.6	616.3	584.0	506.9	73.2	330.6	7.1	34.7	0.5074	0.5099	1112.3	1109.8	1.0275	0.7552	1192.0	912.8
14	-0.398	-0.611	587.6	611.2	583.0	493.2	73.3	361.0	7.2	36.2	0.5043	0.5021	1142.3	1140.0	1.0450	0.7574	1217.6	922.0
15	-0.297	-0.418	584.6	613.3	580.0	481.2	73.1	380.3	7.2	38.3	0.4992	0.4996	1172.0	1170.5	1.0611	0.7537	1242.5	925.2
16	0.000	0.000	580.9	624.3	586.2	477.1	74.1	405.0	7.2	40.4	0.5011	0.5047	1201.0	1201.0	1.0772	0.7472	1270.3	927.2

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	P02/	%EFF-P	%EFF-A	R0-1	R0-2	V0-1	V0-2	PO/PO
DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	PC1	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	-5.78	1.60	15.20	45.41	42.00	55.47	0.3576	0.1124	0.0262	1.3901	92.91	92.57	47.89	2.48	-541.5	-26.6	1.9713
2	-4.86	2.17	14.26	38.78	45.50	57.55	0.3695	0.0892	0.0213	1.3733	93.41	93.11	47.30	8.52	-569.9	-92.8	1.9715
3	-4.46	2.21	13.30	32.63	48.47	59.24	0.3703	0.0651	0.0158	1.3553	94.42	94.16	47.06	14.42	-598.2	-160.0	1.9675
4	-3.92	2.40	11.95	28.08	50.19	59.90	0.3784	0.0495	0.0121	1.3435	95.27	95.06	47.46	19.37	-627.2	-217.1	1.9619
5	-3.72	2.28	11.35	24.70	51.43	60.21	0.3775	0.0410	0.0101	1.3374	95.74	95.56	48.05	23.35	-656.0	-264.0	1.9613
6	-2.46	2.40	9.68	19.36	52.55	58.39	0.3841	0.0355	0.0088	1.3286	95.83	95.66	49.83	30.47	-714.1	-348.9	1.9530
7	-2.43	2.35	7.99	15.19	52.77	58.39	0.3841	0.0373	0.0092	1.3222	95.20	95.01	51.87	36.69	-772.5	-427.2	1.9422
8	-1.55	2.67	6.81	11.70	52.63	57.22	0.3751	0.0395	0.0095	1.3166	94.52	94.30	53.94	42.15	-830.9	-504.0	1.9314
9	-0.44	3.26	6.57	9.10	52.37	56.20	0.3605	0.0416	0.0098	1.3111	93.79	93.54	55.88	46.78	-888.9	-578.9	1.9217
10	0.27	3.45	6.31	7.91	52.11	55.60	0.3520	0.0428	0.0100	1.3083	93.39	93.13	56.87	48.96	-918.7	-617.0	1.9157
11	1.07	3.56	6.22	6.87	51.86	55.06	0.3427	0.0436	0.0100	1.3055	93.03	92.76	57.82	50.95	-948.5	-654.9	1.9103
12	1.62	3.84	6.32	5.12	51.10	53.78	0.3241	0.0459	0.0102	1.3001	92.21	91.91	59.70	54.57	-1008.5	-729.8	1.8979
13	1.89	4.11	6.51	4.39	50.53	52.20	0.3257	0.0639	0.0102	1.2973	89.12	88.71	60.66	56.27	-1039.1	-759.2	1.8898
14	2.12	4.35	6.73	3.73	50.08	50.30	0.3381	0.0670	0.0211	1.2944	83.84	83.23	61.39	57.66	-1069.0	-779.0	1.8847
15	2.31	4.54	7.10	3.51	49.40	48.39	0.3578	0.1364	0.0296	1.2986	78.39	77.57	62.17	58.66	-1098.9	-790.2	1.8868
16	1.82	4.06	9.15	3.48	49.26	47.10	0.3810	0.1773	0.0390	1.3051	73.42	72.39	62.52	59.04	-1126.9	-795.1	1.8997

TC/TO	PO/PO	EFF-AD	EFF-P	WCI/A1	TC2/TC1	P02/P01	EFF-AD	EFF-P
INLET	INLET	%	%	LB/SEC	ROTOR	ROTOR	%	%
1.2354	1.9242	87.28	88.39	35.62	1.0898	1.3170	90.92	91.27

TABLE XIX

# AERODYNAMIC SUMMARY - STATOR 2 (SI Units)

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	O <sub>2</sub> SPEED	CODE	O <sub>2</sub> POINT	NO.	0
	RADIAN	RADIAN	M/SEC	M/SEC	M/SEC	M/SEC	M/SEC	M/SEC	RADIAN	RADIAN			PO/PO		INLET	STAGE	TOT/
																	TOT
1	0.1439	0.1717	240.9	173.2	144.9	173.2	192.4	0.0	0.9200	0.0000	0.6545	0.4613	1.8694		1.2708	1.3182	1.1063
2	0.1237	0.1450	237.2	176.7	156.6	176.7	178.2	0.0	0.8458	0.0000	0.6482	0.4742	1.8923		1.2549	1.3181	1.1016
3	0.1072	0.1226	233.6	179.5	166.1	179.5	164.4	0.0	0.7777	0.0000	0.6409	0.4842	1.9121		1.2430	1.3171	1.0961
4	0.0933	0.1037	230.4	179.9	171.3	179.9	154.1	0.0	0.7306	0.0000	0.6335	0.4871	1.9227		1.2351	1.3167	1.0924
5	0.0814	0.0878	228.7	179.9	175.1	179.9	147.1	0.0	0.6978	0.0000	0.6294	0.4880	1.9302		1.2311	1.3162	1.0904
6	0.0613	0.0619	223.7	177.4	177.2	177.4	136.6	0.0	0.6564	0.0000	0.6161	0.4819	1.9329		1.2260	1.3149	1.0882
7	0.0455	0.0426	218.0	173.6	173.6	173.6	128.9	0.0	0.6325	0.0000	0.5998	0.4716	1.9273		1.2242	1.3121	1.0872
8	0.0329	0.0283	212.0	169.7	173.2	169.7	122.3	0.0	0.6146	0.0000	0.5823	0.4606	1.9185		1.2233	1.3078	1.0865
9	0.0230	0.0182	206.2	166.0	170.1	166.0	116.5	0.0	0.6004	0.0000	0.5652	0.4500	1.9085		1.2237	1.3021	1.0858
10	0.0189	0.0142	203.0	163.7	168.1	163.7	113.7	0.0	0.5946	0.0000	0.5557	0.4436	1.9018		1.2241	1.2987	1.0855
11	0.0155	0.0111	199.9	161.5	166.2	161.5	111.0	0.0	0.5889	0.0000	0.5457	0.4371	1.8948		1.2247	1.2949	1.0851
12	0.0102	0.0069	193.7	156.4	162.0	156.4	106.2	0.0	0.5803	0.0000	0.5280	0.4224	1.8792		1.2283	1.2873	1.0845
13	0.0081	0.0055	190.5	153.2	158.0	153.2	106.5	0.0	0.5929	0.0000	0.5175	0.4122	1.8687		1.2343	1.2828	1.0868
14	0.0056	0.0038	188.8	151.1	153.7	151.1	109.7	0.0	0.6201	0.0000	0.5093	0.4038	1.8601		1.2500	1.2775	1.0917
15	0.0027	0.0017	184.3	147.9	149.8	147.9	115.8	0.0	0.6578	0.0000	0.5083	0.3917	1.8481		1.2705	1.2719	1.0996
16	0.0000	0.0000	193.4	147.2	148.6	147.2	123.7	0.0	0.6941	0.0000	0.5116	0.3853	1.8416		1.2996	1.2651	1.1088

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	PO2/	STATC-ST	PO2/	INLET	EFF-P	TOT-INLET	EFF-A	TOT-STG	EFF-P	TOT-STG
1	0.6508	0.0566	0.1702	0.9200	45.91	57.61	0.4399	0.2068	0.0420	0.9483	62.49	77.18	78.24	77.06	77.06	77.06	77.06	77.06	77.06
2	0.7250	0.0525	0.1506	0.6458	50.47	59.91	0.4100	0.1634	0.0343	0.9598	67.99	83.65	83.65	80.18	80.18	80.59	81.34	81.34	81.34
3	0.7931	0.0553	0.1419	0.7777	54.14	61.77	0.3823	0.1167	0.0253	0.9718	75.29	87.28	87.28	85.06	85.06	84.97	85.54	85.54	85.54
4	0.8402	0.0432	0.1404	0.7306	56.31	62.59	0.3672	0.0843	0.0189	0.9800	81.26	89.39	89.39	88.39	88.39	88.32	88.76	88.76	88.76
5	0.8730	0.0530	0.1423	0.6978	57.84	63.01	0.3605	0.0677	0.0156	0.9842	84.59	91.61	91.61	90.32	90.32	90.10	90.48	90.48	90.48
6	0.9144	0.0687	0.1469	0.6564	58.98	62.66	0.3561	0.0455	0.0112	0.9897	89.31	91.87	91.87	92.34	92.34	92.05	92.35	92.35	92.35
7	0.9383	0.0863	0.1514	0.6325	58.84	61.52	0.3574	0.0356	0.0093	0.9923	91.45	91.54	91.54	92.58	92.58	92.28	92.58	92.58	92.58
8	0.9562	0.1107	0.1552	0.6146	58.24	60.19	0.3590	0.0326	0.0090	0.9933	91.95	91.95	91.95	92.21	92.21	91.91	92.21	92.21	92.21
9	0.9704	0.1219	0.1597	0.6004	57.42	58.82	0.3604	0.0353	0.0103	0.9931	91.05	90.58	90.58	91.39	91.39	91.07	91.40	91.40	91.40
10	0.9762	0.1276	0.1625	0.5946	56.84	57.96	0.3621	0.0386	0.0116	0.9927	90.11	89.90	89.90	90.77	90.77	90.49	90.84	90.84	90.84
11	0.9819	0.1326	0.1655	0.5889	56.28	57.08	0.3644	0.0442	0.0137	0.9919	88.58	89.08	89.08	90.01	90.01	89.82	90.19	90.19	90.19
12	0.9905	0.1525	0.1746	0.5803	54.85	55.02	0.3719	0.0570	0.0187	0.9901	85.17	86.43	86.43	87.57	87.57	86.32	88.73	88.73	88.73
13	0.9779	0.1561	0.1827	0.5929	53.28	53.53	0.3830	0.0671	0.0226	0.9888	82.73	83.42	83.42	84.80	84.80	84.74	85.27	85.27	85.27
14	0.9507	0.1712	0.2009	0.6201	51.24	52.07	0.4005	0.0807	0.0279	0.9849	79.52	77.53	77.53	79.39	79.39	78.84	79.56	79.56	79.56
15	0.9130	0.1751	0.2192	0.6578	49.27	50.06	0.4354	0.1279	0.0453	0.9795	69.87	70.83	70.83	73.21	73.21	71.19	72.17	72.17	72.17
16	0.8767	0.1849	0.2457	0.6941	47.99	48.65	0.4713	0.1874	0.0681	0.9694	59.00	63.52	63.52	66.47	66.47	63.64	64.84	64.84	64.84

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	PO2/	STATC-ST	PO2/	INLET	EFF-P	TOT-INLET	EFF-A	TOT-STG	EFF-P	TOT-STG
1	0.6508	0.0566	0.1702	0.9200	45.91	57.61	0.4399	0.2068	0.0420	0.9483	62.49	77.18	78.24	77.06	77.06	77.06	77.06	77.06	77.06
2	0.7250	0.0525	0.1506	0.6458	50.47	59.91	0.4100	0.1634	0.0343	0.9598	67.99	83.65	83.65	80.18	80.18	80.59	81.34	81.34	81.34
3	0.7931	0.0553	0.1419	0.7777	54.14	61.77	0.3823	0.1167	0.0253	0.9718	75.29	87.28	87.28	85.06	85.06	84.97	85.54	85.54	85.54
4	0.8402	0.0432	0.1404	0.7306	56.31	62.59	0.3672	0.0843	0.0189	0.9800	81.26	89.39	89.39	88.39	88.39	88.32	88.76	88.76	88.76
5	0.8730	0.0530	0.1423	0.6978	57.84	63.01	0.3605	0.0677	0.0156	0.9842	84.59	91.61	91.61	90.32	90.32	90.10	90.48	90.48	90.48
6	0.9144	0.0687	0.1469	0.6564	58.98	62.66	0.3561	0.0455	0.0112	0.9897	89.31	91.87	91.87	92.34	92.34	92.05	92.35	92.35	92.35
7	0.9383	0.0863	0.1514	0.6325	58.84	61.52	0.3574	0.0356	0.0093	0.9923	91.45	91.54	91.54	92.58	92.58	92.28	92.58	92.58	92.58
8	0.9562	0.1107	0.1552	0.6146	58.24	60.19	0.3590	0.0326	0.0090	0.9933	91.95	91.95	91.95	92.21	92.21	91.91	92.21	92.21	92.21
9	0.9704	0.1219	0.1597	0.6004	57.42	58.82	0.3604	0.0353	0.0103	0.9931	91.05	90.58	90.58	91.39	91.39	91.07	91.40	91.40	91.40
10	0.9762	0.1276	0.1625	0.5946	56.84	57.96	0.3621	0.0386	0.0116	0.9927	90.11	89.90	89.90	90.77	90.77	90.49	90.84	90.84	90.84
11	0.9819	0.1326	0.1655	0.5889	56.28	57.08	0.3644	0.0442	0.0137	0.9919	88.58	89.08	89.08	90.01	90.01	89.82	90.19	90.19	90.19
12	0.9905	0.1525	0.1746	0.5803	54.85	55.02	0.3719	0.0570	0.0187	0.9901	85.17	86.43	86.43	87.57	87.57	86.32	88.73	88.73	88.73
13	0.9779	0.1561	0.1827	0.5929	53.28	53.53	0.3830	0.0671	0.0226	0.9888	82.73	83.42	83.42	84.80	84.80	84.74	85.27	85.27	85.27
14	0.9507	0.1712	0.2009	0.6201	51.24	52.07	0.4005	0.0807	0.0279	0.9849	79.52	77.53	77.53	79.39	79.39	78.84	79.56	79.56	79.56
15	0.9130	0.1751	0.2192	0.6578	49.27	50.06	0.4354	0.1279	0.0453	0.9795	69.87	70.83	70.83	73.21	73.21	71.19	72.17	72.17	72.17
16	0.8767	0.1849	0.2457	0.6941	47.99	48.65	0.4713	0.1874	0.0681	0.9694	59.00	63.52	63.52	66.47	66.47	63.64	64.84	64.84	64.84

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	PO2/	STATC-ST	PO2/	INLET	EFF-P	TOT-INLET	EFF-A	TOT-STG	EFF-P	TOT-STG
1	0.6508	0.0566	0.1702	0.9200	45.91	57.61	0.4399	0.2068	0.0420	0.9483	62.49	77.18	78.24	77.06	77.06	77.06	77.06	77.06	77.06
2	0.7250	0.0525	0.1506	0.6458	50.47	59.91	0.4100	0.1634	0.0343	0.9598	67.99	83.65	83.65	80.18	80.18	80.59	81.34	81.34	81.34
3	0.7931	0.0553	0.1419	0.7777	54.14	61.77	0.3823	0.1167	0.0253	0.9718	75.29	87.28	87.28	85.06	85.06	84.97	85.54	85.54	85.54
4	0.8402	0.0432	0.1404	0.7306	56.31	62.59	0.3672	0.0843	0.0189	0.9800	81.26	89.39	89.39	88.39	88.39	88.32	88.76	88.76	88.76
5	0.8730	0.0530	0.1423	0.6978	57.84	63.01	0.3605	0.0677	0.0156	0.9842	84.59	91.61	91.61	90.32	90.32	90.10	90.48	90.48	90.48
6	0.9144	0.0687	0.1469	0.6564	58.98	62.66	0.3561	0.0455	0.0112	0.9897	89.31	91.87	91.87	92.34	92.34	92.05	92.35	92.35	92.35
7	0.9383	0.0863	0.1514	0.6325	58.84	61.52	0.3574	0.0356	0.0093	0.9923	91.45	91.54	91.54	92.58	92.58	92.28	92		

TABLE XIX (Cont'd)  
AERODYNAMIC SUMMARY - STATOR 2  
(English Units)

SL	EPSI-1	FPSI-2	V-1	V-2	VM-1	VM-2	V6-1	V6-2	R-1	B-2	M-1	M-2	RUN NO	0, SPEED CODE	0, POINT NO	0	TOT/PO	TOT/STG
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE							STAGE	TOT
1	8.242	9.838	790.3	568.3	475.3	568.3	631.3	631.3	0.0	52.7	0.0	0.6545	0.4613	1.8694	1.2708	1.3182	1.1063	
2	7.090	8.306	778.3	579.8	513.9	579.8	584.5	584.5	0.0	48.5	0.0	0.6482	0.4742	1.8923	1.2549	1.3181	1.1016	
3	6.145	7.022	766.6	588.8	544.8	588.8	539.3	539.3	0.0	44.6	0.0	0.6409	0.4842	1.9121	1.2430	1.3171	1.0961	
4	5.347	5.942	756.0	590.3	562.2	590.3	505.5	505.5	0.0	41.9	0.0	0.6335	0.4871	1.9227	1.2351	1.3167	1.0924	
5	4.664	5.030	750.2	590.3	574.4	590.3	482.7	482.7	0.0	40.0	0.0	0.6294	0.4880	1.9302	1.2311	1.3162	1.0904	
6	3.513	3.548	734.0	582.1	581.3	582.1	448.2	448.2	0.0	37.6	0.0	0.6161	0.4819	1.9329	1.2260	1.3149	1.0882	
7	2.605	2.440	715.3	569.7	576.9	569.7	422.9	422.9	0.0	36.2	0.0	0.5998	0.4716	1.9273	1.2242	1.3121	1.0872	
8	1.882	1.624	695.6	556.8	568.3	556.8	401.1	401.1	0.0	35.2	0.0	0.5823	0.4606	1.9185	1.2233	1.3078	1.0865	
9	1.321	1.041	676.5	544.6	558.2	544.6	382.2	382.2	0.0	34.4	0.0	0.5652	0.4500	1.9085	1.2237	1.3021	1.0858	
10	1.085	0.814	665.9	537.2	551.6	537.2	373.0	373.0	0.0	34.1	0.0	0.5557	0.4436	1.9018	1.2241	1.2987	1.0855	
11	0.885	0.636	655.9	529.8	545.4	529.8	364.3	364.3	0.0	33.7	0.0	0.5467	0.4371	1.8948	1.2247	1.2949	1.0851	
12	0.586	0.396	635.6	513.3	531.6	513.3	348.5	348.5	0.0	33.2	0.0	0.5280	0.4224	1.8792	1.2283	1.2873	1.0845	
13	0.464	0.313	625.1	502.6	518.4	502.6	349.3	349.3	0.0	34.0	0.0	0.5175	0.4122	1.8687	1.2343	1.2828	1.0868	
14	0.321	0.216	619.5	495.7	504.2	495.7	340.0	340.0	0.0	35.5	0.0	0.5093	0.4038	1.8601	1.2500	1.2775	1.0917	
15	0.155	0.100	621.2	485.3	491.5	485.3	379.8	379.8	0.0	37.7	0.0	0.5063	0.3917	1.8481	1.2705	1.2719	1.0996	
16	-0.000	0.000	634.5	483.0	487.7	483.0	405.9	405.9	0.0	39.8	0.0	0.5116	0.3853	1.8416	1.2996	1.2651	1.1088	

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	U-FAC	OMEGA-B	LOSS-P	P02/	STATC-ST	EFF-P	EFF-A	EFF-P	EFF-A
DEGREE	DEGREE	DEGREE	DEGREE	DEGREE				TOTAL	TOTAL	P01		TOT-INLET	TOT-INLET	TOT-STG	TOT-STG
1	-37.29	-3.24	9.75	52.71	45.91	57.61	0.4399	0.0420	0.2068	0.9483	62.49	72.18	74.50	77.06	77.94
2	-41.54	-3.06	8.63	48.46	50.47	59.91	0.4100	0.0343	0.0343	0.9598	67.99	78.34	80.18	80.59	81.34
3	-45.44	-3.17	8.13	44.56	54.14	61.77	0.3823	0.0253	0.0253	0.9718	75.29	83.65	85.06	84.97	85.54
4	-48.14	-2.30	8.04	41.86	56.31	62.59	0.3672	0.0843	0.0189	0.9800	81.26	87.28	88.39	88.32	88.76
5	-50.02	-3.03	8.15	39.98	57.84	63.01	0.3605	0.0677	0.0156	0.9842	84.59	89.39	90.32	90.10	90.48
6	-52.39	-3.93	8.42	37.61	58.98	62.66	0.3561	0.0455	0.0112	0.9897	89.31	91.61	92.34	92.05	92.55
7	-53.76	-5.52	8.67	36.24	58.84	61.52	0.3574	0.0356	0.0093	0.9923	91.45	91.87	92.58	92.28	92.58
8	-54.78	-6.34	8.89	35.22	58.24	60.18	0.3590	0.0326	0.0090	0.9933	91.95	91.54	92.28	91.91	92.21
9	-55.60	-6.98	9.15	34.40	57.42	58.82	0.3604	0.0353	0.0103	0.9931	91.05	90.58	91.39	91.07	91.40
10	-55.93	-7.31	9.31	34.07	56.84	57.96	0.3621	0.0386	0.0116	0.9927	90.11	89.90	90.77	90.49	90.84
11	-56.26	-7.66	9.48	33.74	56.28	57.08	0.3644	0.0442	0.0137	0.9919	88.58	89.08	90.01	89.82	90.19
12	-56.75	-8.74	10.00	33.25	54.85	55.02	0.3719	0.0570	0.0187	0.9901	85.17	86.43	87.57	88.32	88.73
13	-56.03	-8.94	10.47	33.97	53.28	53.53	0.3839	0.0671	0.0226	0.9888	82.73	84.40	84.80	84.74	85.27
14	-54.47	-8.81	11.51	35.53	51.24	52.07	0.4005	0.0807	0.0279	0.9866	79.52	77.53	79.39	78.84	79.56
15	-52.31	-10.26	12.56	37.69	49.27	50.06	0.4354	0.1279	0.0453	0.9795	69.87	70.83	73.21	71.19	72.17
16	-50.23	-10.60	14.08	39.77	47.99	48.65	0.4713	0.0681	0.0681	0.9694	59.00	63.52	66.47	63.64	64.84

SL	INCRF	WCRF	TOT/TO	EFF-P	EFF-AD	EFF-P
RPM	INLET	INLET		INLET	STAGE	TOT-STG
8367.212.50	1.2354	1.8984	85.31	86.57	86.30	317.18

## APPENDIX C

## TABLE XX

## AIRFOIL GEOMETRY ON DESIGN CONICAL SURFACES - ROTOR 1

(For Definitions see Figure 15 and 25)

	HUB	ROOT										TIP										TIP								
		INLET					EXIT					INCHES					METERS													
		DIAMETER =					DIAMETER =					METERS					INCHES													
MULTIPLE - CIRCULAR - ARC AIRFOILS, 28 BLADES																														
PERCENT FLOW	.00	2.50	5.00	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.00	95.00	100.00	PERCENT SPAN (LE)	.00	4.31	8.37	15.88	29.08	40.60	50.97	60.47	69.30	77.59	85.42	92.88	96.48	100.00	
PERCENT SPAN (AV)	.00	4.30	8.27	15.56	28.43	39.80	52.55	68.58	74.93	84.89	92.55	96.29	100.00	PERCENT SPAN (TE)	.00	4.29	8.17	15.24	27.78	38.99	49.28	58.83	67.80	76.28	84.37	92.21	96.10	100.00		
SI Units (Meters & Radians)																														
c	.0897	.0905	.0913	.0928	.0955	.0979	.1001	.1021	.1039	.1057	.1073	.1089	.1097	.1105	c <sub>f</sub>	.0458	.0449	.0479	.0499	.0533	.0564	.0591	.0615	.0639	.0660	.0681	.0700	.0710	.0719	
t/c	.0800	.0780	.0764	.0730	.0688	.0642	.0603	.0553	.0503	.0459	.0420	.0381	.0341	.0300	% c to max t	57.600	57.976	58.329	58.978	60.110	61.097	61.986	62.801	63.559	64.272	64.946	65.587	66.200	66.780	
a/c	.5782	.5740	.5734	.5811	.5994	.6078	.6209	.6392	.6555	.6716	.6844	.6952	.7044	.7124	RLE (x 10 <sup>3</sup> )	.0330	.0323	.0315	.0300	.0272	.0249	.0229	.0209	.0190	.0178	.0170	.0168	.0178	.0178	
RLE (x 10 <sup>3</sup> )	.0330	.0323	.0315	.0300	.0272	.0249	.0229	.0209	.0190	.0178	.0170	.0168	.0178	.0178	RTE (x 10 <sup>2</sup> )	.5689	.5727	.5903	.6256	.6834	.7413	.7989	.8443	.8808	.9053	.9245	.9436	.9589	.9743	
$\beta^*_{1s}$	.6671	.6699	.6865	.7195	.7745	.8275	.8801	.9185	.9284	.9447	.9633	.9824	.9974	1.0129	$\beta^*_{1s}$	.6671	.6699	.6865	.7195	.7745	.8275	.8801	.9185	.9284	.9447	.9633	.9824	.9974	1.0129	
$\phi$	1.3247	1.1591	1.0635	.9075	.6711	.4824	.3430	.2604	.2014	.1610	.1255	.1000	.0794	.0624	$\phi$	1.3197	1.1496	1.0507	.8902	.6527	.4665	.3307	.2518	.2040	.1640	.1284	.1029	.0794	.0624	.0484
$\phi_E$	.3696	.3655	.3547	.3044	.2135	.1586	.1429	.1339	.1204	.1029	.0900	.0794	.0700	.0624	$\phi_E$	.3696	.3655	.3547	.3044	.2135	.1586	.1429	.1339	.1204	.1029	.0900	.0794	.0700	.0624	.0484
$\phi_{ef}$	.3502	.3472	.3370	.2877	.1998	.1498	.1349	.1264	.1149	.1029	.0900	.0794	.0700	.0624	$\phi_{ef}$	.3502	.3472	.3370	.2877	.1998	.1498	.1349	.1264	.1149	.1029	.0900	.0794	.0700	.0624	.0484
$\epsilon$	.1948	.1884	.1776	.1546	.1140	.0834	.0600	.0412	.0254	.0118	.0000	.0000	.0000	.0000	$\epsilon$	.1948	.1884	.1776	.1546	.1140	.0834	.0600	.0412	.0254	.0118	.0000	.0000	.0000	.0000	.0000
$\sigma$	2.2727	2.1640	2.0755	1.9350	1.7379	1.6021	1.5004	1.4203	1.3552	1.3009	1.2547	1.2142	1.1959	1.1784	$\sigma$	2.2727	2.1640	2.0755	1.9350	1.7379	1.6021	1.5004	1.4203	1.3552	1.3009	1.2547	1.2142	1.1959	1.1784	.8486
s/c	.4400	.4621	.4818	.5168	.5754	.6242	.6665	.7041	.7379	.7687	.7970	.8236	.8463	.8646	English Units (Inches & Degrees)															
c	3.5300	3.5632	3.5955	3.6553	3.7415	3.8554	3.9405	4.0190	4.0922	4.1610	4.2263	4.2888	4.3194	4.3500	c	3.5300	3.5632	3.5955	3.6553	3.7415	3.8554	3.9405	4.0190	4.0922	4.1610	4.2263	4.2888	4.3194	4.3500	
c <sub>f</sub>	1.8020	1.8454	1.8871	1.9643	2.1001	2.2187	2.3254	2.4232	2.5140	2.5993	2.6799	2.7566	2.7937	2.8299	c <sub>f</sub>	1.8020	1.8454	1.8871	1.9643	2.1001	2.2187	2.3254	2.4232	2.5140	2.5993	2.6799	2.7566	2.7937	2.8299	2.8299
t/c	.0800	.0780	.0764	.0730	.0688	.0642	.0591	.0533	.0479	.0420	.0360	.0300	.0240	.0180	% c to max t	57.600	57.976	58.329	58.978	60.110	61.097	61.986	62.801	63.559	64.272	64.946	65.587	66.200	66.780	66.780
a/c	.5782	.5740	.5734	.5811	.5994	.6078	.6209	.6392	.6555	.6716	.6844	.6952	.7044	.7124	a/c	.5782	.5740	.5734	.5811	.5994	.6078	.6209	.6392	.6555	.6716	.6844	.6952	.7044	.7124	.7124
RLE	.3258	.3212	.3162	.3084	.2847	.2644	.2464	.2304	.2164	.2044	.1944	.1864	.1804	.1764	RLE	.3258	.3212	.3162	.3084	.2847	.2644	.2464	.2304	.2164	.2044	.1944	.1864	.1804	.1764	.1764
RTE	.3258	.3212	.3162	.3084	.2847	.2644	.2464	.2304	.2164	.2044	.1944	.1864	.1804	.1764	RTE	.3258	.3212	.3162	.3084	.2847	.2644	.2464	.2304	.2164	.2044	.1944	.1864	.1804	.1764	.1764
$\beta^*_{1s}$	35.224	35.384	35.334	34.226	38.434	42.474	46.774	50.427	53.628	56.428	58.928	61.128	63.028	64.628	$\beta^*_{1s}$	35.224	35.384	35.334	34.226	38.434	42.474	46.774	50.427	53.628	56.428	58.928	61.128	63.028	64.628	64.628
$\phi$	75.616	65.866	60.201	51.005	37.398	26.740	18.947	14.428	11.228	9.075	7.189	5.628	4.428	3.528	$\phi$	75.616	65.866	60.201	51.005	37.398	26.740	18.947	14.428	11.228	9.075	7.189	5.628	4.428	3.528	3.528
$\phi_E$	21.175	20.944	20.325	17.439	12.231	9.084	8.185	8.015	7.828	7.628	7.428	7.228	7.028	6.828	$\phi_E$	21.175	20.944	20.325	17.439	12.231	9.084	8.185	8.015	7.828	7.628	7.428	7.228	7.028	6.828	6.828
$\phi_f$	20.064	19.893	19.311	16.485	11.450	8.475	7.729	8.500	6.700	4.900	3.100	1.300	.500	.000	$\phi_f$	20.064	19.893	19.311	16.485	11.450	8.475	7.729	8.500	6.700	4.900	3.100	1.300	.500	.000	.000
$\phi_{ef}$	11.163	10.793	10.178	8.860	6.533	4.780	3.439	2.359	1.456	.677	.000	.000	.000	.000	$\phi_{ef}$	11.163	10.793	10.178	8.860	6.533	4.780	3.439	2.359	1.456	.677	.000	.000	.000	.000	.000
$\epsilon$	2.2727	2.1640	2.0755	1.9350	1.7379	1.6021	1.5004	1.4203	1.3552	1.3009	1.2547	1.2142	1.1959	1.1784	$\epsilon$	2.2727	2.1640	2.0755	1.9350	1.7379	1.6021	1.5004	1.4203	1.3552	1.3009	1.2547	1.2142	1.1959	1.1784	1.1784
$\sigma$	.4400	.4621	.4818	.5168	.5754	.6242	.6665	.7041	.7379	.7687	.7970	.8236	.8463	.8646	$\sigma$	.4400	.4621	.4818	.5168	.5754	.6242	.6665	.7041	.7379	.7687	.7970	.8236	.8463	.8646	.8646

# AIRFOIL GEOMETRY ON DESIGN CONICAL SURFACES – STATOR 1

English Units (Inches & Degrees)

c	2.0200	2.0373	2.0517	2.0768	2.0990	2.1193	2.1382	2.1560	2.1728	2.1889	2.2045	2.2123	2.2200
c <sub>f</sub>	.7040	.0587	.6458	.6888	.7155	.7384	.7605	.7881	.8150	.8594	.9462	1.0001	1.1100
1/c	.0044	.0044	.0044	.0044	.0044	.0044	.0044	.0044	.0044	.0044	.0044	.0044	.0044
% to max t	51.100	50.411	50.232	50.072	50.002	50.000	50.000	50.000	50.000	50.000	50.000	50.000	50.000
σ/c	.5478	.5343	.5273	.5150	.5047	.5022	.4985	.4945	.4927	.4849	.4779	.4811	.4909
RLE	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070
RTE	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070	.0070
β <sub>12</sub>	54.882	45.268	41.410	38.199	36.742	35.879	35.429	35.205	35.278	34.039	39.054	41.044	43.801
β <sub>12</sub> <sup>2</sup>	59.212	50.133	46.588	43.839	42.791	42.252	42.121	42.199	42.546	43.544	46.743	48.802	51.586
φ <sup>882</sup>	63.882	49.023	43.423	39.140	37.294	36.095	35.276	34.845	34.808	35.622	39.515	44.065	49.461
φ <sup>8</sup>	61.877	47.966	42.761	38.806	37.093	35.941	35.181	34.775	34.753	35.580	38.485	44.048	49.461
φ <sub>f</sub>	6.949	7.550	8.237	10.252	11.540	12.120	12.583	12.995	13.182	13.356	13.610	21.418	25.098
φ <sub>ef</sub>	5.843	6.977	7.652	10.073	11.409	12.045	12.529	12.954	13.680	15.330	18.790	21.405	25.098
φ <sub>ef</sub>	15.884	10.512	7.801	4.864	3.342	2.476	1.891	1.467	1.203	.988	.688	.410	.000
σ	2.4981	2.3215	2.1691	1.9904	1.8430	1.7271	1.6327	1.5542	1.4872	1.4290	1.3778	1.3341	1.3317
σ/c	4.003	4.308	4.568	.5024	.5426	.5790	.6125	.6434	.6724	.6998	.7258	.7385	.7509

TABLE XXII  
AIRFOIL GEOMETRY ON DESIGN CONICAL SURFACES — ROTOR 2

	HUB	PERCENT FLOW (LE) PERCENT SPAN (AV) PERCENT SPAN (TE)	ROOT										TIP	
			INCHES		METERS			INCHES		METERS				
			INLET DIAMETER =		EXIT DIAMETER =			INLET DIAMETER =		EXIT DIAMETER =				
			MULTIPLE - CIRCULAR - ARC AIRFOILS, 35 BLADES											
			2.50	5.00	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.00	100.00
c	.0859	.0860	.0861	.0863	.0866	.0868	.0871	.0873	.0875	.0877	.0879	.0881	.0882	.0883
c <sub>f</sub>	.0302	.0310	.0317	.0330	.0353	.0373	.0392	.0410	.0427	.0443	.0458	.0473	.0488	.0488
1/c	.0800	.0776	.0755	.0717	.0649	.0588	.0532	.0480	.0437	.0390	.0350	.0300	.0300	.0300
% c to max. t	51.200	51.575	51.915	52.531	53.615	54.585	55.480	56.319	57.115	57.875	58.604	59.314	59.460	60.000
RLE (x 10 <sup>2</sup> )	.5512	.5497	.5470	.5423	.5386	.5340	.5294	.5248	.5204	.5159	.5114	.5069	.5024	.4979
RTE (x 10 <sup>2</sup> )	.0317	.0310	.0305	.0292	.0272	.0254	.0239	.0221	.0205	.0193	.0183	.0178	.0178	.0178
β <sub>1/2</sub>	.8079	.7808	.7815	.7868	.8201	.8616	.8931	.9154	.9407	.9635	.9826	.9994	1.0204	1.0204
β <sub>1/2 ss</sub>	.9367	.9122	.8999	.8965	.9158	.9458	.9675	.9811	.9862	1.0021	1.0214	1.0383	1.0472	1.0593
φ	1.0348	.9076	.7979	.6466	.4844	.3709	.2819	.2219	.1722	.1404	.1184	.1014	.1077	.1494
φ <sub>e</sub>	1.0000	.8744	.7691	.6220	.4647	.3569	.2744	.2141	.1712	.1417	.1190	.1038	.1091	.1494
φ <sub>f</sub>	.1013	.1152	.1284	.1388	.1245	.1069	.0803	.0737	.0226	-.0108	-.0525	-.0635	-.0698	-.0698
φ <sub>ef</sub>	.0801	.0971	.1126	.1261	.1159	.1011	.0767	.0718	.0211	-.0102	-.0542	-.0612	-.0627	-.0698
ε	.2233	.1982	.1779	.1449	.0971	.0435	.0388	.0200	.0055	-.0058	-.0131	-.0080	-.0080	.0000
σ	2.1441	2.0768	2.0186	1.9190	1.7630	1.6415	1.5423	1.4588	1.3877	1.3257	1.2711	1.2219	1.1990	1.1790
s/c	.4664	.4815	.4954	.5211	.5672	.6072	.6484	.6855	.7206	.7543	.7867	.8184	.8340	.8496

	HUB	PERCENT FLOW (LE) PERCENT SPAN (AV) PERCENT SPAN (TE)	English Units (Inches & Degrees)										TIP	
			INCHES		METERS			INCHES		METERS				
			INLET DIAMETER =		EXIT DIAMETER =			INLET DIAMETER =		EXIT DIAMETER =				
			MULTIPLE - CIRCULAR - ARC AIRFOILS, 35 BLADES											
c	3.3820	3.3860	3.3897	3.3922	3.4078	3.4182	3.4277	3.4366	3.4452	3.4534	3.4611	3.4687	3.4760	
c <sub>f</sub>	1.1900	1.2206	1.2485	1.2994	1.3895	1.4702	1.5446	1.6144	1.6805	1.7436	1.8043	1.8630	1.9200	
1/c	.0800	.0776	.0755	.0717	.0649	.0588	.0532	.0480	.0437	.0390	.0350	.0300	.0300	
% c to max. t	51.200	51.575	51.915	52.531	53.615	54.585	55.480	56.319	57.115	57.875	58.604	59.314	59.460	
RLE	.5512	.5497	.5470	.5423	.5386	.5340	.5294	.5248	.5204	.5159	.5114	.5069	.5024	
RTE	.0317	.0310	.0305	.0292	.0272	.0254	.0239	.0221	.0205	.0193	.0183	.0178	.0178	
β <sub>1/2</sub>	80.79	78.08	78.15	78.68	82.01	86.16	89.31	91.54	94.07	96.35	98.26	99.94	102.04	
β <sub>1/2 ss</sub>	93.67	91.22	89.99	89.65	91.58	94.58	96.75	98.11	98.62	100.21	102.14	104.72	105.93	
φ	103.48	90.76	79.79	64.66	48.44	37.09	28.19	22.19	17.22	14.04	11.84	10.14	11.94	
φ <sub>e</sub>	100.00	87.44	76.91	62.20	46.47	35.69	27.44	21.41	17.12	14.17	11.90	10.38	14.94	
φ <sub>f</sub>	10.13	11.52	12.84	13.88	12.45	10.69	8.03	7.37	2.26	-.0108	-.0525	-.0635	-.0698	
φ <sub>ef</sub>	8.01	9.71	11.26	12.61	11.59	10.11	7.67	7.18	2.11	-.0102	-.0542	-.0612	-.0627	
ε	22.33	19.82	17.79	14.49	9.71	4.35	3.88	2.00	0.55	-.0058	-.0131	-.0080	-.0080	
σ	2.1441	2.0768	2.0186	1.9190	1.7630	1.6415	1.5423	1.4588	1.3877	1.3257	1.2711	1.2219	1.1990	
s/c	.4664	.4815	.4954	.5211	.5672	.6072	.6484	.6855	.7206	.7543	.7867	.8184	.8496	

## AIRFOIL GEOMETRY ON DESIGN CONICAL SURFACES – STATOR 2

[illegible]

## APPENDIX D

TABLE XXIV

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

(For Definitions see Figure 26)

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)			
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS	
.0000	-.0131	.0156		.0000	-.0003	.0004		.0000	-.0127	.0150		.0000	-.0003	.0004	
.0107	-.0073	.0245		.0003	-.0002	.0006		.0108	-.0073	.0233		.0003	-.0002	.0006	
.1095	.0459	.1065		.0028	.0012	.0027		.1100	.0421	.0999		.0028	.0011	.0025	
.2190	.1027	.1922		.0056	.0026	.0049		.2201	.0947	.1800		.0056	.0024	.0046	
.3285	.1567	.2721		.0083	.0040	.0069		.3301	.1444	.2547		.0084	.0037	.0065	
.4380	.2079	.3467		.0111	.0053	.0088		.4401	.1913	.3242		.0112	.0049	.0082	
.5475	.2564	.4164		.0139	.0065	.0106		.5501	.2356	.3891		.0140	.0060	.0099	
.6571	.3023	.4814		.0167	.0077	.0122		.6602	.2773	.4495		.0168	.0070	.0114	
.7666	.3455	.5419		.0195	.0088	.0138		.7702	.3164	.5057		.0196	.0080	.0128	
.8761	.3863	.5982		.0223	.0098	.0152		.8802	.3530	.5577		.0224	.0090	.0142	
.9856	.4245	.6505		.0250	.0108	.0165		.9903	.3871	.6058		.0252	.0098	.0154	
1.0951	.4603	.6988		.0278	.0117	.0178		1.1003	.4189	.6501		.0279	.0106	.0165	
1.2046	.4937	.7435		.0306	.0125	.0189		1.2103	.4483	.6909		.0307	.0114	.0175	
1.3141	.5246	.7845		.0334	.0133	.0199		1.3204	.4754	.7281		.0335	.0121	.0185	
1.4236	.5533	.8225		.0362	.0141	.0209		1.4304	.5003	.7622		.0363	.0127	.0194	
1.5331	.5800	.8567		.0389	.0147	.0218		1.5404	.5231	.7928		.0391	.0133	.0201	
1.6426	.6038	.8856		.0417	.0153	.0225		1.6504	.5438	.8198		.0419	.0138	.0208	
1.7522	.6221	.9066		.0445	.0158	.0230		1.7604	.5602	.8401		.0447	.0142	.0213	
1.8617	.6341	.9196		.0473	.0161	.0234		1.8705	.5712	.8532		.0475	.0145	.0217	
1.9712	.6395	.9247		.0501	.0162	.0235		1.9805	.5765	.8589		.0503	.0146	.0218	
2.0807	.6381	.9218		.0528	.0162	.0234		2.0906	.5758	.8571		.0531	.0146	.0218	
2.1902	.6299	.9107		.0556	.0160	.0231		2.2006	.5691	.8478		.0559	.0145	.0215	
2.2997	.6146	.8913		.0584	.0156	.0226		2.3106	.5561	.8305		.0587	.0141	.0211	
2.4092	.5920	.8630		.0612	.0150	.0219		2.4206	.5364	.8049		.0615	.0136	.0204	
2.5187	.5618	.8253		.0640	.0143	.0210		2.5307	.5099	.7705		.0643	.0130	.0196	
2.6282	.5236	.7777		.0668	.0133	.0198		2.6407	.4761	.7261		.0671	.0121	.0185	
2.7377	.4768	.7189		.0695	.0121	.0183		2.7507	.4345	.6725		.0699	.0110	.0171	
2.8473	.4210	.6480		.0723	.0107	.0165		2.8608	.3846	.6066		.0727	.0098	.0154	
2.9568	.3557	.5634		.0751	.0090	.0143		2.9708	.3258	.5278		.0755	.0083	.0134	
3.0663	.2798	.4623		.0779	.0071	.0117		3.0808	.2571	.4331		.0783	.0065	.0110	
3.1758	.1933	.3453		.0807	.0049	.0088		3.1909	.1782	.3222		.0810	.0045	.0082	
3.2853	.0940	.2017		.0834	.0024	.0051		3.3009	.0873	.1857		.0838	.0022	.0047	
3.3861	-.0096	.0444		.0860	-.0002	.0011		3.4030	-.0073	.0353		.0864	-.0002	.0009	
3.4948	-.0185	.0308		.0882	-.0005	.0008		3.4109	-.0149	.0235		.0866	-.0004	.0006	
RADIUS (INCHES) = 6.574				RADIUS (METERS) = .1670				RADIUS (INCHES) = 6.913				RADIUS (METERS) = .1756			
CHORD (INCHES) = 3.395				CHORD (METERS) = .0862				CHORD (INCHES) = 3.411				CHORD (METERS) = .0866			
ZCSL (INCHES) = 1.8005				ZCSL (METERS) = .0457				ZCSL (INCHES) = 1.8133				ZCSL (METERS) = .0461			
YCSL (INCHES) = .5938				YCSL (METERS) = .0151				YCSL (INCHES) = .5483				YCSL (METERS) = .0139			
RLE (INCHES) = .0130				RLE (METERS) = .000330				RLE (INCHES) = .0129				RLE (METERS) = .000328			
RTE (INCHES) = .0164				RTE (METERS) = .000417				RTE (INCHES) = .0136				RTE (METERS) = .000345			
X-AREA (SQ. IN.) = .7238				X-AREA (SQ. METERS) = .000467				X-AREA (SQ. IN.) = .7090				X-AREA (SQ. METERS) = .000457			
GAMMA-CHORD (DEG.) = -1.79				GAMMA-CHORD (RAD.) = -.0313				GAMMA-CHORD (DEG.) = .62				GAMMA-CHORD (RAD.) = .0108			

# AIRFOIL COORDINATES ON MANUFACTURING SURFACES – ROTOR 1

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)			
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS	
.0000	-.0123	.0143		.0000	-.0003	.0004		.0000	-.0122	.0141		.0000	-.0003	.0004	
.0108	-.0074	.0221		.0003	-.0002	.0006		.0108	-.0073	.0216		.0003	-.0002	.0005	
.1110	.0389	.0942		.0028	.0010	.0024		.1115	.0380	.0923		.0028	.0010	.0023	
.1694	.0078	.1694		.0056	.0022	.0043		.2230	.0053	.1656		.0057	.0022	.0042	
.2320	.1340	.2396		.0085	.0034	.0061		.3345	.0238	.2338		.0085	.0033	.0059	
.3048	.1774	.3048		.0113	.0045	.0077		.4460	.1719	.2973		.0113	.0044	.0076	
.3655	.2182	.3655		.0141	.0055	.0093		.5575	.2112	.3564		.0142	.0054	.0091	
.4218	.2563	.4218		.0169	.0065	.0107		.6690	.2480	.4113		.0170	.0063	.0104	
.4739	.2919	.4739		.0197	.0074	.0120		.7805	.2622	.4620		.0198	.0072	.0117	
.5221	.3249	.5221		.0226	.0083	.0133		.8921	.3139	.5088		.0227	.0080	.0129	
.5663	.3555	.5663		.0254	.0090	.0144						.0255	.0087	.0140	
.6068	.3835	.6068		.0282	.0097	.0154		1.0036	.3432	.5517		.0283	.0094	.0150	
.6437	.4091	.6437		.0310	.0104	.0164		1.1151	.3700	.5909		.0312	.0100	.0159	
.6770	.4323	.6770		.0338	.0110	.0172		1.2266	.3944	.6264		.0340	.0106	.0167	
.7071	.4533	.7071		.0367	.0115	.0180		1.3381	.4163	.6587		.0368	.0111	.0175	
.7340	.4719	.7340		.0395	.0120	.0186		1.4496	.4359	.6874		.0397	.0115	.0181	
.7578	.4888	.7578		.0423	.0124	.0192		1.5611	.4531	.7128		.0425	.0119	.0187	
.7765	.5022	.7765		.0451	.0128	.0197		1.6726	.4683	.7351		.0453	.0122	.0191	
.7888	.5113	.7888		.0479	.0130	.0200		1.7841	.4804	.7528		.0481	.0124	.0194	
.7942	.5155	.7942		.0508	.0131	.0202		1.8956	.4884	.7642		.0510	.0125	.0195	
.7927	.5145	.7927		.0536	.0131	.0201		2.0071	.4917	.7790		.0538	.0125	.0195	
.7840	.5082	.7840		.0564	.0129	.0199		2.1186	.4902	.7870		.0566	.0123	.0193	
.7680	.4984	.7680		.0592	.0126	.0195		2.2301	.4838	.7963		.0595	.0120	.0189	
.7442	.4787	.7442		.0620	.0122	.0189		2.3416	.4722	.7925		.0623	.0116	.0183	
.7122	.4550	.7122		.0649	.0116	.0181		2.4531	.4551	.7191		.0651	.0110	.0175	
.6713	.4248	.6713		.0677	.0108	.0171		2.5647	.4323	.6878		.0680	.0102	.0165	
.6208	.3879	.6208		.0705	.0099	.0158		2.6762	.4034	.6480		.0708	.0093	.0152	
.5598	.3436	.5598		.0733	.0087	.0142		2.7877	.3680	.5988		.0736	.0083	.0137	
.4866	.2913	.4866		.0761	.0074	.0124		2.8992	.3257	.5394		.0765	.0070	.0119	
.3991	.2303	.3991		.0790	.0059	.0101		3.0107	.2759	.4683		.0793	.0055	.0097	
.2954	.1599	.2954		.0818	.0041	.0075		3.1222	.2179	.3835		.0821	.0038	.0072	
.1692	.0784	.1692		.0846	.0020	.0043		3.2337	.1509	.2831		.0850	.0019	.0041	
.0294	-.0063	.0294		.0872	-.0002	.0007		3.3452	.0738	.1618		.0874	-.0002	.0007	
.0190	-.0017	.0190		.0874	-.0003	.0005		3.4488	-.0042	.0242		.0878	-.0003	.0005	
								3.4567	-.0123	.0180					

TABLE XXIV (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0119	.0136	.0000	-.0003	.0003	.0000	-.0116	.0132	.0000	-.0003	.0003
.0108	-.0074	.0208	.0003	-.0002	.0005	.0107	-.0074	.0200	.0003	-.0002	.0005
.1123	.0355	.0885	.0029	.0009	.0022	.1131	.0333	.0850	.0029	.0008	.0022
.2247	.0809	.1592	.0057	.0021	.0040	.2262	.0762	.1528	.0057	.0019	.0039
.3370	.1236	.2252	.0086	.0031	.0057	.3393	.1168	.2163	.0086	.0030	.0055
.4493	.1639	.2868	.0114	.0042	.0073	.4524	.1550	.2755	.0115	.0039	.0070
.5617	.2017	.3440	.0143	.0051	.0087	.5655	.1909	.3307	.0144	.0048	.0084
.6740	.2370	.3972	.0171	.0060	.0101	.6786	.2244	.3819	.0172	.0057	.0097
.7863	.2698	.4464	.0200	.0069	.0113	.7917	.2556	.4294	.0201	.0065	.0109
.8987	.3001	.4917	.0228	.0076	.0125	.9048	.2845	.4732	.0230	.0072	.0120
1.0110	.3280	.5332	.0257	.0083	.0135	1.0179	.3111	.5133	.0259	.0079	.0130
1.1233	.3534	.5710	.0285	.0090	.0145	1.1311	.3353	.5500	.0287	.0085	.0140
1.2357	.3760	.6050	.0314	.0096	.0154	1.2442	.3572	.5832	.0316	.0091	.0148
1.3480	.3963	.6355	.0342	.0101	.0161	1.3573	.3768	.6129	.0345	.0096	.0156
1.4603	.4141	.6625	.0371	.0105	.0168	1.4700	.3940	.6393	.0373	.0100	.0162
1.5727	.4296	.6863	.0399	.0109	.0174	1.5835	.4088	.6624	.0402	.0104	.0168
1.6850	.4431	.7069	.0428	.0113	.0180	1.6966	.4215	.6823	.0431	.0107	.0173
1.7973	.4536	.7235	.0457	.0115	.0184	1.8097	.4313	.6984	.0460	.0110	.0177
1.9097	.4604	.7341	.0485	.0117	.0186	1.9228	.4377	.7091	.0488	.0111	.0180
2.0220	.4628	.7383	.0514	.0118	.0188	2.0359	.4397	.7133	.0517	.0112	.0181
2.1343	.4604	.7358	.0542	.0117	.0187	2.1490	.4372	.7108	.0546	.0111	.0181
2.2467	.4533	.7266	.0571	.0115	.0185	2.2621	.4299	.7016	.0575	.0109	.0178
2.3590	.4413	.7104	.0599	.0112	.0180	2.3752	.4180	.6856	.0603	.0106	.0174
2.4713	.4242	.6869	.0628	.0108	.0174	2.4883	.4014	.6624	.0632	.0102	.0168
2.5837	.4018	.6557	.0656	.0102	.0167	2.6014	.3796	.6319	.0661	.0096	.0160
2.6960	.3738	.6164	.0685	.0095	.0157	2.7145	.3526	.5933	.0689	.0090	.0151
2.8084	.3401	.5683	.0713	.0086	.0144	2.8276	.3201	.5462	.0718	.0081	.0139
2.9207	.3001	.5106	.0742	.0076	.0130	2.9407	.2817	.4898	.0747	.0072	.0124
3.0330	.2536	.4421	.0770	.0064	.0112	3.0539	.2372	.4229	.0776	.0060	.0107
3.1454	.2000	.3613	.0799	.0051	.0092	3.1670	.1860	.3443	.0804	.0047	.0087
3.2577	.1381	.2658	.0827	.0035	.0068	3.2801	.1276	.2522	.0833	.0032	.0064
3.3700	.0672	.1517	.0856	.0017	.0039	3.3932	.0615	.1434	.0862	.0016	.0036
3.4739	-.0042	.0275	.0882	-.0002	.0007	3.4974	-.0062	.0266	.0888	-.0002	.0007
3.4824	-.0142	.0174	.0885	-.0003	.0004	3.5063	-.0119	.0166	.0891	-.0003	.0004
RADIUS (INCHES)	7.592		RADIUS (METERS)	.1928		RADIUS (INCHES)	7.792		RADIUS (METERS)	.1979	
CHORD (INCHES)	3.482		CHORD (METERS)	.0885		CHORD (INCHES)	3.506		CHORD (METERS)	.0891	
ZCSL (INCHES)	1.8569		ZCSL (METERS)	.0472		ZCSL (INCHES)	1.8717		ZCSL (METERS)	.0475	
YCSL (INCHES)	.4616		YCSL (METERS)	.0117		YCSL (INCHES)	.4414		YCSL (METERS)	.0112	
RLE (INCHES)	.0123		RLE (METERS)	.000312		RLE (INCHES)	.0121		RLE (METERS)	.000307	
RTE (INCHES)	.0121		RTE (METERS)	.000307		RTE (INCHES)	.0122		RTE (METERS)	.000310	
X-AREA (SQ. IN.)	.6877		X-AREA (SQ. METERS)	.000444		X-AREA (SQ. IN.)	.6841		X-AREA (SQ. METERS)	.000441	
GAMMA-CHORD(DEG.)	6.96		GAMMA-CHORD(RAD.)	.1215		GAMMA-CHORD(DEG.)	8.82		GAMMA-CHORD(RAD.)	.1539	

TABLE XXIV (Cont'd)  
AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)			
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS	
.0000	-.0114	.0128		.0000	-.0003	.0003		.0000	-.0110	.0123		.0000	-.0003	.0003	
.0107	-.0074	.0193		.0003	-.0002	.0005		.0106	-.0075	.0182		.0003	-.0002	.0005	
.1139	.0311	.0817		.0029	.0008	.0021		.1151	.0274	.0764		.0029	.0007	.0019	
.2277	.0717	.1467		.0058	.0018	.0037		.2301	.0643	.1371		.0058	.0016	.0035	
.3416	.1101	.2076		.0087	.0028	.0053		.3452	.0992	.1941		.0088	.0025	.0049	
.4555	.1463	.2645		.0116	.0037	.0067		.4603	.1321	.2474		.0117	.0034	.0063	
.5693	.1803	.3177		.0145	.0046	.0081		.5753	.1632	.2973		.0146	.0041	.0076	
.6832	.2121	.3671		.0174	.0054	.0093		.6904	.1923	.3438		.0175	.0049	.0087	
.7971	.2418	.4129		.0202	.0061	.0105		.8054	.2194	.3870		.0205	.0056	.0098	
.9109	.2692	.4552		.0231	.0068	.0116		.9205	.2446	.4269		.0234	.0062	.0108	
1.0248	.2945	.4940		.0260	.0075	.0125		1.0356	.2678	.4635		.0263	.0068	.0118	
1.1387	.3176	.5295		.0289	.0081	.0134		1.1506	.2890	.4970		.0292	.0073	.0126	
1.2525	.3385	.5616		.0318	.0086	.0143		1.2657	.3082	.5274		.0321	.0078	.0134	
1.3664	.3571	.5905		.0347	.0091	.0150		1.2808	.3253	.5547		.0351	.0083	.0141	
1.4803	.3735	.6160		.0376	.0095	.0156		1.4958	.3404	.5790		.0380	.0086	.0147	
1.5941	.3877	.6385		.0405	.0098	.0162		1.6109	.3534	.6002		.0409	.0090	.0152	
1.7080	.3998	.6578		.0434	.0102	.0167		1.6260	.3645	.6186		.0438	.0093	.0157	
1.8219	.4094	.6739		.0463	.0104	.0171		1.7410	.3734	.6341		.0468	.0095	.0161	
1.9358	.4158	.6846		.0492	.0106	.0174		1.9561	.3796	.6447		.0497	.0096	.0164	
2.0496	.4181	.6892		.0521	.0106	.0175		2.0712	.3821	.6497		.0526	.0097	.0165	
2.1635	.4160	.6872		.0550	.0106	.0175		2.1862	.3805	.6484		.0555	.0097	.0165	
2.2774	.4094	.6788		.0578	.0104	.0172		2.3013	.3747	.6408		.0585	.0095	.0163	
2.3912	.3982	.6635		.0607	.0101	.0169		2.4164	.3647	.6266		.0614	.0093	.0159	
2.5051	.3823	.6412		.0636	.0097	.0163		2.5314	.3502	.6056		.0643	.0089	.0154	
2.6190	.3615	.6115		.0665	.0092	.0155		2.6465	.3312	.5776		.0672	.0084	.0147	
2.7328	.3356	.5740		.0694	.0085	.0146		2.7615	.3076	.5421		.0701	.0078	.0138	
2.8467	.3043	.5281		.0723	.0077	.0134		2.8766	.2790	.4986		.0731	.0071	.0127	
2.9606	.2675	.4730		.0752	.0068	.0120		2.9917	.2452	.4464		.0760	.0062	.0113	
3.0744	.2248	.4079		.0781	.0057	.0104		3.1067	.2061	.3847		.0789	.0052	.0098	
3.1883	.1759	.3314		.0810	.0045	.0084		3.2218	.1612	.3124		.0818	.0041	.0079	
3.3022	.1202	.2422		.0839	.0031	.0062		3.3369	.1102	.2281		.0848	.0028	.0058	
3.4161	.0576	.1374		.0868	.0015	.0035		3.4519	.0526	.1293		.0877	.0013	.0033	
3.5299	-.0062	.0257		.0894	-.0002	.0007		3.5578	-.0061	.0241		.0904	-.0002	.0006	
				.0897	-.0003	.0004		3.5670	-.0112	.0149		.0906	-.0003	.0004	
RADIUS (INCHES)	7.991			RADIUS (METERS)	.2030			RADIUS (INCHES)	8.290			RADIUS (METERS)	.2106		
CHORD (INCHES)	3.530			CHORD (METERS)	.0897			CHORD (INCHES)	3.567			CHORD (METERS)	.0906		
ZCSL (INCHES)	1.8857			ZCSL (INCHES)	.0479			ZCSL (INCHES)	1.9065			ZCSL (METERS)	.0484		
YCSL (INCHES)	.4225			YCSL (METERS)	.0107			YCSL (INCHES)	.3919			YCSL (METERS)	.0100		
RLE (INCHES)	.0119			RLE (METERS)	.000302			RLE (INCHES)	.0117			RLE (METERS)	.000297		
RTE (INCHES)	.0121			RTE (METERS)	.000307			RTE (INCHES)	.0118			RTE (METERS)	.000300		
X-AREA (SQ. IN.)	.6802			X-AREA (SQ. METERS)	.000439			X-AREA (SQ. IN.)	.6749			X-AREA (SQ. METERS)	.000435		
GAMMA-CHORD( DEG.)	10.45			GAMMA-CHORD( DEG.)	.1858			GAMMA-CHORD( DEG.)	13.46			GAMMA-CHORD( DEG.)	.2348		

TABLE XXIV (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0108	.0120	.0000	-.0003	.0003	.0000	-.0107	.0117	.0000	-.0003	.0003
.0106	-.0076	.0176	.0003	-.0002	.0004	.0106	-.0076	.0170	.0003	-.0002	.0004
.1159	.0249	.0729	.0029	.0006	.0019	.1167	.0226	.0697	.0030	.0004	.0018
.2318	.0593	.1309	.0059	.0015	.0033	.2334	.0546	.1250	.0059	.0014	.0032
.3476	.0918	.1853	.0088	.0023	.0047	.3501	.0849	.1770	.0089	.0022	.0045
.4635	.1226	.2364	.0118	.0031	.0060	.4668	.1136	.2258	.0119	.0029	.0057
.5794	.1516	.2841	.0147	.0039	.0072	.5835	.1406	.2715	.0148	.0036	.0069
.6953	.1788	.3287	.0177	.0045	.0083	.7002	.1659	.3141	.0178	.0042	.0080
.8112	.2042	.3701	.0206	.0052	.0094	.8169	.1896	.3538	.0207	.0048	.0090
.9271	.2277	.4084	.0235	.0058	.0104	.9336	.2116	.3905	.0237	.0054	.0099
1.0429	.2495	.4436	.0265	.0063	.0113	1.0503	.2319	.4244	.0267	.0059	.0108
1.1588	.2694	.4758	.0294	.0068	.0121	1.1670	.2504	.4553	.0296	.0064	.0116
1.2747	.2874	.5051	.0324	.0073	.0128	1.2837	.2673	.4834	.0326	.0068	.0123
1.3906	.3035	.5314	.0353	.0077	.0135	1.4004	.2824	.5087	.0356	.0072	.0129
1.5065	.3178	.5547	.0383	.0081	.0141	1.5171	.2957	.5312	.0385	.0075	.0135
1.6224	.3301	.5752	.0412	.0084	.0146	1.6338	.3073	.5510	.0415	.0078	.0140
1.7382	.3406	.5929	.0442	.0087	.0151	1.7505	.3171	.5680	.0445	.0081	.0144
1.8541	.3490	.6079	.0471	.0089	.0154	1.8672	.3250	.5827	.0474	.0083	.0148
1.9700	.3551	.6185	.0500	.0090	.0157	1.9839	.3309	.5931	.0504	.0084	.0151
2.0859	.3577	.6237	.0530	.0091	.0158	2.1006	.3336	.5986	.0534	.0085	.0152
2.2018	.3564	.6227	.0559	.0091	.0158	2.2173	.3325	.5979	.0563	.0084	.0152
2.3177	.3512	.6154	.0589	.0089	.0156	2.3339	.3277	.5911	.0593	.0083	.0150
2.4335	.3419	.6018	.0618	.0087	.0153	2.4506	.3190	.5780	.0622	.0081	.0147
2.5494	.3284	.5816	.0648	.0083	.0148	2.5673	.3063	.5585	.0652	.0078	.0142
2.6653	.3105	.5546	.0677	.0079	.0141	2.6840	.2895	.5322	.0682	.0074	.0135
2.7812	.2883	.5203	.0706	.0073	.0132	2.8007	.2685	.4989	.0711	.0068	.0127
2.8971	.2614	.4784	.0736	.0066	.0122	2.9174	.2432	.4582	.0741	.0062	.0116
3.0129	.2297	.4280	.0765	.0058	.0109	3.0341	.2134	.4094	.0771	.0054	.0104
3.1288	.1929	.3686	.0795	.0049	.0094	3.1508	.1788	.3520	.0800	.0045	.0089
3.2447	.1507	.2991	.0824	.0038	.0076	3.2675	.1394	.2850	.0830	.0035	.0072
3.3606	.1029	.2181	.0854	.0026	.0055	3.3842	.0947	.2074	.0860	.0024	.0053
3.4765	.0488	.1237	.0883	.0012	.0031	3.5009	.0446	.1175	.0889	.0011	.0030
3.5930	-.0061	.0233	.0910	-.0002	.0006	3.6080	-.0062	.0226	.0916	-.0002	.0006
3.5924	-.0110	.0145	.0912	-.0003	.0004	3.6176	-.0108	.0140	.0919	-.0003	.0004
RADIUS (INCHES) = 8.490			RADIUS (METERS) = .2156			RADIUS (INCHES) = 8.690			RADIUS (METERS) = .2207		
CHORD (INCHES) = 3.592			CHORD (METERS) = .0912			CHORD (INCHES) = 3.618			CHORD (METERS) = .0919		
ZCSSL (INCHES) = 1.9194			ZCSSL (METERS) = .0488			ZCSSL (INCHES) = 1.9330			ZCSSL (METERS) = .0491		
YCSSL (INCHES) = .3712			YCSSL (METERS) = .0094			YCSSL (INCHES) = .3509			YCSSL (METERS) = .0089		
RLE (INCHES) = .0115			RLE (METERS) = .000292			RLE (INCHES) = .0114			RLE (METERS) = .000290		
RTE (INCHES) = .0118			RTE (METERS) = .000300			RTE (INCHES) = .0118			RTE (METERS) = .000300		
X-AREA (SQ. IN.) = .6730			X-AREA (SQ. METERS) = .000434			X-AREA (SQ. IN.) = .6723			X-AREA (SQ. METERS) = .000434		
GAMMA-CHORD(DEG.) = 15.30			GAMMA-CHORD(RAD.) = .2670			GAMMA-CHORD(DEG.) = 17.01			GAMMA-CHORD(RAD.) = .2968		

TABLE XXIV (Cont'd)  
AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0104	.0113	.0000	-.0003	.0003	.0000	-.0101	.0109	.0000	-.0003	.0003
.0105	-.0077	.0162	.0003	-.0002	.0004	.0104	-.0078	.0153	.0003	-.0002	.0004
.1178	.0195	.0654	.0030	.0005	.0017	.1189	.0167	.0614	.0030	.0004	.0016
.2356	.0483	.1171	.0060	.0012	.0030	.2378	.0424	.1096	.0060	.0011	.0028
.3533	.0756	.1657	.0090	.0016	.0042	.3567	.0667	.1550	.0091	.0017	.0039
.4711	.1014	.2114	.0120	.0026	.0054	.4756	.0898	.1978	.0121	.0023	.0050
.5889	.1257	.2543	.0150	.0032	.0065	.5945	.1116	.2379	.0151	.0028	.0060
.7067	.1484	.2943	.0179	.0038	.0075	.7134	.1320	.2754	.0181	.0034	.0070
.8244	.1699	.3316	.0209	.0043	.0084	.8322	.1511	.3104	.0211	.0038	.0079
.9422	.1898	.3662	.0239	.0048	.0093	.9511	.1689	.3428	.0242	.0043	.0087
1.0600	.2081	.3981	.0269	.0053	.0101	1.0700	.1853	.3727	.0272	.0047	.0095
1.1778	.2249	.4273	.0299	.0057	.0109	1.1889	.2003	.4001	.0302	.0051	.0102
1.2956	.2402	.4538	.0329	.0061	.0115	1.3078	.2140	.4251	.0332	.0054	.0108
1.4133	.2539	.4778	.0359	.0064	.0121	1.4267	.2263	.4476	.0362	.0057	.0114
1.5311	.2660	.4992	.0389	.0068	.0127	1.5456	.2372	.4677	.0393	.0060	.0119
1.6489	.2766	.5180	.0419	.0070	.0132	1.6645	.2467	.4854	.0423	.0063	.0123
1.7667	.2856	.5347	.0449	.0073	.0136	1.7834	.2548	.5008	.0453	.0065	.0127
1.8844	.2929	.5483	.0479	.0074	.0139	1.9023	.2615	.5141	.0483	.0066	.0131
2.0022	.2987	.5587	.0509	.0076	.0142	2.0212	.2668	.5243	.0513	.0068	.0133
2.1200	.3015	.5646	.0538	.0077	.0143	2.1401	.2696	.5304	.0544	.0068	.0135
2.2378	.3010	.5646	.0568	.0076	.0143	2.2590	.2694	.5309	.0574	.0068	.0135
2.3556	.2969	.5587	.0598	.0075	.0142	2.3778	.2660	.5257	.0604	.0068	.0134
2.4733	.2893	.5467	.0628	.0073	.0139	2.4967	.2593	.5147	.0634	.0066	.0131
2.5911	.2780	.5285	.0658	.0071	.0134	2.6156	.2492	.4976	.0664	.0063	.0126
2.7089	.2629	.5038	.0688	.0067	.0128	2.7345	.2357	.4744	.0695	.0060	.0120
2.8267	.2439	.4723	.0718	.0062	.0120	2.8534	.2187	.4447	.0725	.0056	.0113
2.9445	.2209	.4337	.0748	.0056	.0110	2.9723	.1980	.4082	.0755	.0050	.0104
3.0622	.1938	.3875	.0778	.0049	.0098	3.0912	.1736	.3645	.0785	.0044	.0093
3.1800	.1624	.3331	.0808	.0041	.0085	3.2101	.1453	.3130	.0815	.0037	.0080
3.2978	.1264	.2696	.0838	.0032	.0068	3.3290	.1129	.2531	.0846	.0029	.0064
3.4156	.0857	.1961	.0868	.0022	.0050	3.4479	.0762	.1839	.0876	.0019	.0047
3.5334	.0399	.1112	.0897	.0010	.0028	3.5668	.0350	.1042	.0906	.0009	.0026
3.6511	-.0064	.0217	.0925	-.0002	.0006	3.6756	-.0065	.0207	.0934	-.0002	.0005
			.0927	-.0003	.0003	3.6857	-.0104	.0130	.0936	-.0003	.0003
RADIUS (INCHES)	8.989		RADIUS (METERS)	.2283		RADIUS (INCHES)	9.288		RADIUS (METERS)	.2359	
CHORD (INCHES)	3.451		CHORD (METERS)	.0927		CHORD (INCHES)	3.686		CHORD (METERS)	.0936	
ZC SL (INCHES)	1.9528		ZC SL (METERS)	.0496		ZC SL (INCHES)	1.9718		ZC SL (METERS)	.0501	
YCSL (INCHES)	.3236		YCSL (METERS)	.0082		YCSL (INCHES)	.2964		YCSL (METERS)	.0075	
RLE (INCHES)	.0112		RLE (METERS)	.00284		RLE (INCHES)	.0110		RLE (METERS)	.00279	
RTE (INCHES)	.0118		RTE (METERS)	.00300		RTE (INCHES)	.0117		RTE (METERS)	.00297	
X-AREA (SQ. IN.)	.6709		X-AREA (SQ. METERS)	.000433		X-AREA (SQ. IN.)	.6686		X-AREA (SQ. METERS)	.000431	
GAMMA-CHORD (DEG.)	19.67		GAMMA-CHORD (RAD.)	.3433		GAMMA-CHORD (DEG.)	22.22		GAMMA-CHORD (RAD.)	.3878	

TABLE XXIV (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0098	.0104	.0000	-.0002	.0003	.0000	-.0096	.0101	.0000	-.0002	.0003
.0102	-.0079	.0143	.0003	-.0002	.0004	.0101	-.0079	.0136	.0003	-.0002	.0003
.1203	.0131	.0563	.0031	.0003	.0014	.1214	.0104	.0526	.0031	.0003	.0013
.2007	.0350	.1002	.0061	.0009	.0025	.2428	.0296	.0934	.0062	.0008	.0024
.3610	.0558	.1416	.0092	.0014	.0036	.3641	.0477	.1318	.0092	.0012	.0033
.4814	.0755	.1806	.0122	.0019	.0046	.4855	.0649	.1680	.0123	.0016	.0043
.6017	.0940	.2173	.0153	.0024	.0055	.6069	.0810	.2020	.0154	.0021	.0051
.7221	.1114	.2515	.0183	.0028	.0064	.7283	.0962	.2338	.0185	.0024	.0059
.8424	.1277	.2835	.0214	.0032	.0072	.8497	.1104	.2635	.0216	.0028	.0067
.9628	.1428	.3132	.0245	.0036	.0080	.9710	.1235	.2910	.0247	.0031	.0074
1.0831	.1568	.3406	.0275	.0040	.0087	1.0924	.1356	.3164	.0277	.0034	.0080
1.2035	.1696	.3657	.0306	.0043	.0093	1.2138	.1467	.3397	.0308	.0037	.0086
1.3238	.1813	.3886	.0336	.0046	.0099	1.3352	.1568	.3610	.0339	.0040	.0092
1.4442	.1917	.4092	.0367	.0049	.0104	1.4566	.1658	.3802	.0370	.0042	.0097
1.5645	.2010	.4277	.0397	.0051	.0109	1.5779	.1739	.3973	.0401	.0044	.0101
1.6849	.2090	.4439	.0428	.0053	.0113	1.6993	.1808	.4124	.0432	.0046	.0105
1.8052	.2159	.4579	.0459	.0055	.0116	1.8207	.1868	.4255	.0462	.0047	.0108
1.9256	.2215	.4702	.0489	.0056	.0119	1.9421	.1916	.4369	.0493	.0049	.0111
2.0459	.2261	.4796	.0520	.0057	.0122	2.0635	.1957	.4458	.0524	.0050	.0113
2.1663	.2286	.4858	.0550	.0058	.0123	2.1848	.1980	.4520	.0555	.0050	.0115
2.2866	.2284	.4868	.0581	.0058	.0124	2.3062	.1982	.4534	.0586	.0050	.0115
2.4070	.2257	.4823	.0611	.0057	.0122	2.4276	.1959	.4496	.0617	.0050	.0114
2.5273	.2200	.4722	.0642	.0056	.0120	2.5490	.1911	.4404	.0647	.0049	.0112
2.6477	.2114	.4565	.0673	.0054	.0116	2.6704	.1837	.4259	.0678	.0047	.0108
2.7680	.1999	.4350	.0703	.0051	.0110	2.7917	.1736	.4059	.0709	.0044	.0103
2.8884	.1853	.4075	.0734	.0047	.0103	2.9131	.1609	.3801	.0740	.0041	.0097
3.0087	.1676	.3737	.0764	.0043	.0095	3.0345	.1454	.3484	.0771	.0037	.0089
3.1291	.1466	.3332	.0795	.0037	.0085	3.1559	.1270	.3105	.0802	.0032	.0079
3.2494	.1224	.2857	.0825	.0031	.0073	3.2773	.1058	.2640	.0832	.0027	.0068
3.3698	.0948	.2306	.0856	.0024	.0059	3.3986	.0816	.2144	.0863	.0021	.0054
3.4901	.0636	.1672	.0886	.0016	.0042	3.5200	.0543	.1552	.0894	.0014	.0039
3.6105	.0287	.0945	.0917	.0007	.0024	3.6414	.0237	.0876	.0925	.0006	.0022
3.7308	-.0066	.0188	.0945	-.0002	.0005	3.7527	-.0068	.0179	.0953	-.0002	.0005
3.7308	-.0068	.0120	.0948	-.0002	.0003	3.7628	-.0096	.0115	.0956	-.0002	.0003
RADIUS (INCHES) = 9.688			RADIUS (METERS) = .2461			RADIUS (INCHES) = 9.987			RADIUS (METERS) = .2537		
CHORD (INCHES) = 3.731			CHORD (METERS) = .0948			CHORD (INCHES) = 3.763			CHORD (METERS) = .0956		
ZCSSL (INCHES) = 1.9956			ZCSSL (METERS) = .0507			ZCSSL (INCHES) = 2.0129			ZCSSL (METERS) = .0511		
YCSL (INCHES) = .2609			YCSL (METERS) = .0066			YCSL (INCHES) = .2344			YCSL (METERS) = .0060		
RLE (INCHES) = .0106			RLE (METERS) = .000269			RLE (INCHES) = .0104			RLE (METERS) = .000264		
RTE (INCHES) = .0113			RTE (METERS) = .000287			RTE (INCHES) = .0111			RTE (METERS) = .000282		
X-AREA (SQ. IN.) = .6639			X-AREA(SQ.METERS) = .000428			X-AREA (SQ. IN.) = .6594			X-AREA(SQ.METERS) = .000425		
GAMMA-CHORD(DEC.) = 25.43			GAMMA-CHORD(RAD.) = .4438			GAMMA-CHORD(DEC.) = 27.75			GAMMA-CHORD(RAD.) = .4843		

TABLE XXIV (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0093	.0098	.0000	-.0002	.0002	.0000	-.0090	.0094	.0000	-.0002	.0002
.0099	-.0079	.0130	.0003	-.0002	.0003	.0096	-.0078	.0122	.0002	-.0002	.0003
.1224	.0081	.0493	.0031	.0002	.0013	.1237	.0057	.0458	.0031	.0001	.0012
.2448	.0247	.0872	.0062	.0006	.0022	.2475	.0196	.0805	.0063	.0005	.0020
.3672	.0405	.1229	.0093	.0010	.0031	.3712	.0328	.1132	.0094	.0008	.0029
.4896	.0553	.1565	.0124	.0014	.0040	.4950	.0451	.1440	.0126	.0011	.0037
.6120	.0693	.1881	.0155	.0018	.0048	.6187	.0567	.1729	.0157	.0014	.0044
.7344	.0824	.2176	.0187	.0021	.0055	.7425	.0674	.1998	.0189	.0017	.0051
.8568	.0945	.2451	.0218	.0024	.0062	.8662	.0773	.2248	.0220	.0020	.0057
.9792	.1058	.2706	.0249	.0027	.0069	.9899	.0864	.2480	.0251	.0022	.0063
1.1016	.1162	.2941	.0280	.0030	.0075	1.1137	.0947	.2693	.0283	.0024	.0068
1.2240	.1256	.3157	.0311	.0032	.0080	1.2374	.1022	.2887	.0314	.0026	.0073
1.3464	.1342	.3353	.0342	.0034	.0085	1.3612	.1089	.3063	.0346	.0028	.0078
1.4688	.1418	.3531	.0373	.0036	.0090	1.4849	.1148	.3221	.0377	.0029	.0082
1.5912	.1486	.3689	.0404	.0038	.0094	1.6087	.1199	.3362	.0409	.0030	.0085
1.7136	.1544	.3828	.0435	.0039	.0097	1.7324	.1243	.3484	.0440	.0032	.0088
1.8360	.1594	.3948	.0466	.0040	.0100	1.8562	.1278	.3589	.0471	.0032	.0091
1.9584	.1634	.4051	.0497	.0041	.0103	1.9799	.1305	.3677	.0503	.0033	.0093
2.0808	.1666	.4133	.0529	.0042	.0105	2.1036	.1326	.3747	.0534	.0034	.0095
2.2032	.1686	.4192	.0560	.0043	.0106	2.2274	.1337	.3798	.0566	.0034	.0096
2.3256	.1688	.4208	.0591	.0043	.0107	2.3511	.1334	.3812	.0597	.0034	.0097
2.4480	.1668	.4174	.0622	.0042	.0106	2.4749	.1315	.3780	.0629	.0033	.0096
2.5704	.1627	.4090	.0653	.0041	.0104	2.5986	.1279	.3702	.0660	.0032	.0094
2.6929	.1563	.3955	.0684	.0040	.0100	2.7224	.1225	.3577	.0691	.0031	.0091
2.8152	.1476	.3768	.0715	.0037	.0096	2.8461	.1153	.3405	.0723	.0029	.0086
2.9377	.1366	.3527	.0746	.0035	.0090	2.9699	.1064	.3184	.0754	.0027	.0081
3.0600	.1233	.3232	.0777	.0031	.0082	3.0936	.0956	.2913	.0786	.0024	.0074
3.1825	.1075	.2878	.0808	.0027	.0073	3.2173	.0830	.2590	.0817	.0021	.0066
3.3049	.0893	.2463	.0839	.0023	.0063	3.3411	.0685	.2213	.0849	.0017	.0056
3.4273	.0685	.1983	.0871	.0017	.0050	3.4648	.0521	.1778	.0880	.0013	.0045
3.5497	.0451	.1435	.0902	.0011	.0036	3.5886	.0337	.1284	.0911	.0009	.0033
3.6721	.0190	.0811	.0933	.0005	.0021	3.7123	.0133	.0725	.0943	.0003	.0018
3.7844	-.0070	.0168	.0961	-.0002	.0004	3.8263	-.0070	.0150	.0972	-.0002	.0004
3.7945	-.0094	.0110	.0964	-.0002	.0003	3.8361	-.0088	.0101	.0974	-.0002	.0003
RADIUS (INCHES)	= 10.287		RADIUS (METERS)	= .2613		RADIUS (INCHES)	= 10.686		RADIUS (METERS)	= .2714	
CHORD (INCHES)	= 3.795		CHORD (METERS)	= .0964		CHORD (INCHES)	= 3.836		CHORD (METERS)	= .0974	
ZCSL (INCHES)	= 2.0296		ZCSL (METERS)	= .0516		ZCSL (INCHES)	= 2.0500		ZCSL (METERS)	= .0521	
YCSL (INCHES)	= .2086		YCSL (METERS)	= .0053		YCSL (INCHES)	= .1779		YCSL (METERS)	= .0045	
RLE (INCHES)	= .0102		RLE (METERS)	= .000259		RLE (INCHES)	= .0098		RLE (METERS)	= .000249	
RTE (INCHES)	= .0109		RTE (METERS)	= .000277		RTE (INCHES)	= .0103		RTE (METERS)	= .000262	
X-AREA (SQ. IN.)	= .6547		X-AREA (SQ. METERS)	= .000422		X-AREA (SQ. IN.)	= .6485		X-AREA (SQ. METERS)	= .000418	
GAMMA-CHORD (DEG.)	= 29.96		GAMMA-CHORD (RAD.)	= .5229		GAMMA-CHORD (DEG.)	= 32.73		GAMMA-CHORD (RAD.)	= .5713	

TABLE XXIV (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0087	.0091	.0000	-.0002	.0002	.0000	-.0083	.0086	.0000	-.0002	.0002
.0073	-.0077	.0116	.0002	-.0002	.0003	.0089	-.0076	.0107	.0002	-.0002	.0003
.1247	.0039	.0430	.0032	.0001	.0011	.1266	.0009	.0386	.0032	.0000	.0010
.2494	.0157	.0754	.0063	.0004	.0019	.2533	.0096	.0671	.0044	.0002	.0017
.3742	.0269	.1059	.0095	.0007	.0027	.3799	.0176	.0939	.0097	.0004	.0024
.4989	.0372	.1345	.0127	.0009	.0034	.5066	.0250	.1189	.0129	.0006	.0030
.6236	.0469	.1613	.0158	.0012	.0041	.6332	.0317	.1422	.0161	.0008	.0036
.7483	.0558	.1863	.0190	.0014	.0047	.7599	.0378	.1639	.0193	.0010	.0042
.8730	.0640	.2095	.0222	.0016	.0053	.8865	.0433	.1840	.0225	.0011	.0047
.9978	.0714	.2309	.0253	.0018	.0059	1.0132	.0481	.2024	.0257	.0012	.0051
1.1225	.0781	.2505	.0285	.0020	.0064	1.1398	.0522	.2192	.0290	.0013	.0056
1.2472	.0841	.2684	.0317	.0021	.0068	1.2665	.0558	.2343	.0322	.0014	.0060
1.3719	.0894	.2846	.0348	.0023	.0072	1.3931	.0587	.2479	.0354	.0015	.0063
1.4967	.0940	.2990	.0380	.0024	.0076	1.5198	.0610	.2599	.0386	.0015	.0066
1.6214	.0979	.3118	.0412	.0025	.0079	1.6464	.0626	.2703	.0418	.0016	.0069
1.7461	.1011	.3229	.0444	.0026	.0082	1.7730	.0637	.2793	.0450	.0016	.0071
1.8708	.1036	.3323	.0475	.0026	.0084	1.8997	.0642	.2863	.0483	.0016	.0073
1.9955	.1054	.3401	.0507	.0027	.0086	2.0263	.0642	.2921	.0515	.0016	.0074
2.1203	.1066	.3462	.0539	.0027	.0088	2.1530	.0635	.2964	.0547	.0016	.0075
2.2450	.1070	.3508	.0570	.0027	.0089	2.2796	.0623	.2993	.0579	.0016	.0076
2.3697	.1063	.3518	.0602	.0027	.0089	2.4063	.0605	.2994	.0611	.0015	.0076
2.4944	.1044	.3488	.0634	.0027	.0089	2.5329	.0581	.2963	.0643	.0015	.0075
2.6192	.1012	.3415	.0665	.0026	.0087	2.6596	.0551	.2895	.0676	.0014	.0074
2.7439	.0966	.3299	.0697	.0025	.0084	2.7862	.0515	.2791	.0708	.0013	.0071
2.8686	.0906	.3138	.0729	.0023	.0080	2.9129	.0473	.2649	.0740	.0012	.0067
2.9933	.0832	.2932	.0760	.0021	.0074	3.0395	.0424	.2469	.0772	.0011	.0063
3.1180	.0744	.2680	.0792	.0019	.0068	3.1662	.0370	.2251	.0804	.0009	.0057
3.2428	.0642	.2380	.0824	.0016	.0060	3.2928	.0310	.1994	.0836	.0008	.0051
3.3675	.0526	.2031	.0855	.0013	.0052	3.4195	.0243	.1697	.0869	.0006	.0043
3.4922	.0395	.1630	.0887	.0010	.0041	3.5461	.0171	.1359	.0901	.0004	.0035
3.6169	.0250	.1175	.0919	.0006	.0030	3.6727	.0093	.0978	.0933	.0002	.0025
3.7417	.0089	.0662	.0950	.0002	.0017	3.7994	.0009	.0554	.0965	.0000	.0014
3.86570	-.0070	.0138	.0980	-.0002	.0003	3.9170	-.0072	.0120	.0995	-.0002	.0003
3.8664	-.0084	.0095	.0982	-.0002	.0002	3.9260	-.0079	.0087	.0997	-.0002	.0002
RADIUS (INCHES)	10.985		RADIUS (METERS)	.2790		RADIUS (INCHES)	11.584		RADIUS (METERS)	.2942	
CHORD (INCHES)	3.866		CHORD (METERS)	.0982		CHORD (INCHES)	3.926		CHORD (METERS)	.0997	
ZCSL (INCHES)	2.0662		ZCSL (METERS)	.0525		ZCSL (INCHES)	2.0976		ZCSL (METERS)	.0533	
YCSSL (INCHES)	.1547		YCSSL (METERS)	.0039		YCSSL (INCHES)	.1141		YCSSL (METERS)	.0029	
RLE (INCHES)	.0095		RLE (METERS)	.000241		RLE (INCHES)	.0091		RLE (METERS)	.000231	
RTE (INCHES)	.0099		RTE (METERS)	.000251		RTE (INCHES)	.0093		RTE (METERS)	.000236	
X-AREA (SQ. IN.)	.6458		X-AREA (SQ. METERS)	.000417		X-AREA (SQ. IN.)	.6361		X-AREA (SQ. METERS)	.000410	
GAMMA-CHORD (DEG.)	34.72		GAMMA-CHORD (RAD.)	.6059		GAMMA-CHORD (DEG.)	37.93		GAMMA-CHORD (RAD.)	.6620	

TABLE XXIV (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0080	.0083	.0000	-.0002	.0002	.0000	-.0074	.0077	.0000	-.0002	.0002
.0086	-.0074	.0102	.0002	-.0002	.0003	.0079	-.0069	.0093	.0002	-.0002	.0002
.1279	.0003	.0370	.0032	.0000	.0009	.1299	.0003	.0340	.0023	.0000	.0009
.2557	.0079	.0643	.0045	.0002	.0016	.2598	.0072	.0589	.0046	.0002	.0015
.3836	.0148	.0898	.0097	.0004	.0023	.3897	.0133	.0821	.0099	.0003	.0021
.5115	.0210	.1137	.0130	.0005	.0029	.5196	.0185	.1036	.0132	.0005	.0026
.6393	.0265	.1358	.0162	.0007	.0034	.6495	.0229	.1234	.0165	.0006	.0031
.7672	.0313	.1563	.0195	.0008	.0040	.7794	.0265	.1415	.0198	.0007	.0036
.8951	.0355	.1750	.0227	.0009	.0044	.9093	.0295	.1580	.0231	.0007	.0040
1.0230	.0390	.1922	.0260	.0010	.0049	1.0392	.0317	.1729	.0264	.0008	.0044
1.1508	.0419	.2077	.0292	.0011	.0053	1.1691	.0332	.1862	.0297	.0008	.0047
1.2787	.0442	.2216	.0325	.0011	.0056	1.2990	.0340	.1980	.0330	.0009	.0050
1.4066	.0459	.2339	.0357	.0012	.0059	1.4289	.0341	.2082	.0363	.0009	.0053
1.5344	.0469	.2446	.0390	.0012	.0062	1.5588	.0337	.2168	.0396	.0009	.0055
1.6623	.0474	.2537	.0422	.0012	.0064	1.6887	.0326	.2240	.0429	.0008	.0057
1.7902	.0472	.2613	.0455	.0012	.0066	1.8186	.0309	.2296	.0462	.0008	.0058
1.9181	.0465	.2673	.0487	.0012	.0068	1.9485	.0286	.2337	.0495	.0007	.0059
2.0459	.0452	.2718	.0520	.0011	.0069	2.0784	.0257	.2363	.0528	.0007	.0060
2.1738	.0434	.2748	.0552	.0011	.0070	2.2083	.0222	.2374	.0561	.0006	.0060
2.3017	.0408	.2764	.0585	.0010	.0070	2.3382	.0180	.2370	.0594	.0005	.0060
2.4295	.0380	.2757	.0617	.0010	.0070	2.4681	.0135	.2350	.0627	.0003	.0060
2.5574	.0349	.2722	.0650	.0009	.0069	2.5980	.0092	.2307	.0660	.0002	.0059
2.6853	.0317	.2654	.0682	.0008	.0067	2.7279	.0054	.2238	.0693	.0001	.0057
2.8131	.0283	.2552	.0715	.0007	.0065	2.8578	.0020	.2142	.0726	.0001	.0054
2.9410	.0248	.2417	.0747	.0006	.0061	2.9877	-.0009	.2021	.0759	-.0000	.0051
3.0689	.0211	.2249	.0779	.0005	.0057	3.1176	-.0034	.1872	.0792	-.0001	.0048
3.1968	.0173	.2046	.0812	.0004	.0052	3.2475	-.0055	.1697	.0825	-.0001	.0043
3.3246	.0134	.1808	.0844	.0003	.0046	3.3774	-.0070	.1495	.0858	-.0002	.0038
3.4525	.0094	.1535	.0877	.0002	.0039	3.5073	-.0081	.1266	.0891	-.0002	.0032
3.5804	.0053	.1227	.0909	.0001	.0031	3.6372	-.0087	.1007	.0924	-.0002	.0026
3.7082	.0011	.0881	.0942	.0000	.0022	3.7671	-.0087	.0725	.0957	-.0002	.0018
3.8361	-.0031	.0498	.0974	-.0001	.0013	3.8970	-.0082	.0413	.0990	-.0002	.0010
3.9555	-.0070	.0107	.1005	-.0002	.0003	4.0187	-.0072	.0096	.1021	-.0002	.0002
3.9640	-.0073	.0079	.1007	-.0002	.0002	4.0269	-.0071	.0075	.1023	-.0002	.0002
RADIUS (INCHES)	11.984		RADIUS (METERS)	.3044		RADIUS (INCHES)	12.621		RADIUS (METERS)	.3206	
CHORD (INCHES)	3.964		CHORD (METERS)	.1007		CHORD (INCHES)	4.027		CHORD (METERS)	.1023	
ZCSL (INCHES)	2.1231		ZCSL (METERS)	.0539		ZCSL (INCHES)	2.1563		ZCSL (METERS)	.0548	
YCSL (INCHES)	.0951		YCSL (METERS)	.0024		YCSL (INCHES)	.0675		YCSL (METERS)	.0017	
PLE (INCHES)	.0087		PLE (METERS)	.000221		PLE (INCHES)	.0080		PLE (METERS)	.000203	
RTE (INCHES)	.0086		RTE (METERS)	.000218		RTE (INCHES)	.0083		RTE (METERS)	.000211	
X-AREA (SQ. IN.)	.6376		X-AREA (SQ. METERS)	.000411		X-AREA (SQ. IN.)	.6020		X-AREA (SQ. METERS)	.000388	
GAMMA-CHORD(100, IN.)	39.51		GAMMA-CHORD(100, IN.)	.6895		GAMMA-CHORD(100, IN.)	41.40		GAMMA-CHORD(100, IN.)	.7226	

TABLE XXIV (Cont'd)  
AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)			
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS	
.0000	-.0074	.0077		.0000	-.0073	.0075		.0000	-.0073	.0075		.0000	-.0073	.0075	
.0079	-.0069	.0093		.0077	-.0068	.0088		.0077	-.0068	.0088		.0077	-.0068	.0088	
.1304	.0338	.0338		.1314	.0320	.0302		.1314	.0320	.0302		.1314	.0320	.0302	
.2609	.0093	.0585		.2628	.0105	.0518		.2628	.0105	.0518		.2628	.0105	.0518	
.3913	.0163	.0814		.3942	.0181	.0719		.3942	.0181	.0719		.3942	.0181	.0719	
.5218	.0222	.1027		.5256	.0248	.0906		.5256	.0248	.0906		.5256	.0248	.0906	
.6522	.0273	.1222		.6570	.0306	.1076		.6570	.0306	.1076		.6570	.0306	.1076	
.7827	.0314	.1400		.7884	.0354	.1236		.7884	.0354	.1236		.7884	.0354	.1236	
.9131	.0346	.1562		.9198	.0394	.1378		.9198	.0394	.1378		.9198	.0394	.1378	
1.0436	.0370	.1706		1.0511	.0425	.1506		1.0511	.0425	.1506		1.0511	.0425	.1506	
1.1740	.0386	.1834		1.1825	.0447	.1619		1.1825	.0447	.1619		1.1825	.0447	.1619	
1.3045	.0393	.1946		1.3139	.0461	.1717		1.3139	.0461	.1717		1.3139	.0461	.1717	
1.4349	.0392	.2041		1.4453	.0466	.1800		1.4453	.0466	.1800		1.4453	.0466	.1800	
1.5654	.0383	.2120		1.5767	.0463	.1848		1.5767	.0463	.1848		1.5767	.0463	.1848	
1.6958	.0367	.2183		1.7081	.0452	.1922		1.7081	.0452	.1922		1.7081	.0452	.1922	
1.8263	.0343	.2230		1.8395	.0433	.1961		1.8395	.0433	.1961		1.8395	.0433	.1961	
1.9567	.0311	.2261		1.9709	.0406	.1985		1.9709	.0406	.1985		1.9709	.0406	.1985	
2.0872	.0273	.2275		2.1023	.0372	.1995		2.1023	.0372	.1995		2.1023	.0372	.1995	
2.2176	.0226	.2275		2.2337	.0330	.1991		2.2337	.0330	.1991		2.2337	.0330	.1991	
2.3481	.0172	.2259		2.3651	.0281	.1973		2.3651	.0281	.1973		2.3651	.0281	.1973	
2.4785	.0114	.2226		2.4965	.0227	.1942		2.4965	.0227	.1942		2.4965	.0227	.1942	
2.6090	.0057	.2173		2.6279	.0171	.1892		2.6279	.0171	.1892		2.6279	.0171	.1892	
2.7394	.0008	.2097		2.7593	.0121	.1823		2.7593	.0121	.1823		2.7593	.0121	.1823	
2.8699	-.0034	.1998		2.8907	.0076	.1735		2.8907	.0076	.1735		2.8907	.0076	.1735	
3.0003	-.0069	.1876		3.0221	.0036	.1626		3.0221	.0036	.1626		3.0221	.0036	.1626	
3.1308	-.0097	.1731		3.1534	.0002	.1499		3.1534	.0002	.1499		3.1534	.0002	.1499	
3.2612	-.0116	.1563		3.2848	-.0026	.1352		3.2848	-.0026	.1352		3.2848	-.0026	.1352	
3.3916	-.0129	.1372		3.4152	-.0048	.1186		3.4152	-.0048	.1186		3.4152	-.0048	.1186	
3.5221	-.0133	.1158		3.5476	-.0065	.1001		3.5476	-.0065	.1001		3.5476	-.0065	.1001	
3.6525	-.0129	.0921		3.6790	-.0075	.0797		3.6790	-.0075	.0797		3.6790	-.0075	.0797	
3.7830	-.0118	.0661		3.8104	-.0080	.0575		3.8104	-.0080	.0575		3.8104	-.0080	.0575	
3.9134	-.0097	.0378		3.9418	-.0078	.0333		3.9418	-.0078	.0333		3.9418	-.0078	.0333	
4.0360	-.0071	.0090		4.0653	-.0072	.0089		4.0653	-.0072	.0089		4.0653	-.0072	.0089	
4.1639	-.0070	.0072		4.1932	-.0071	.0073		4.1932	-.0071	.0073		4.1932	-.0071	.0073	
RADIUS (INCHES) = 12.859				RADIUS (INCHES) = 13.239				RADIUS (INCHES) = 13.239				RADIUS (INCHES) = 13.239			
CHORD (INCHES) = 4.044				CHORD (INCHES) = 4.073				CHORD (INCHES) = 4.073				CHORD (INCHES) = 4.073			
ZC (INCHES) = 2.1691				ZC (INCHES) = 2.1875				ZC (INCHES) = 2.1875				ZC (INCHES) = 2.1875			
YCSL (INCHES) = .0618				YCSL (INCHES) = .0518				YCSL (INCHES) = .0518				YCSL (INCHES) = .0518			
RLE (INCHES) = .0080				RLE (INCHES) = .0077				RLE (INCHES) = .0077				RLE (INCHES) = .0077			
RTE (INCHES) = .0080				RTE (INCHES) = .0080				RTE (INCHES) = .0080				RTE (INCHES) = .0080			
X-AREA (SQ. IN.) = .5758				X-AREA (SQ. IN.) = .4734				X-AREA (SQ. IN.) = .4734				X-AREA (SQ. IN.) = .4734			
GAMMA-CHORD(DEC.) = 42.09				GAMMA-CHORD(DEC.) = 44.09				GAMMA-CHORD(DEC.) = 44.09				GAMMA-CHORD(DEC.) = 44.09			

TABLE XXIV (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES -- ROTOR 1

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)			
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS	
.0000	-.0071	.0072		.0000	-.0002	.0002		.0000	-.0070	.0071		.0000	-.0002	.0002	
.0074	-.0067	.0083		.0002	-.0002	.0002		.0073	-.0067	.0079		.0002	-.0002	.0002	
.1324	.0003	.0260		.0034	.0000	.0007		.1331	-.0014	.0233		.0034	-.0000	.0006	
.2647	.0071	.0438		.0047	.0002	.0011		.2662	.0039	.0388		.0068	.0001	.0010	
.3971	.0134	.0605		.0101	.0003	.0015		.3993	.0088	.0535		.0101	.0002	.0014	
.5294	.0190	.0761		.0134	.0005	.0019		.5323	.0133	.0672		.0135	.0003	.0017	
.6618	.0240	.0905		.0168	.0006	.0023		.6654	.0174	.0799		.0169	.0004	.0020	
.7941	.0283	.1038		.0202	.0007	.0026		.7985	.0209	.0917		.0203	.0005	.0023	
.9265	.0319	.1158		.0235	.0008	.0029		.9316	.0241	.1024		.0237	.0006	.0026	
1.0589	.0349	.1267		.0269	.0009	.0032		1.0647	.0268	.1122		.0270	.0007	.0029	
1.1912	.0372	.1364		.0303	.0009	.0035		1.1978	.0289	.1209		.0304	.0007	.0031	
1.3236	.0389	.1449		.0336	.0010	.0037		1.3309	.0304	.1286		.0338	.0008	.0033	
1.4559	.0399	.1522		.0370	.0010	.0039		1.4639	.0315	.1354		.0372	.0008	.0034	
1.5883	.0403	.1583		.0403	.0010	.0040		1.5970	.0321	.1411		.0406	.0008	.0036	
1.7206	.0401	.1632		.0437	.0010	.0041		1.7301	.0323	.1460		.0439	.0008	.0037	
1.8530	.0393	.1670		.0471	.0010	.0042		1.8632	.0321	.1499		.0473	.0008	.0038	
1.9854	.0379	.1696		.0504	.0010	.0043		1.9963	.0315	.1530		.0507	.0008	.0039	
2.1177	.0359	.1712		.0538	.0009	.0043		2.1294	.0306	.1552		.0541	.0008	.0039	
2.2501	.0335	.1717		.0572	.0009	.0044		2.1625	.0294	.1566		.0575	.0007	.0040	
2.3824	.0305	.1711		.0605	.0008	.0043		2.3955	.0278	.1571		.0642	.0007	.0040	
2.5148	.0270	.1695		.0639	.0007	.0043		2.5286	.0260	.1571		.0676	.0006	.0039	
2.6471	.0234	.1664		.0672	.0006	.0042		2.6617	.0240	.1555		.0710	.0006	.0039	
2.7795	.0198	.1614		.0706	.0005	.0041		2.7948	.0217	.1520		.0744	.0005	.0037	
2.9119	.0163	.1544		.0740	.0004	.0039		2.9279	.0193	.1465		.0777	.0004	.0035	
3.0442	.0130	.1456		.0773	.0003	.0037		3.0610	.0167	.1390		.0811	.0004	.0033	
3.1766	.0098	.1348		.0807	.0002	.0034		3.1941	.0140	.1294		.0845	.0003	.0030	
3.3089	.0068	.1222		.0840	.0002	.0031		3.3272	.0112	.1179		.0879	.0002	.0026	
3.4413	.0039	.1077		.0874	.0001	.0027		3.4602	.0084	.1043		.0913	.0001	.0023	
3.5736	.0013	.0913		.0908	.0000	.0023		3.5933	.0054	.0888		.0947	.0001	.0018	
3.7060	-.0011	.0730		.0941	-.0000	.0019		3.7264	.0024	.0713		.0980	-.0000	.0013	
3.8384	-.0033	.0529		.0975	-.0001	.0013		3.8595	-.0007	.0518		.1014	-.0001	.0008	
3.9707	-.0053	.0310		.1009	-.0001	.0008		3.9926	-.0037	.0303		.1046	-.0002	.0002	
4.0954	-.0069	.0086		.1040	-.0002	.0002		4.1184	-.0066	.0083		.1048	-.0002	.0002	
4.1031	-.0070	.0072		.1042	-.0002	.0002		4.1257	-.0067	.0070		.1048	-.0002	.0002	
				RADIUS (INCHES) = 13.572				RADIUS (INCHES) = 13.810				RADIUS (METERS) = .3508			
				CHORD (INCHES) = 4.103				CHORD (INCHES) = 4.126				CHORD (METERS) = .1048			
				ZCSL (INCHES) = 2.1949				ZCSL (INCHES) = 2.2017				ZCSL (METERS) = .0559			
				YCSL (INCHES) = .0393				YCSL (INCHES) = .0308				YCSL (METERS) = .0008			
				RLE (INCHES) = .0075				RLE (INCHES) = .0073				RLE (METERS) = .000185			
				RTE (INCHES) = .0077				RTE (INCHES) = .0074				RTE (METERS) = .000188			
				X-AREA (SQ. IN.) = .4015				X-AREA (SQ. IN.) = .3739				X-AREA (SQ. METERS) = .000241			
				X-AREA-CHORD( DEG.) = 46.20				X-AREA-CHORD( DEG.) = 47.78				X-AREA-CHORD( RAD.) = .8339			

TABLE XXIV (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0068	.0068	.0000	-.0002	.0002	.0000	-.00068	.0067	.0000	-.0002	.0002
.0071	-.0068	.0074	.0002	-.0002	.0002	.0070	-.0070	.0071	.0002	-.0002	.0002
.1350	-.0070	.0169	.0034	-.0002	.0004	.1364	-.0092	.0146	.0035	-.0002	.0004
.2700	-.0072	.0267	.0069	-.0002	.0007	.2728	-.0114	.0223	.0069	-.0003	.0006
.4050	-.0072	.0360	.0103	-.0002	.0009	.4092	-.0133	.0298	.0104	-.0003	.0008
.5400	-.0072	.0450	.0137	-.0002	.0011	.5456	-.0149	.0371	.0139	-.0004	.0009
.6750	-.0070	.0535	.0171	-.0002	.0014	.6820	-.0162	.0441	.0173	-.0004	.0011
.8101	-.0068	.0616	.0206	-.0002	.0016	.8184	-.0173	.0509	.0208	-.0004	.0013
.9451	-.0065	.0693	.0240	-.0002	.0018	.9548	-.0181	.0575	.0243	-.0005	.0015
1.0801	-.0061	.0766	.0274	-.0002	.0019	1.0912	-.0186	.0638	.0277	-.0005	.0016
1.2151	-.0056	.0834	.0309	-.0001	.0021	1.2276	-.0189	.0700	.0312	-.0005	.0018
1.3501	-.0051	.0899	.0343	-.0001	.0023	1.3640	-.0189	.0759	.0346	-.0005	.0019
1.4851	-.0044	.0959	.0377	-.0001	.0024	1.5004	-.0187	.0815	.0381	-.0005	.0021
1.6201	-.0037	.1016	.0412	-.0001	.0026	1.6368	-.0181	.0870	.0416	-.0005	.0022
1.7551	-.0028	.1069	.0446	-.0001	.0027	1.7732	-.0173	.0923	.0450	-.0004	.0023
1.8901	-.0018	.1118	.0480	-.0000	.0028	1.9096	-.0162	.0974	.0485	-.0004	.0025
2.0252	-.0007	.1164	.0514	-.0000	.0030	2.0460	-.0148	.1022	.0520	-.0004	.0026
2.1602	.0006	.1206	.0549	.0000	.0031	2.1824	-.0131	.1069	.0554	-.0003	.0027
2.2952	.0020	.1244	.0583	.0001	.0032	2.3188	-.0111	.1113	.0589	-.0003	.0028
2.4302	.0035	.1280	.0617	.0001	.0033	2.4551	-.0087	.1157	.0624	-.0002	.0029
2.5652	.0054	.1316	.0652	.0001	.0033	2.5915	-.0059	.1203	.0658	-.0001	.0031
2.7002	.0072	.1358	.0686	.0002	.0034	2.7279	-.0030	.1238	.0693	-.0001	.0031
2.8352	.0085	.1342	.0720	.0002	.0034	2.8644	-.0004	.1256	.0728	-.0000	.0032
2.9702	.0093	.1322	.0754	.0002	.0034	3.0007	.0015	.1250	.0762	.0000	.0032
3.1052	.0095	.1278	.0789	.0002	.0032	3.1371	.0028	.1218	.0797	.0001	.0031
3.2403	.0092	.1210	.0823	.0002	.0031	3.2735	.0035	.1161	.0831	.0001	.0029
3.3753	.0083	.1118	.0857	.0002	.0028	3.4099	.0036	.1079	.0866	.0001	.0027
3.5103	.0070	.1003	.0892	.0002	.0025	3.5463	.0032	.0973	.0901	.0001	.0025
3.6453	.0052	.0863	.0926	.0001	.0022	3.6827	.0023	.0841	.0935	.0001	.0021
3.7803	.0029	.0700	.0960	.0001	.0018	3.8191	.0008	.0685	.0970	.0000	.0017
3.9153	.0002	.0512	.0994	.0000	.0013	3.9555	-.0012	.0503	.1005	-.0000	.0013
4.0503	-.0029	.0300	.1029	-.0001	.0008	4.0919	-.0036	.0296	.1039	-.0001	.0008
4.1783	-.0063	.0079	.1061	-.0002	.0002	4.2213	-.0063	.0079	.1072	-.0002	.0002
4.1853	-.0064	.0067	.1063	-.0002	.0002	4.2283	-.0064	.0079	.1074	-.0002	.0002
RADIUS (INCHES) = 14.481			RADIUS (METERS) = .3678			RADIUS (INCHES) = 14.981			RADIUS (METERS) = .3805		
CHORD (INCHES) = 4.185			CHORD (METERS) = .1063			CHORD (INCHES) = 4.228			CHORD (METERS) = .1074		
ZCSSL (INCHES) = 2.2314			ZCSSL (METERS) = .0567			ZCSSL (INCHES) = 2.2564			ZCSSL (METERS) = .0573		
YCSL (INCHES) = .0046			YCSL (METERS) = .0001			YCSL (INCHES) = -.0081			YCSL (METERS) = -.0002		
RLE (INCHES) = .0071			RLE (METERS) = .000180			RLE (INCHES) = .0070			RLE (METERS) = .000178		
RTE (INCHES) = .0070			RTE (METERS) = .000178			RTE (INCHES) = .0070			RTE (METERS) = .000178		
X-AREA (SQ. IN.) = .3667			X-AREA (SQ. METERS) = .000237			X-AREA (SQ. IN.) = .3709			X-AREA (SQ. METERS) = .000239		
GAMMA-CHORD (DEG.) = 51.11			GAMMA-CHORD (RAD.) = .8920			GAMMA-CHORD (DEG.) = 52.78			GAMMA-CHORD (RAD.) = .9212		

TABLE XXIV (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0069	.0065	.0000	-.0002	.0002	.0000	-.0069	.0068	.0000	-.0002	.0002
.0070	-.0070	.0069	.0002	-.0002	.0002	.0071	-.0070	.0071	.0002	-.0002	.0002
.1378	-.0103	.0135	.0035	-.0003	.0003	.1392	-.0105	.0136	.0035	-.0003	.0003
.2755	-.0135	.0203	.0070	-.0003	.0005	.2783	-.0139	.0203	.0071	-.0004	.0005
.4133	-.0163	.0269	.0105	-.0004	.0007	.4175	-.0168	.0269	.0106	-.0004	.0007
.5511	-.0188	.0333	.0140	-.0005	.0008	.5566	-.0192	.0334	.0141	-.0005	.0008
.6888	-.0209	.0395	.0175	-.0005	.0010	.6958	-.0212	.0399	.0177	-.0005	.0010
.8266	-.0227	.0456	.0210	-.0006	.0012	.8349	-.0228	.0464	.0212	-.0006	.0012
.9644	-.0242	.0516	.0245	-.0006	.0013	.9741	-.0239	.0528	.0247	-.0006	.0013
1.1022	-.0252	.0575	.0280	-.0006	.0015	1.1133	-.0245	.0593	.0283	-.0006	.0015
1.2399	-.0259	.0633	.0315	-.0007	.0016	1.2524	-.0246	.0656	.0318	-.0006	.0017
1.3777	-.0263	.0689	.0350	-.0007	.0018	1.3916	-.0242	.0720	.0333	-.0006	.0018
1.5155	-.0262	.0744	.0385	-.0007	.0019	1.5307	-.0234	.0784	.0389	-.0006	.0020
1.6532	-.0258	.0798	.0420	-.0007	.0020	1.6499	-.0230	.0848	.0424	-.0006	.0022
1.7910	-.0249	.0851	.0455	-.0006	.0022	1.8090	-.0201	.0912	.0459	-.0005	.0023
1.9288	-.0237	.0904	.0490	-.0006	.0023	1.9482	-.0176	.0978	.0495	-.0004	.0025
2.0666	-.0220	.0956	.0525	-.0006	.0024	2.0874	-.0145	.1043	.0530	-.0004	.0027
2.2043	-.0199	.1007	.0560	-.0005	.0026	2.2265	-.0109	.1110	.0566	-.0003	.0028
2.3421	-.0173	.1058	.0595	-.0004	.0027	2.3657	-.0067	.1179	.0601	-.0002	.0030
2.4799	-.0142	.1110	.0630	-.0004	.0028	2.5048	-.0018	.1248	.0636	-.0000	.0032
2.6176	-.0104	.1163	.0665	-.0003	.0030	2.6440	.0040	.1325	.0672	.0001	.0034
2.7554	-.0065	.1212	.0700	-.0002	.0031	2.7832	.0102	.1395	.0707	.0003	.0035
2.8932	-.0028	.1248	.0735	-.0001	.0032	2.9223	.0159	.1450	.0742	.0004	.0037
3.0310	.0003	.1255	.0770	.0000	.0032	3.0615	.0204	.1473	.0778	.0005	.0037
3.1687	.0026	.1234	.0805	.0001	.0031	3.2006	.0236	.1462	.0813	.0006	.0037
3.3065	.0042	.1186	.0840	.0001	.0030	3.3398	.0253	.1415	.0848	.0006	.0036
3.4443	.0050	.1111	.0875	.0001	.0028	3.4789	.0255	.1334	.0884	.0006	.0034
3.5820	.0051	.1008	.0910	.0001	.0026	3.6181	.0242	.1217	.0919	.0006	.0031
3.7198	.0044	.0878	.0945	.0001	.0022	3.7572	.0214	.1063	.0954	.0005	.0027
3.8576	.0030	.0718	.0980	.0001	.0018	3.8964	.0170	.0873	.0990	.0004	.0022
3.9954	.0007	.0530	.1015	.0000	.0013	4.0356	.0109	.0644	.1025	.0003	.0016
4.1331	-.0024	.0313	.1050	-.0001	.0008	4.1747	.0031	.0375	.1060	.0001	.0010
4.2639	-.0052	.0079	.1083	-.0002	.0002	4.3069	-.0059	.0083	.1094	-.0002	.0002
4.2709	-.0064	.0067	.1085	-.0002	.0002	4.3139	-.0064	.0068	.1096	-.0002	.0002
RADIUS (INCHES) = 15.481						RADIUS (INCHES) = 15.980					
CHORD (INCHES) = 4.271						CHORD (INCHES) = 4.314					
ZCSL (INCHES) = 2.2823						ZCSL (INCHES) = 2.3057					
YCSL (INCHES) = -.0142						YCSL (INCHES) = -.0064					
RLE (INCHES) = .0070						RLE (INCHES) = .0071					
RTE (INCHES) = .0070						RTE (INCHES) = .0070					
X-AREA (SQ. IN.) = .3777						X-AREA (SQ. IN.) = .3865					
GAMMA-CHORD(100%) = 54.23						GAMMA-CHORD(100%) = 55.70					
RADIUS (METERS) = .3932						RADIUS (METERS) = .4059					
CHORD (METERS) = .1085						CHORD (METERS) = .1096					
ZCSL (METERS) = .0580						ZCSL (METERS) = .0586					
YCSL (METERS) = -.0004						YCSL (METERS) = -.0002					
RLE (METERS) = .000178						RLE (METERS) = .000180					
RTE (METERS) = .000178						RTE (METERS) = .000178					
X-AREA (SQ. METERS) = .000244						X-AREA (SQ. METERS) = .000249					
GAMMA-CHORD(RAD.) = .9464						GAMMA-CHORD(RAD.) = .9722					

TABLE XXIV (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0069	.0068	.0000	-.0002	.0002	.0000	-.0071	.0069	.0000	-.0002	.0002
.0071	-.0070	.0071	.0002	-.0002	.0002	.0073	-.0072	.0073	.0002	-.0002	.0002
.1404	-.0100	.0142	.0036	-.0003	.0004	.1413	-.0077	.0149	.0036	-.0002	.0004
.2808	-.0126	.0216	.0071	-.0003	.0005	.2826	-.0111	.0229	.0072	-.0003	.0006
.4212	-.0147	.0291	.0107	-.0004	.0007	.4240	-.0131	.0311	.0108	-.0003	.0008
.5616	-.0162	.0367	.0143	-.0004	.0009	.5653	-.0139	.0394	.0144	-.0004	.0010
.7021	-.0172	.0443	.0178	-.0004	.0011	.7066	-.0141	.0478	.0179	-.0004	.0012
.8425	-.0176	.0519	.0214	-.0004	.0015	.8479	-.0136	.0564	.0215	-.0003	.0014
.9829	-.0175	.0596	.0250	-.0004	.0015	.9892	-.0125	.0650	.0251	-.0003	.0017
1.1233	-.0167	.0674	.0285	-.0004	.0017	1.1306	-.0107	.0739	.0287	-.0003	.0019
1.2637	-.0154	.0753	.0321	-.0004	.0019	1.2719	-.0082	.0829	.0323	-.0002	.0021
1.4041	-.0135	.0833	.0357	-.0003	.0021	1.4132	-.0051	.0921	.0359	-.0001	.0023
1.5445	-.0109	.0914	.0392	-.0003	.0023	1.5545	-.0013	.1015	.0395	-.0000	.0026
1.6850	-.0078	.0997	.0428	-.0002	.0025	1.6958	.0032	.1111	.0431	.0001	.0028
1.8254	-.0039	.1081	.0464	-.0001	.0027	1.8372	.0084	.1210	.0467	.0002	.0031
1.9658	.0005	.1167	.0499	.0000	.0030	1.9785	.0143	.1310	.0503	.0004	.0033
2.1062	.0057	.1255	.0535	.0001	.0032	2.1198	.0210	.1413	.0538	.0005	.0036
2.2466	.0116	.1345	.0571	.0003	.0034	2.2611	.0284	.1519	.0574	.0007	.0039
2.3870	.0182	.1437	.0606	.0005	.0037	2.4025	.0367	.1629	.0610	.0009	.0041
2.5274	.0255	.1531	.0642	.0006	.0039	2.5438	.0458	.1740	.0646	.0012	.0044
2.6678	.0337	.1639	.0678	.0009	.0042	2.6851	.0555	.1867	.0682	.0014	.0047
2.8083	.0431	.1737	.0713	.0011	.0044	2.8264	.0671	.1988	.0718	.0017	.0050
2.9487	.0511	.1815	.0749	.0013	.0046	2.9677	.0770	.2083	.0754	.0020	.0053
3.0891	.0572	.1855	.0785	.0015	.0047	3.1091	.0845	.2139	.0790	.0021	.0054
3.2295	.0609	.1851	.0820	.0015	.0047	3.2504	.0889	.2143	.0826	.0023	.0054
3.3699	.0620	.1799	.0856	.0016	.0046	3.3917	.0899	.2092	.0861	.0023	.0053
3.5103	.0605	.1701	.0892	.0015	.0043	3.5530	.0874	.1985	.0897	.0022	.0050
3.6507	.0564	.1556	.0927	.0014	.0040	3.6744	.0814	.1821	.0933	.0021	.0046
3.7911	.0496	.1362	.0963	.0013	.0035	3.8157	.0718	.1598	.0969	.0018	.0041
3.9316	.0400	.1118	.0999	.0010	.0028	3.9570	.0583	.1315	.1005	.0015	.0033
4.0720	.0275	.0822	.1034	.0007	.0021	4.0983	.0409	.0967	.1041	.0010	.0025
4.2124	.0120	.0472	.1070	.0003	.0012	4.2397	.0193	.0552	.1077	.0005	.0014
4.3460	-.0055	.0089	.1104	-.0001	.0002	4.3742	-.0052	.0093	.1111	-.0001	.0002
4.3528	-.0064	.0069	.1106	-.0002	.0002	4.3809	-.0064	.0070	.1113	-.0002	.0002
RADIUS (INCHES)	16.430		RADIUS (METERS)	.4173		RADIUS (INCHES)	16.780		RADIUS (METERS)	.4262	
CHORD (INCHES)	4.353		CHORD (METERS)	.1106		CHORD (INCHES)	4.381		CHORD (METERS)	.1113	
ZCSL (INCHES)	2.3303		ZCSL (METERS)	.0592		ZCSL (INCHES)	2.3471		ZCSL (METERS)	.0596	
YCSL (INCHES)	.0134		YCSL (METERS)	.0003		YCSL (INCHES)	.0284		YCSL (METERS)	.0007	
RLE (INCHES)	.0071		RLE (METERS)	.000180		RLE (INCHES)	.0073		RLE (METERS)	.000185	
RTE (INCHES)	.0070		RTE (METERS)	.000178		RTE (INCHES)	.0071		RTE (METERS)	.000180	
X-AREA (SQ. IN.)	.3939		X-AREA (SQ. METERS)	.000254		X-AREA (SQ. IN.)	.3998		X-AREA (SQ. METERS)	.000258	
GAMMA-CHORD (DEG.)	56.63		GAMMA-CHORD (RAD.)	.9883		GAMMA-CHORD (DEG.)	57.30		GAMMA-CHORD (RAD.)	1.0000	

TABLE XXV  
AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0030	.0083	.0000	-.0002	.0002	.0000	-.0067	.0073	.0000	-.0002	.0002
.0078	-.0056	.0125	.0002	-.0001	.0003	.0067	-.0049	.0103	.0002	-.0001	.0003
.0624	.0111	.0386	.0016	.0003	.0010	.0629	.0100	.0353	.0016	.0003	.0009
.1249	.0302	.0677	.0032	.0008	.0017	.1259	.0275	.0632	.0032	.0007	.0016
.1873	.0495	.0961	.0048	.0013	.0024	.1889	.0457	.0911	.0048	.0012	.0023
.2497	.0688	.1237	.0063	.0017	.0031	.2518	.0641	.1183	.0064	.0016	.0030
.3122	.0881	.1505	.0079	.0022	.0038	.3148	.0825	.1448	.0080	.0021	.0037
.3746	.1075	.1767	.0095	.0027	.0045	.3777	.1010	.1705	.0096	.0026	.0043
.4371	.1269	.2022	.0111	.0032	.0051	.4407	.1195	.1954	.0112	.0030	.0050
.4995	.1464	.2272	.0127	.0037	.0058	.5036	.1381	.2197	.0128	.0035	.0056
.5619	.1661	.2519	.0143	.0042	.0064	.5666	.1569	.2436	.0144	.0040	.0062
.6244	.1857	.2752	.0159	.0047	.0070	.6295	.1755	.2664	.0160	.0045	.0068
.6868	.2045	.2962	.0174	.0052	.0075	.6925	.1936	.2865	.0176	.0049	.0073
.7492	.2210	.3140	.0190	.0056	.0080	.7554	.2034	.3048	.0192	.0053	.0077
.8117	.2351	.3299	.0206	.0060	.0084	.8184	.2230	.3196	.0208	.0057	.0081
.8741	.2468	.3424	.0222	.0063	.0087	.8813	.2340	.3316	.0224	.0059	.0084
.9366	.2561	.3518	.0238	.0065	.0089	.9443	.2428	.3405	.0240	.0062	.0086
.9990	.2629	.3585	.0254	.0067	.0091	1.0072	.2491	.3466	.0256	.0063	.0088
1.0614	.2672	.3621	.0270	.0069	.0092	1.0702	.2529	.3498	.0272	.0064	.0089
1.1239	.2690	.3628	.0285	.0068	.0092	1.1331	.2544	.3502	.0288	.0065	.0089
1.1863	.2682	.3605	.0301	.0066	.0092	1.1961	.2534	.3476	.0304	.0064	.0089
1.2487	.2649	.3551	.0317	.0067	.0090	1.2590	.2498	.3419	.0320	.0063	.0087
1.3112	.2586	.3466	.0333	.0060	.0088	1.3220	.2436	.3332	.0336	.0062	.0085
1.3736	.2495	.3347	.0349	.0063	.0085	1.3849	.2347	.3213	.0352	.0060	.0082
1.4360	.2375	.3193	.0365	.0060	.0081	1.4479	.2229	.3059	.0368	.0057	.0078
1.4985	.2222	.3001	.0381	.0056	.0076	1.5108	.2081	.2869	.0384	.0053	.0073
1.5609	.2034	.2768	.0396	.0052	.0070	1.5738	.1900	.2640	.0400	.0048	.0067
1.6234	.1829	.2489	.0412	.0040	.0063	1.6367	.1685	.2367	.0416	.0043	.0060
1.6858	.1542	.2159	.0428	.0035	.0055	1.6997	.1431	.2047	.0432	.0030	.0052
1.7482	.1228	.1770	.0444	.0031	.0045	1.7627	.1134	.1671	.0448	.0025	.0042
1.8107	.0861	.1310	.0460	.0022	.0033	1.8256	.0730	.1231	.0464	.0020	.0031
1.8731	.0431	.0764	.0476	.0014	.0019	1.8886	.0390	.0714	.0480	.0010	.0018
1.9309	-.0039	.0150	.0490	-.0001	.0004	1.9464	-.0033	.0145	.0496	-.0001	.0004
1.9355	-.0078	.0099	.0492	-.0002	.0003	1.9515	-.0076	.0095	.0496	-.0002	.0002
RADIUS (INCHES) = 7.540						RADIUS (INCHES) = 7.740					
CHORD (INCHES) = 1.936						CHORD (INCHES) = 1.952					
ZC3L (INCHES) = .9810						ZC3L (INCHES) = .9914					
YC3L (INCHES) = .2331						YC3L (INCHES) = .2238					
RLE (INCHES) = .0084						RLE (INCHES) = .0072					
RTE (INCHES) = .0069						RTE (INCHES) = .0069					
X-AREA (SQ. IN.) = .1469						X-AREA (SQ. IN.) = .1433					
GAMMA-CHORD (DEG.) = 33.11						GAMMA-CHORD (DEG.) = 31.67					
RADIUS (METERS) = .1315						RADIUS (METERS) = .1566					
CHORD (METERS) = .0492						CHORD (METERS) = .0496					
ZC3L (METERS) = .0249						ZC3L (METERS) = .0252					
YC3L (METERS) = .0059						YC3L (METERS) = .0057					
RLE (METERS) = .000214						RLE (METERS) = .000133					
RTE (METERS) = .000174						RTE (METERS) = .000176					
X-AREA (SQ. METERS) = .000051						X-AREA (SQ. METERS) = .000032					
GAMMA-CHORD (RAD.) = .5778						GAMMA-CHORD (RAD.) = .5528					

TABLE XXV (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0063	.0069	.0000	-.0002	.0002	.0000	-.0064	.0070	.0000	-.0002	.0002
.0064	-.0047	.0095	.0002	-.0001	.0002	.0066	-.0049	.0097	.0002	-.0001	.0002
.0635	.0030	.0332	.0016	.0002	.0008	.0640	.0031	.0330	.0016	.0002	.0008
.1270	.0249	.0599	.0032	.0006	.0015	.1280	.0229	.0587	.0033	.0006	.0015
.1905	.0409	.0861	.0048	.0010	.0022	.1920	.0378	.0838	.0049	.0010	.0022
.2540	.0571	.1116	.0065	.0015	.0028	.2559	.0526	.1081	.0065	.0013	.0027
.3175	.0733	.1363	.0081	.0019	.0035	.3199	.0575	.1315	.0081	.0017	.0033
.3810	.0897	.1602	.0097	.0023	.0041	.3839	.0623	.1541	.0098	.0021	.0039
.4445	.1062	.1835	.0113	.0027	.0047	.4479	.0671	.1758	.0114	.0025	.0045
.5080	.1228	.2061	.0129	.0031	.0052	.5119	.0719	.1968	.0130	.0028	.0050
.5715	.1397	.2281	.0145	.0035	.0058	.5759	.0759	.2169	.0146	.0032	.0055
.6350	.1565	.2494	.0161	.0040	.0063	.6399	.0809	.2362	.0163	.0036	.0060
.6985	.1728	.2685	.0177	.0044	.0068	.7038	.0858	.2534	.0179	.0040	.0064
.7620	.1893	.2851	.0194	.0049	.0072	.7678	.0907	.2682	.0195	.0043	.0068
.8255	.2057	.2989	.0210	.0051	.0076	.8318	.0958	.2803	.0211	.0045	.0071
.8890	.2220	.3099	.0226	.0053	.0079	.8958	.1009	.2898	.0228	.0048	.0074
.9525	.2383	.3181	.0242	.0055	.0081	.9598	.1061	.2968	.0244	.0049	.0075
1.0160	.2547	.3237	.0258	.0057	.0082	1.0238	.1087	.3012	.0260	.0050	.0077
1.0795	.2714	.3266	.0274	.0059	.0083	1.0878	.1119	.3031	.0276	.0051	.0077
1.1430	.2883	.3268	.0290	.0059	.0083	1.1518	.1151	.3025	.0293	.0051	.0077
1.2065	.3050	.3243	.0306	.0058	.0082	1.2157	.1183	.2993	.0309	.0051	.0076
1.2700	.3217	.3188	.0323	.0057	.0081	1.2797	.1215	.2935	.0325	.0050	.0075
1.3335	.3383	.3102	.0339	.0056	.0079	1.3437	.1247	.2850	.0341	.0049	.0072
1.3970	.3547	.2986	.0355	.0054	.0076	1.4077	.1279	.2737	.0358	.0047	.0070
1.4605	.3710	.2838	.0371	.0051	.0072	1.4717	.1311	.2595	.0374	.0044	.0066
1.5240	.3871	.2656	.0387	.0047	.0067	1.5357	.1343	.2422	.0390	.0041	.0062
1.5875	.4031	.2437	.0403	.0043	.0062	1.5997	.1375	.2217	.0406	.0037	.0056
1.6510	.4190	.2179	.0419	.0038	.0055	1.6636	.1407	.1976	.0423	.0033	.0050
1.7145	.4347	.1877	.0435	.0032	.0048	1.7276	.1439	.1696	.0439	.0028	.0043
1.7780	.4503	.1525	.0452	.0025	.0033	1.7916	.1471	.1374	.0455	.0022	.0035
1.8415	.4658	.1118	.0468	.0017	.0028	1.8556	.1503	.1003	.0471	.0015	.0025
1.9050	.4812	.0664	.0484	.0008	.0016	1.9196	.1535	.0576	.0488	.0007	.0015
1.9685	.4965	.0137	.0499	-.0001	.0003	1.9778	.1567	.0130	.0502	-.0001	.0003
1.9850	.5074	.0090	.0500	-.0002	.0002	1.9836	.1571	.0085	.0504	-.0002	.0002
RADIUS (INCHES) = 7.985						RADIUS (INCHES) = 9.230					
CHORD (INCHES) = 1.968						CHORD (INCHES) = 1.984					
ZCSSL (INCHES) = .9980						ZCSSL (INCHES) = 1.0035					
YCSSL (INCHES) = .2061						YCSSL (INCHES) = .1887					
RLE (INCHES) = .0068						RLE (INCHES) = .0069					
RTE (INCHES) = .0070						RTE (INCHES) = .0071					
X-AREA (SQ. IN.) = .1464						X-AREA (SQ. IN.) = .1497					
GAMMA-CHORD (SEC.) = 23.50						GAMMA-CHORD (SEC.) = 27.47					
RADIUS (METERS) = .2028						RADIUS (METERS) = .2330					
CHORD (METERS) = .0500						CHORD (METERS) = 1.984					
ZCSSL (METERS) = .0254						ZCSSL (METERS) = 1.0035					
YCSSL (METERS) = .0062						YCSSL (METERS) = .1887					
RLE (METERS) = .00172						RLE (METERS) = .0069					
RTE (METERS) = .00178						RTE (METERS) = .0071					
X-AREA (SQ. METERS) = .00094						X-AREA (SQ. METERS) = .00180					
GAMMA-CHORD (RAD.) = .5148						GAMMA-CHORD (RAD.) = .4794					

TABLE XXV (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0065	.0070	.0000	-.0002	.0002	.0000	-.0065	.0071	.0000	-.0002	.0002
.0066	-.0050	.0097	.0002	-.0001	.0002	.0067	-.0050	.0099	.0002	-.0001	.0003
.0042	.0080	.0333	.0016	.0002	.0008	.0645	.0034	.0342	.0016	.0002	.0009
.1285	.0224	.0588	.0033	.0002	.0015	.1291	.0231	.0603	.0033	.0006	.0015
.1927	.0369	.0836	.0049	.0009	.0021	.1936	.0372	.0949	.0049	.0009	.0022
.2563	.0522	.1074	.0065	.0013	.0027	.2581	.0520	.1082	.0066	.0013	.0027
.3212	.0635	.1303	.0082	.0017	.0033	.3227	.0646	.1304	.0082	.0016	.0033
.3854	.0737	.1523	.0098	.0020	.0039	.3872	.0731	.1512	.0098	.0020	.0039
.4496	.0838	.1733	.0114	.0024	.0044	.4517	.0814	.1719	.0115	.0023	.0044
.5133	.0978	.1936	.0131	.0027	.0049	.5162	.0945	.1912	.0131	.0027	.0049
.5781	.1221	.2129	.0147	.0031	.0054	.5808	.1177	.2095	.0148	.0030	.0053
.6423	.1360	.2312	.0163	.0035	.0059	.6453	.1305	.2267	.0164	.0033	.0058
.7065	.1491	.2476	.0179	.0036	.0063	.7098	.1424	.2420	.0180	.0036	.0061
.7703	.1626	.2615	.0196	.0041	.0066	.7744	.1528	.2548	.0197	.0039	.0065
.8351	.1753	.2729	.0212	.0045	.0069	.8389	.1615	.2653	.0213	.0042	.0067
.8993	.1882	.2817	.0228	.0045	.0072	.9034	.1635	.2734	.0229	.0043	.0069
.9635	.1943	.2882	.0245	.0047	.0073	.9680	.1738	.2791	.0246	.0044	.0071
1.0278	.2008	.2921	.0261	.0048	.0075	1.0325	.1774	.2836	.0262	.0045	.0072
1.0920	.2068	.2937	.0277	.0048	.0075	1.0970	.1793	.2836	.0279	.0046	.0072
1.1562	.2122	.2927	.0294	.0049	.0074	1.1616	.1733	.2823	.0295	.0046	.0072
1.2205	.2180	.2893	.0310	.0048	.0073	1.2261	.1776	.2785	.0311	.0046	.0069
1.2847	.2234	.2833	.0326	.0047	.0072	1.2906	.1741	.2723	.0328	.0044	.0069
1.3489	.2284	.2747	.0343	.0046	.0070	1.3552	.1687	.2637	.0344	.0042	.0067
1.4132	.2334	.2635	.0359	.0044	.0067	1.4197	.1613	.2524	.0361	.0041	.0064
1.4774	.2384	.2494	.0375	.0042	.0063	1.4842	.1520	.2385	.0377	.0039	.0061
1.5416	.2434	.2324	.0392	.0039	.0059	1.5488	.1436	.2217	.0393	.0036	.0056
1.6059	.2484	.2122	.0408	.0035	.0054	1.6133	.1271	.2021	.0410	.0032	.0051
1.6701	.2534	.1888	.0424	.0032	.0048	1.6778	.1133	.1793	.0426	.0028	.0046
1.7343	.2584	.1617	.0441	.0026	.0041	1.7424	.0931	.1531	.0443	.0024	.0039
1.7986	.2634	.1306	.0457	.0020	.0033	1.8069	.0724	.1233	.0459	.0018	.0031
1.8628	.2684	.0951	.0473	.0014	.0024	1.8714	.0489	.0895	.0475	.0012	.0023
1.9270	.2734	.0543	.0489	.0006	.0014	1.9359	.0224	.0512	.0492	.0006	.0013
1.9854	.2784	.0125	.0504	-.0001	.0003	1.9944	-.0041	.0121	.0507	-.0001	.0003
1.9913	-.0070	.0083	.0506	-.0002	.0002	2.0005	-.0069	.0080	.0508	-.0002	.0002
RADIUS (INCHES) = 8.350			RADIUS (METERS) = .2121			RADIUS (INCHES) = 9.500			RADIUS (METERS) = .2159		
CHORD (INCHES) = 1.991			CHORD (METERS) = .0506			CHORD (INCHES) = 2.000			CHORD (METERS) = .0508		
ZCSSL (INCHES) = 1.0031			ZCSSL (METERS) = .0255			ZCSSL (INCHES) = 1.0034			ZCSSL (METERS) = .0255		
YCSSL (INCHES) = .1816			YCSSL (METERS) = .0046			YCSSL (INCHES) = .1743			YCSSL (METERS) = .0044		
RLE (INCHES) = .0071			RLE (METERS) = .00018			RLE (INCHES) = .0071			RLE (METERS) = .000175		
X-AREA (SQ. IN.) = 15.6			X-AREA (SQ. METERS) = .000098			X-AREA (SQ. IN.) = .1539			X-AREA (SQ. METERS) = .000179		
GAMMA-CHORD (DEG.) = 26.54			GAMMA-CHORD (RAD.) = .4632			GAMMA-CHORD (DEG.) = 25.55			GAMMA-CHORD (RAD.) = .4459		

TABLE XXV (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 1

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)			
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS	
.0003	-.0034	.0070		.0000	-.0002	.0002		.0000	-.0004	.0070		.0000	-.0004	.0002	
.0067	-.0050	.0098		.0002	-.0001	.0002		.0067	-.0030	.0097		.0002	-.0001	.0002	
.0659	.0073	.0341		.0017	.0002	.0009		.0665	.0073	.0347		.0017	.0002	.0009	
.1319	.0207	.0600		.0034	.0003	.0015		.1330	.0204	.0607		.0034	.0003	.0015	
.1979	.0336	.0842		.0050	.0003	.0021		.1994	.0328	.0850		.0051	.0006	.0022	
.2638	.0459	.1065		.0067	.0012	.0027		.2659	.0446	.1076		.0068	.0011	.0027	
.3298	.0577	.1280		.0084	.0015	.0033		.3324	.0557	.1285		.0084	.0014	.0033	
.3957	.0689	.1477		.0101	.0017	.0038		.3989	.0662	.1477		.0101	.0017	.0038	
.4617	.0796	.1659		.0117	.0020	.0042		.4654	.0760	.1652		.0118	.0015	.0042	
.5276	.0897	.1826		.0134	.0023	.0046		.5319	.0851	.1912		.0135	.0022	.0046	
.5936	.0995	.1980		.0151	.0025	.0050		.5983	.0937	.1957		.0152	.0024	.0050	
.6595	.0086	.2119		.0168	.0026	.0054		.6648	.0916	.2086		.0169	.0023	.0053	
.7255	.0167	.2238		.0184	.0030	.0057		.7313	.0886	.2196		.0186	.0028	.0056	
.7914	.0237	.2337		.0201	.0031	.0059		.7978	.0845	.2286		.0203	.0029	.0059	
.8574	.0232	.2414		.0218	.0033	.0061		.8643	.0813	.2356		.0220	.0030	.0060	
.9233	.0334	.2471		.0235	.0034	.0063		.9308	.0726	.2406		.0231	.0031	.0061	
.9893	.0363	.2506		.0251	.0035	.0064		.9972	.0729	.2436		.0253	.0032	.0062	
1.0552	.0379	.2521		.0268	.0035	.0064		1.0637	.0704	.2447		.0270	.0032	.0062	
1.1212	.0381	.2515		.0295	.0035	.0064		1.1302	.0729	.2437		.0302	.0032	.0062	
1.1871	.0370	.2489		.0302	.0035	.0063		1.1967	.0746	.2408		.0304	.0032	.0061	
1.2531	.0345	.2441		.0318	.0034	.0062		1.2632	.0721	.2358		.0321	.0034	.0060	
1.3191	.0307	.2372		.0335	.0033	.0060		1.3297	.0718	.2289		.0338	.0030	.0058	
1.3850	.0255	.2282		.0352	.0032	.0058		1.3961	.0713	.2199		.0355	.0029	.0056	
1.4510	.0189	.2170		.0369	.0030	.0055		1.4626	.0722	.2088		.0372	.0027	.0053	
1.5169	.0109	.2035		.0385	.0028	.0052		1.5291	.0739	.1956		.0388	.0025	.0050	
1.5829	.0015	.1878		.0402	.0026	.0048		1.5956	.0711	.1803		.0405	.0023	.0046	
1.6488	.0006	.1698		.0419	.0022	.0043		1.6621	.0611	.1627		.0422	.0024	.0041	
1.7148	.0000	.1494		.0436	.0020	.0039		1.7285	.0539	.1430		.0439	.0018	.0036	
1.7807	.0000	.1264		.0452	.0016	.0032		1.7950	.0573	.1208		.0456	.0015	.0031	
1.8467	.0000	.1008		.0469	.0012	.0026		1.8615	.0434	.0963		.0473	.0011	.0024	
1.9126	.0000	.0725		.0486	.0008	.0018		1.9280	.0261	.0692		.0490	.0007	.0018	
1.9786	.0000	.0413		.0503	.0003	.0010		1.9945	.0114	.0395		.0507	.0003	.0010	
2.0445	-.0046	.0107		.0518	-.0001	.0003		2.0544	-.0047	.0104		.0522	-.0001	.0003	
				.0519	-.0002	.0002		2.0610	-.0064	.0072		.0523	-.0002	.0002	
RADIUS (INCHES) = 9.500				RADIUS (METERS) = 24.13				RADIUS (INCHES) = 10.000				RADIUS (METERS) = 25.40			
CHORD (INCHES) = 2.045				CHORD (METERS) = .0519				CHORD (INCHES) = 2.061				CHORD (METERS) = .0523			
ZC5L (INCHES) = 1.0238				ZC5L (METERS) = .0260				ZC5L (INCHES) = 1.0312				ZC5L (METERS) = .0262			
YC5L (INCHES) = .1494				YC5L (METERS) = .0038				YC5L (INCHES) = .1478				YC5L (METERS) = .0036			
RLE (INCHES) = .0071				RLE (METERS) = .000130				RLE (INCHES) = .0070				RLE (METERS) = .000178			
RTE (INCHES) = .0070				RTE (METERS) = .000178				RTE (INCHES) = .0070				RTE (METERS) = .000179			
X-AREA (SQ. IN.) = .1602				X-AREA (SQ. METERS) = .000105				X-AREA (SQ. IN.) = .1753				X-AREA (SQ. METERS) = .000113			
GAMMA-CHORD(50.0) = 21.74				GAMMA-CHORD(RAD.) = .3794				GAMMA-CHORD(50.0) = 20.47				GAMMA-CHORD(RAD.) = .3573			

TABLE XXV (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0065	.0071	.0000	-.0002	.0002	.0000	-.0065	.0070	.0000	-.0002	.0002
.0067	-.0030	.0098	.0002	-.0002	.0003	.0067	-.0050	.0097	.0002	-.0001	.0002
.0649	.0080	.0339	.0016	.0001	.0009	.0653	.0076	.0338	.0017	.0002	.0009
.1298	.0223	.0598	.0033	.0006	.0015	.1307	.0213	.0595	.0033	.0005	.0015
.1947	.0363	.0845	.0049	.0009	.0021	.1961	.0347	.0838	.0050	.0009	.0021
.2596	.0521	.1079	.0066	.0013	.0027	.2614	.0476	.1067	.0066	.0012	.0027
.3245	.0635	.1301	.0082	.0016	.0033	.3268	.0602	.1283	.0083	.0015	.0033
.3894	.0766	.1512	.0099	.0019	.0038	.3921	.0725	.1486	.0100	.0016	.0038
.4543	.0834	.1710	.0115	.0023	.0043	.4575	.0843	.1676	.0116	.0021	.0043
.5192	.1020	.1898	.0132	.0026	.0049	.5228	.0938	.1955	.0133	.0024	.0047
.5841	.1144	.2075	.0148	.0029	.0053	.5882	.1070	.2021	.0149	.0027	.0051
.6489	.1263	.2238	.0165	.0032	.0057	.6535	.1177	.2174	.0166	.0030	.0055
.7138	.1371	.2381	.0181	.0035	.0060	.7169	.1274	.2307	.0183	.0032	.0059
.7787	.1465	.2500	.0198	.0037	.0064	.7842	.1357	.2417	.0199	.0034	.0061
.8436	.1542	.2597	.0214	.0039	.0066	.8496	.1425	.2505	.0216	.0036	.0064
.9085	.1603	.2670	.0231	.0041	.0068	.9143	.1478	.2571	.0232	.0038	.0065
.9734	.1647	.2719	.0247	.0042	.0069	.9803	.1516	.2615	.0245	.0039	.0066
1.0383	.1675	.2746	.0264	.0043	.0070	1.0456	.1539	.2637	.0266	.0039	.0067
1.1032	.1687	.2750	.0280	.0043	.0070	1.1110	.1547	.2637	.0282	.0039	.0067
1.1681	.1692	.2730	.0297	.0043	.0069	1.1763	.1540	.2615	.0299	.0035	.0066
1.2330	.1660	.2688	.0313	.0042	.0068	1.2417	.1518	.2511	.0315	.0039	.0065
1.2979	.1620	.2621	.0330	.0041	.0067	1.3070	.1479	.2504	.0332	.0038	.0064
1.3628	.1565	.2531	.0346	.0040	.0064	1.3724	.1426	.2414	.0349	.0036	.0061
1.4277	.1492	.2417	.0363	.0038	.0061	1.4377	.1355	.2301	.0365	.0034	.0058
1.4926	.1401	.2277	.0379	.0036	.0058	1.5031	.1289	.2184	.0382	.0032	.0055
1.5575	.1291	.2112	.0396	.0033	.0054	1.5685	.1166	.2002	.0398	.0030	.0051
1.6224	.1163	.1919	.0412	.0030	.0049	1.6338	.1045	.1915	.0415	.0027	.0046
1.6873	.1014	.1698	.0429	.0026	.0043	1.6992	.0908	.1600	.0432	.0023	.0041
1.7522	.0844	.1445	.0445	.0021	.0037	1.7645	.0751	.1358	.0448	.0019	.0034
1.8171	.0652	.1160	.0462	.0017	.0029	1.8299	.0576	.1086	.0465	.0015	.0028
1.8820	.0437	.0835	.0478	.0011	.0021	1.8952	.0382	.0783	.0481	.0010	.0020
1.9468	.0196	.0479	.0494	.0005	.0012	1.9606	.0167	.0446	.0498	.0004	.0011
2.0056	-.0042	.0116	.0509	-.0001	.0003	2.0196	-.0044	.0111	.0513	-.0004	.0003
2.0117	-.0067	.0078	.0511	-.0002	.0002	2.0259	-.0066	.0075	.0515	-.0002	.0002
RADIUS (INCHES) = 8.700			RADIUS (METERS) = .2210			RADIUS (INCHES) = 9.000			RADIUS (METERS) = .2286		
CHORD (INCHES) = 2.012			CHORD (METERS) = .0511			CHORD (INCHES) = 2.026			CHORD (METERS) = .0515		
ZC SL (INCHES) = 1.0101			ZC SL (METERS) = .0257			ZC SL (INCHES) = 1.0158			ZC SL (METERS) = .0258		
YCSL (INCHES) = .1678			YCSL (METERS) = .0043			YCSL (INCHES) = .1590			YCSL (METERS) = .0040		
RLE (INCHES) = .0071			RLE (METERS) = .000173			RLE (INCHES) = .0070			RLE (METERS) = .000178		
RTE (INCHES) = .0070			RTE (METERS) = .000178			RTE (INCHES) = .0070			RTE (METERS) = .000178		
X-AREA (SQ. IN.) = .1568			X-AREA (SQ. METERS) = .000104			X-AREA (SQ. IN.) = .1611			X-AREA (SQ. METERS) = .000104		
GAMMA-CHORD(DEC.) = 24.57			GAMMA-CHORD(DEC.) = 4.287			GAMMA-CHORD(DEC.) = 23.31			GAMMA-CHORD(DEC.) = 4.068		

TABLE XXV (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0064	.0071	.0000	-.0002	.0002	.0000	-.0062	.0069	.0000	-.0002	.0002
.0068	-.0050	.0099	.0002	-.0001	.0003	.0066	-.0049	.0098	.0002	-.0001	.0002
.0074	.0070	.0355	.0017	.0002	.0009	.0682	.0067	.0363	.0017	.0002	.0009
.1348	.0197	.0624	.0034	.0005	.0016	.1364	.0189	.0636	.0035	.0003	.0016
.2022	.0316	.0871	.0051	.0008	.0022	.2046	.0302	.0887	.0052	.0008	.0023
.2696	.0427	.1099	.0068	.0011	.0028	.2729	.0406	.1117	.0069	.0010	.0028
.3370	.0530	.1307	.0086	.0013	.0033	.3411	.0393	.1326	.0087	.0013	.0034
.4044	.0625	.1496	.0103	.0016	.0038	.4093	.0380	.1515	.0104	.0015	.0038
.4717	.0712	.1667	.0120	.0018	.0042	.4775	.0370	.1585	.0121	.0017	.0043
.5391	.0791	.1819	.0137	.0020	.0046	.5457	.0360	.1655	.0139	.0019	.0047
.6065	.0862	.1954	.0154	.0022	.0050	.6133	.0353	.1666	.0156	.0020	.0050
.6739	.0926	.2071	.0171	.0024	.0053	.6821	.0347	.1679	.0173	.0022	.0053
.7413	.0981	.2170	.0188	.0025	.0055	.7504	.0343	.1713	.0191	.0023	.0055
.8087	.1025	.2250	.0205	.0026	.0057	.8186	.0341	.2248	.0208	.0024	.0057
.8761	.1060	.2310	.0223	.0027	.0059	.8868	.0339	.2305	.0225	.0025	.0059
.9435	.1085	.2352	.0240	.0028	.0060	.9550	.0338	.2343	.0243	.0025	.0060
1.0109	.1100	.2375	.0257	.0028	.0060	1.0232	.0339	.2363	.0260	.0025	.0060
1.0783	.1115	.2379	.0274	.0029	.0060	1.0914	.0330	.2364	.0277	.0025	.0060
1.1457	.1130	.2365	.0291	.0026	.0060	1.1596	.0333	.2347	.0295	.0025	.0060
1.2131	.1094	.2331	.0308	.0026	.0059	1.2279	.0327	.2311	.0312	.0025	.0059
1.2805	.1058	.2279	.0325	.0027	.0058	1.2961	.0321	.2257	.0329	.0024	.0057
1.3478	.1022	.2208	.0342	.0026	.0056	1.3643	.0317	.2184	.0347	.0023	.0055
1.4152	.0976	.2117	.0359	.0025	.0054	1.4325	.0314	.2093	.0364	.0022	.0053
1.4826	.0920	.2007	.0377	.0023	.0051	1.5007	.0312	.1982	.0381	.0021	.0050
1.5500	.0853	.1877	.0394	.0020	.0048	1.5689	.0300	.1852	.0399	.0019	.0047
1.6174	.0776	.1727	.0411	.0020	.0044	1.6371	.0290	.1703	.0416	.0018	.0043
1.6848	.0688	.1556	.0428	.0017	.0040	1.7054	.0280	.1533	.0433	.0015	.0039
1.7522	.0590	.1365	.0445	.0015	.0035	1.7736	.0271	.1343	.0450	.0013	.0034
1.8196	.0481	.1152	.0462	.0012	.0029	1.8418	.0263	.1132	.0468	.0011	.0029
1.8870	.0361	.0916	.0479	.0009	.0023	1.9100	.0255	.0900	.0485	.0008	.0023
1.9544	.0230	.0658	.0496	.0006	.0017	1.9782	.0249	.0646	.0502	.0005	.0016
2.0218	.0089	.0376	.0514	.0002	.0010	2.0464	.0242	.0368	.0520	.0002	.0009
2.0826	-.0048	.0100	.0529	-.0001	.0003	2.1080	-.0049	.0099	.0535	-.0001	.0003
2.0892	-.0063	.0070	.0531	-.0002	.0002	2.1146	-.0063	.0070	.0537	-.0002	.0002
RADIUS (INCHES) = 11.000			RADIUS (METERS) = .2794			RADIUS (INCHES) = 12.000			RADIUS (METERS) = .3048		
CHORD (INCHES) = 2.089			CHORD (METERS) = .0531			CHORD (INCHES) = 2.115			CHORD (METERS) = .0537		
ZCSL (INCHES) = 1.0443			ZCSL (METERS) = .0265			ZCSL (INCHES) = 1.0569			ZCSL (METERS) = .0268		
YCSL (INCHES) = .1355			YCSL (METERS) = .0034			YCSL (INCHES) = .1316			YCSL (METERS) = .0033		
RLE (INCHES) = .0071			RLE (METERS) = .00181			RLE (INCHES) = .0070			RLE (METERS) = .00177		
RTE (INCHES) = .0070			RTE (METERS) = .00178			RTE (INCHES) = .0070			RTE (METERS) = .00178		
X-AREA (SQ. IN.) = .1898			X-AREA (SQ. M.) = .00122			X-AREA (SQ. IN.) = .2045			X-AREA (SQ. M.) = .00132		
GAMMA-CHORD (DEG.) = 18.84			GAMMA-CHORD (RAD.) = .3288			GAMMA-CHORD (DEG.) = 18.02			GAMMA-CHORD (RAD.) = .3146		

TABLE XXV (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 1

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)			
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS	
.0000	-.0063	.0070		.0000	-.0002	.0002		.0000	-.0062	.0070		.0000	-.0002	.0002	
.0068	-.0050	.0099		.0002	-.0004	.0003		.0068	-.0051	.0100		.0002	-.0001	.0003	
.0690	.0061	.0368		.0018	.0001	.0009		.0697	.0037	.0375		.0018	.0001	.0010	
.1380	.0177	.0847		.0035	.0005	.0016		.1395	.0169	.0660		.0035	.0004	.0017	
.2070	.0285	.0902		.0053	.0007	.0023		.2093	.0272	.0921		.0053	.0007	.0023	
.2760	.0384	.1135		.0070	.0010	.0029		.2790	.0367	.1160		.0071	.0009	.0029	
.3450	.0474	.1347		.0088	.0012	.0034		.3488	.0453	.1376		.0089	.0012	.0035	
.4140	.0556	.1537		.0105	.0014	.0039		.4185	.0531	.1570		.0106	.0013	.0040	
.4829	.0630	.1728		.0123	.0016	.0043		.4883	.0601	.1742		.0124	.0015	.0044	
.5519	.0695	.1958		.0140	.0018	.0047		.5580	.0662	.1894		.0142	.0017	.0048	
.6209	.0751	.2188		.0158	.0019	.0050		.6273	.0714	.2026		.0159	.0018	.0051	
.6899	.0800	.2399		.0175	.0020	.0053		.6975	.0758	.2137		.0177	.0019	.0054	
.7589	.0839	.2590		.0193	.0021	.0056		.7673	.0794	.2228		.0195	.0020	.0057	
.8279	.0871	.2763		.0210	.0022	.0057		.8371	.0822	.2301		.0213	.0021	.0058	
.8969	.0895	.2918		.0228	.0023	.0059		.9068	.0843	.2354		.0230	.0021	.0060	
.9659	.0918	.3054		.0245	.0023	.0060		.9766	.0866	.2390		.0248	.0022	.0061	
1.0349	.0938	.3172		.0263	.0023	.0060		1.0463	.0882	.2406		.0266	.0022	.0061	
1.1039	.0957	.3271		.0280	.0023	.0060		1.1161	.0900	.2404		.0283	.0022	.0061	
1.1729	.0973	.3352		.0298	.0023	.0060		1.1858	.0911	.2384		.0301	.0022	.0061	
1.2413	.0983	.3415		.0315	.0023	.0059		1.2556	.0934	.2346		.0319	.0021	.0060	
1.3109	.0988	.3459		.0333	.0022	.0057		1.3253	.0910	.2289		.0337	.0021	.0058	
1.3799	.0985	.3485		.0350	.0021	.0056		1.3951	.0879	.2213		.0354	.0020	.0056	
1.4488	.0973	.3495		.0368	.0020	.0053		1.4648	.0840	.2118		.0372	.0018	.0054	
1.5178	.0946	.3481		.0386	.0019	.0050		1.5346	.0794	.2005		.0390	.0018	.0051	
1.5868	.0909	.3424		.0403	.0016	.0047		1.6044	.0740	.1872		.0408	.0016	.0048	
1.6558	.0864	.3324		.0421	.0014	.0043		1.6741	.0679	.1719		.0425	.0015	.0044	
1.7248	.0811	.3180		.0438	.0014	.0039		1.7439	.0610	.1547		.0443	.0013	.0039	
1.7938	.0749	.3000		.0456	.0012	.0034		1.8136	.0534	.1354		.0461	.0011	.0034	
1.8628	.0679	.2781		.0473	.0010	.0029		1.8834	.0450	.1141		.0478	.0009	.0029	
1.9318	.0601	.2524		.0491	.0007	.0023		1.9531	.0359	.0906		.0496	.0007	.0023	
2.0008	.0515	.2224		.0508	.0004	.0016		2.0229	.0259	.0649		.0514	.0004	.0016	
2.0698	.0420	.1884		.0526	.0001	.0009		2.0926	.0152	.0369		.0532	.0001	.0009	
2.1388	.0320	.1500		.0542	-.0001	.0002		2.1557	-.0050	.0097		.0548	-.0001	.0002	
2.2078	.0210	.1076		.0559	-.0002	.0002		2.2194	-.0061	.0068		.0566	-.0002	.0002	
2.2768	.0090	.0616		.0576	-.0002	.0002		2.2831	-.0061	.0068		.0584	-.0002	.0002	
2.3458	.0000	.0116		.0593	-.0002	.0002		2.3468	-.0061	.0068		.0602	-.0002	.0002	
2.4148	.0000	.0000		.0610	-.0002	.0002		2.4105	-.0061	.0068		.0620	-.0002	.0002	
2.4838	.0000	.0000		.0627	-.0002	.0002		2.4742	-.0061	.0068		.0638	-.0002	.0002	
2.5528	.0000	.0000		.0644	-.0002	.0002		2.5379	-.0061	.0068		.0656	-.0002	.0002	
2.6218	.0000	.0000		.0661	-.0002	.0002		2.6016	-.0061	.0068		.0674	-.0002	.0002	
2.6908	.0000	.0000		.0678	-.0002	.0002		2.6653	-.0061	.0068		.0692	-.0002	.0002	
2.7598	.0000	.0000		.0695	-.0002	.0002		2.7290	-.0061	.0068		.0710	-.0002	.0002	
2.8288	.0000	.0000		.0712	-.0002	.0002		2.7927	-.0061	.0068		.0728	-.0002	.0002	
2.8978	.0000	.0000		.0729	-.0002	.0002		2.8564	-.0061	.0068		.0746	-.0002	.0002	
2.9668	.0000	.0000		.0746	-.0002	.0002		2.9201	-.0061	.0068		.0764	-.0002	.0002	
3.0358	.0000	.0000		.0763	-.0002	.0002		2.9838	-.0061	.0068		.0782	-.0002	.0002	
3.1048	.0000	.0000		.0780	-.0002	.0002		3.0475	-.0061	.0068		.0800	-.0002	.0002	
3.1738	.0000	.0000		.0797	-.0002	.0002		3.1112	-.0061	.0068		.0818	-.0002	.0002	
3.2428	.0000	.0000		.0814	-.0002	.0002		3.1749	-.0061	.0068		.0836	-.0002	.0002	
3.3118	.0000	.0000		.0831	-.0002	.0002		3.2386	-.0061	.0068		.0854	-.0002	.0002	
3.3808	.0000	.0000		.0848	-.0002	.0002		3.3023	-.0061	.0068		.0872	-.0002	.0002	
3.4498	.0000	.0000		.0865	-.0002	.0002		3.3660	-.0061	.0068		.0890	-.0002	.0002	
3.5188	.0000	.0000		.0882	-.0002	.0002		3.4297	-.0061	.0068		.0908	-.0002	.0002	
3.5878	.0000	.0000		.0899	-.0002	.0002		3.4934	-.0061	.0068		.0926	-.0002	.0002	
3.6568	.0000	.0000		.0916	-.0002	.0002		3.5571	-.0061	.0068		.0944	-.0002	.0002	
3.7258	.0000	.0000		.0933	-.0002	.0002		3.6208	-.0061	.0068		.0962	-.0002	.0002	
3.7948	.0000	.0000		.0950	-.0002	.0002		3.6845	-.0061	.0068		.0980	-.0002	.0002	
3.8638	.0000	.0000		.0967	-.0002	.0002		3.7482	-.0061	.0068		.1000	-.0002	.0002	
3.9328	.0000	.0000		.0984	-.0002	.0002		3.8119	-.0061	.0068		.1018	-.0002	.0002	
4.0018	.0000	.0000		.1001	-.0002	.0002		3.8756	-.0061	.0068		.1036	-.0002	.0002	
4.0708	.0000	.0000		.1018	-.0002	.0002		3.9393	-.0061	.0068		.1054	-.0002	.0002	
4.1398	.0000	.0000		.1035	-.0002	.0002		4.0030	-.0061	.0068		.1072	-.0002	.0002	
4.2088	.0000	.0000		.1052	-.0002	.0002		4.0667	-.0061	.0068		.1090	-.0002	.0002	
4.2778	.0000	.0000		.1069	-.0002	.0002		4.1304	-.0061	.0068		.1108	-.0002	.0002	
4.3468	.0000	.0000		.1086	-.0002	.0002		4.1941	-.0061	.0068		.1126	-.0002	.0002	
4.4158	.0000	.0000		.1103	-.0002	.0002		4.2578	-.0061	.0068		.1144	-.0002	.0002	
4.4848	.0000	.0000		.1120	-.0002	.0002		4.3215	-.0061	.0068		.1162	-.0002	.0002	
4.5538	.0000	.0000		.1137	-.0002	.0002		4.3852	-.0061	.0068		.1180	-.0002	.0002	
4.6228	.0000	.0000		.1154	-.0002	.0002		4.4489	-.0061	.0068		.1198	-.0002	.0002	
4.6918	.0000	.0000		.1171	-.0002	.0002		4.5126	-.0061	.0068		.1216	-.0002	.0002	
4.7608	.0000	.0000		.1188	-.0002	.0002		4.5763	-.0061	.0068		.1234	-.0002	.0002	
4.8298	.0000	.0000		.1205	-.0002	.0002		4.6400	-.0061	.0068		.1252	-.0002	.0002	
4.8988	.0000	.0000		.1222	-.0002	.0002		4.7037	-.0061	.0068		.1270	-.0002	.0002	
4.9678	.0000	.0000		.1239	-.0002	.0002		4.7674	-.0061	.0068		.1288	-.0002	.0002	
5.0368	.0000	.0000		.1256	-.0002	.0002		4.8311	-.0061	.0068		.1306	-.0002	.0002	
5.1058	.0000	.0000		.1273	-.0002	.0002		4.8948	-.0061	.0068		.1324	-.0002	.0002	
5.1748	.0000	.0000		.1290	-.0002	.0002		4.9585	-.0061	.0068		.1342	-.0002	.0002	
5.2438	.0000	.0000		.1307	-.0002	.0002		5.0222	-.0061	.0068		.1360	-.0002	.0002	
5.3128	.0000	.0000		.1324	-.0002	.0002		5.0859	-.0061	.0068		.1378	-.0002	.0002	
5.3818	.0000	.0000		.1341	-.0002	.0002		5.1496	-.0061	.0068		.1396	-.0002	.0002	
5.4508	.0000	.0000		.1358	-.0002	.0002		5.2133	-.0061	.0068		.1414	-.0002	.0002	
5.5198	.0000	.0000		.1375	-.0002	.0002		5.2770	-.0061	.0068		.1432	-.0002	.0002	
5.5888	.0000	.0000		.1392	-.0002	.0002		5.3407	-.0061	.0068		.1450	-.0002	.0002	
5.6578	.0000	.0000		.1409	-.0002	.0002		5.4044	-.0061	.0068		.1468	-.0002	.0002	
5.7268	.0000	.0000		.1426	-.0002	.0002		5.4681	-.0061	.0068		.1486	-.0002	.0002	
5.7958	.0000	.0000		.1443	-.0002	.0002		5.5318	-.0061	.0068		.1504	-.0002	.0002	
5.8648	.0000	.0000		.1460	-.0002	.0002		5.5955	-.0061	.0068		.1522	-.0002	.0002	
5.9338	.0000	.0000		.1477	-.0002	.0002		5.6592	-.0061	.0068		.1540	-.0002	.0002	
6.0028	.0000	.0000		.1494	-.0002</										

TABLE XXV (Cont'd)  
AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0061	.0069	.0000	-.0001	.0002	.0000	-.0061	.0070	.0000	-.0002	.0002
.0067	-.0049	.0100	.0002	-.0001	.0003	.0067	-.0048	.0103	.0002	-.0001	.0003
.0705	.0064	.0395	.0018	.0002	.0010	.0709	.0076	.0416	.0018	.0002	.0011
.1410	.0130	.0897	.0036	.0003	.0018	.1418	.0205	.0737	.0036	.0003	.0019
.2115	.0288	.0972	.0054	.0007	.0025	.2126	.0323	.1029	.0054	.0003	.0026
.2820	.0335	.1223	.0072	.0010	.0031	.2835	.0431	.1294	.0072	.0011	.0033
.3525	.0473	.1448	.0090	.0012	.0037	.3544	.0527	.1532	.0090	.0013	.0039
.4230	.0552	.1650	.0107	.0014	.0042	.4253	.0612	.1744	.0108	.0016	.0044
.4935	.0621	.1825	.0125	.0016	.0046	.4962	.0687	.1932	.0126	.0017	.0049
.5640	.0681	.1985	.0143	.0017	.0050	.5670	.0752	.2095	.0144	.0019	.0053
.6345	.0731	.2119	.0161	.0013	.0054	.6379	.0806	.2235	.0162	.0020	.0057
.7050	.0772	.2232	.0179	.0020	.0057	.7088	.0849	.2351	.0180	.0022	.0060
.7755	.0804	.2322	.0197	.0020	.0059	.7797	.0882	.2444	.0198	.0022	.0062
.8460	.0826	.2392	.0215	.0021	.0061	.8506	.0904	.2515	.0216	.0023	.0064
.9166	.0841	.2442	.0233	.0024	.0062	.9214	.0917	.2564	.0234	.0023	.0065
.9871	.0849	.2474	.0251	.0022	.0063	.9923	.0927	.2593	.0252	.0023	.0066
1.0576	.0850	.2487	.0269	.0022	.0063	1.0632	.0920	.2604	.0270	.0023	.0066
1.1281	.0845	.2482	.0287	.0021	.0063	1.1341	.0911	.2595	.0288	.0023	.0066
1.1986	.0832	.2458	.0304	.0021	.0062	1.2050	.0895	.2567	.0306	.0023	.0065
1.2691	.0813	.2415	.0322	.0021	.0061	1.2758	.0872	.2520	.0324	.0022	.0064
1.3396	.0787	.2354	.0340	.0020	.0060	1.3467	.0842	.2454	.0342	.0021	.0062
1.4101	.0754	.2274	.0358	.0019	.0058	1.4176	.0805	.2369	.0360	.0020	.0060
1.4806	.0715	.2174	.0376	.0013	.0055	1.4885	.0761	.2264	.0378	.0019	.0058
1.5511	.0668	.2056	.0394	.0017	.0052	1.5594	.0710	.2139	.0396	.0018	.0054
1.6216	.0615	.1918	.0412	.0016	.0049	1.6302	.0653	.1995	.0414	.0017	.0051
1.6921	.0554	.1761	.0430	.0014	.0045	1.7011	.0588	.1830	.0432	.0016	.0046
1.7626	.0487	.1583	.0448	.0012	.0040	1.7720	.0516	.1644	.0450	.0013	.0042
1.8331	.0413	.1385	.0466	.0010	.0035	1.8429	.0438	.1438	.0468	.0011	.0037
1.9036	.0332	.1166	.0484	.0008	.0030	1.9138	.0352	.1209	.0486	.0003	.0031
1.9741	.0244	.0925	.0501	.0006	.0023	1.9846	.0259	.0958	.0504	.0007	.0024
2.0446	.0149	.0662	.0519	.0004	.0017	2.0555	.0159	.0685	.0522	.0004	.0017
2.1151	.0048	.0376	.0537	.0004	.0010	2.1264	.0053	.0388	.0540	.0001	.0010
2.1789	-.0050	.0097	.0553	-.0001	.0002	2.1906	-.0050	.0098	.0556	-.0001	.0002
2.1856	-.0061	.0068	.0555	-.0002	.0002	2.1973	-.0060	.0068	.0558	-.0001	.0002
RADIUS (INCHES) = 15.000	RADIUS (METERS) = .3810		RADIUS (INCHES) = 15.500	RADIUS (METERS) = .3937		CHORD (INCHES) = 2.197	CHORD (METERS) = .0558		CHORD (INCHES) = 2.197	CHORD (METERS) = .0558	
CHORD (INCHES) = 2.186	CHORD (METERS) = .0555		CHORD (INCHES) = 2.197	CHORD (METERS) = .0558		ZC SL (INCHES) = 1.0922	ZC SL (METERS) = .0277		ZC SL (INCHES) = 1.0978	ZC SL (METERS) = .0279	
YC SL (INCHES) = 1.318	YC SL (METERS) = .0333		YC SL (INCHES) = 1.318	YC SL (METERS) = .0333		YC SL (INCHES) = 1.318	YC SL (METERS) = .0333		YC SL (INCHES) = 1.318	YC SL (METERS) = .0333	
RLE (INCHES) = .0071	RLE (METERS) = .00018		RLE (INCHES) = .0071	RLE (METERS) = .00018		RLE (INCHES) = .0071	RLE (METERS) = .00018		RLE (INCHES) = .0071	RLE (METERS) = .00018	
RTE (INCHES) = .0070	RTE (METERS) = .00017		RTE (INCHES) = .0070	RTE (METERS) = .00017		RTE (INCHES) = .0070	RTE (METERS) = .00017		RTE (INCHES) = .0070	RTE (METERS) = .00017	
X-AREA (SQ. IN.) = .2514	X-AREA (SQ. M.) = .000162		X-AREA (SQ. IN.) = .2514	X-AREA (SQ. M.) = .000162		X-AREA (SQ. IN.) = .2514	X-AREA (SQ. M.) = .000162		X-AREA (SQ. IN.) = .2514	X-AREA (SQ. M.) = .000162	
GAMMA-CHORD (DEG.) = 17.40	GAMMA-CHORD (RAD.) = .3037		GAMMA-CHORD (DEG.) = 17.40	GAMMA-CHORD (RAD.) = .3037		GAMMA-CHORD (DEG.) = 17.40	GAMMA-CHORD (RAD.) = .3037		GAMMA-CHORD (DEG.) = 17.40	GAMMA-CHORD (RAD.) = .3037	

TABLE XXV (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0062	.0073	.0000	-.0002	.0002	.0000	-.0000	.0074	.0000	-.0002	.0002
.0066	-.0046	.0109	.0002	-.0001	.0003	.0066	-.0006	.0112	.0002	-.0001	.0003
.0713	.0108	.0461	.0018	.0003	.0012	.0714	.0125	.0485	.0018	.0003	.0012
.1425	.0267	.0821	.0036	.0007	.0021	.1428	.0301	.0966	.0036	.0008	.0022
.2138	.0413	.1143	.0054	.0015	.0029	.2143	.0462	.1211	.0054	.0012	.0031
.2851	.0546	.1443	.0072	.0014	.0037	.2857	.0609	.1523	.0073	.0015	.0039
.3563	.0666	.1709	.0091	.0017	.0043	.3571	.0742	.1803	.0091	.0015	.0046
.4276	.0772	.1945	.0109	.0021	.0049	.4285	.0861	.2052	.0109	.0022	.0052
.4989	.0867	.2153	.0127	.0022	.0055	.4999	.0966	.2273	.0127	.0025	.0058
.5701	.0948	.2335	.0145	.0024	.0059	.5714	.1038	.2465	.0145	.0027	.0063
.6414	.1017	.2491	.0163	.0026	.0063	.6428	.1137	.2631	.0163	.0029	.0067
.7127	.1073	.2621	.0181	.0027	.0067	.7142	.1202	.2769	.0181	.0031	.0070
.7839	.1118	.2726	.0199	.0028	.0069	.7856	.1253	.2882	.0200	.0032	.0073
.8552	.1149	.2806	.0217	.0029	.0071	.8570	.1292	.2969	.0218	.0033	.0075
.9265	.1169	.2862	.0235	.0030	.0073	.9284	.1317	.3030	.0236	.0033	.0077
.9977	.1176	.2895	.0253	.0030	.0074	.9999	.1330	.3068	.0254	.0034	.0078
1.0690	.1175	.2906	.0272	.0030	.0074	1.0713	.1331	.3081	.0272	.0034	.0078
1.1403	.1164	.2896	.0290	.0030	.0074	1.1427	.1322	.3072	.0290	.0034	.0078
1.2115	.1145	.2865	.0308	.0029	.0073	1.2141	.1302	.3041	.0308	.0033	.0077
1.2828	.1117	.2813	.0326	.0028	.0071	1.2855	.1272	.2988	.0327	.0032	.0076
1.3541	.1080	.2740	.0344	.0027	.0070	1.3570	.1232	.2912	.0345	.0031	.0074
1.4254	.1034	.2645	.0362	.0026	.0067	1.4284	.1182	.2813	.0363	.0030	.0071
1.4966	.0979	.2528	.0380	.0025	.0064	1.4998	.1121	.2691	.0381	.0028	.0068
1.5679	.0915	.2390	.0398	.0023	.0061	1.5712	.1050	.2545	.0399	.0027	.0065
1.6392	.0843	.2229	.0416	.0021	.0057	1.6426	.0969	.2376	.0417	.0025	.0060
1.7104	.0761	.2046	.0434	.0019	.0052	1.7141	.0877	.2182	.0435	.0022	.0055
1.7817	.0671	.1839	.0453	.0017	.0047	1.7855	.0775	.1963	.0454	.0020	.0050
1.8530	.0571	.1609	.0471	.0015	.0041	1.8569	.0662	.1718	.0472	.0017	.0044
1.9242	.0463	.1353	.0489	.0012	.0034	1.9283	.0539	.1446	.0490	.0014	.0037
1.9955	.0345	.1072	.0507	.0009	.0027	1.9997	.0405	.1146	.0508	.0010	.0029
2.0668	.0219	.0765	.0525	.0006	.0019	2.0712	.0260	.0818	.0526	.0007	.0021
2.1380	.0083	.0431	.0543	.0002	.0011	2.1426	.0104	.0459	.0544	.0003	.0012
2.2093	-.0047	.0103	.0559	-.0001	.0003	2.2075	-.0046	.0106	.0561	-.0001	.0003
2.2806	-.0061	.0070	.0561	-.0002	.0002	2.2140	-.0061	.0071	.0562	-.0002	.0002
RADIUS (INCHES) = 16.000			RADIUS (METERS) = .4064			RADIUS (INCHES) = 16.200			RADIUS (METERS) = .4115		
CHORD (INCHES) = 2.209			CHORD (METERS) = .0561			CHORD (INCHES) = 2.214			CHORD (METERS) = .0562		
ZCSSL (INCHES) = 1.1037			ZCSSL (METERS) = .0280			ZCSSL (INCHES) = 1.1062			ZCSSL (METERS) = .0281		
YCSL (INCHES) = .1610			YCSL (METERS) = .0041			YCSL (INCHES) = .1739			YCSL (METERS) = .0044		
RLE (INCHES) = .0071			RLE (METERS) = .0018			RLE (INCHES) = .0072			RLE (METERS) = .0018		
RTE (INCHES) = .0070			RTE (METERS) = .0017			RTE (INCHES) = .0070			RTE (METERS) = .0017		
X-AREA (SQ. IN.) = .2699			X-AREA (SQ. M.) = .00174			X-AREA (SQ. IN.) = .2743			X-AREA (SQ. M.) = .00177		
GAMMA-CHORD (DEG.) = 13.10			GAMMA-CHORD (DEG.) = .3158			GAMMA-CHORD (DEG.) = 18.17			GAMMA-CHORD (DEG.) = .3172		

TABLE XXV (Cont'd)  
AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 1

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0063	.0076	.0000	-.0002	.0002	.0000	-.0065	.0079	.0000	-.0002	.0002
.0065	-.0044	.0116	.0002	-.0001	.0003	.0066	-.0044	.0079	.0002	-.0001	.0003
.0716	.0146	.0515	.0018	.0004	.0013	.0717	.0162	.0539	.0018	.0004	.0014
.1432	.0343	.0923	.0036	.0005	.0023	.1435	.0375	.0968	.0036	.0010	.0025
.2148	.0524	.1292	.0055	.0013	.0033	.2153	.0571	.1354	.0055	.0015	.0034
.2864	.0690	.1626	.0073	.0018	.0041	.2870	.0752	.1705	.0073	.0019	.0043
.3580	.0841	.1926	.0091	.0021	.0049	.3588	.0916	.2019	.0091	.0023	.0051
.4297	.0977	.2193	.0109	.0025	.0056	.4305	.0965	.2301	.0109	.0027	.0058
.5013	.1103	.2430	.0127	.0028	.0062	.5023	.1138	.2551	.0128	.0030	.0065
.5729	.1204	.2638	.0146	.0031	.0067	.5740	.1316	.2770	.0146	.0033	.0070
.6445	.1296	.2817	.0164	.0033	.0072	.6458	.1419	.2961	.0164	.0036	.0075
.7161	.1374	.2968	.0182	.0035	.0075	.7175	.1507	.3121	.0182	.0030	.0079
.7877	.1438	.3092	.0200	.0037	.0079	.7893	.1580	.3255	.0200	.0040	.0083
.8593	.1488	.3190	.0218	.0039	.0081	.8611	.1639	.3361	.0219	.0042	.0085
.9309	.1524	.3262	.0236	.0039	.0083	.9328	.1683	.3441	.0237	.0043	.0087
1.0025	.1545	.3308	.0255	.0039	.0084	1.0046	.1712	.3493	.0255	.0043	.0089
1.0741	.1553	.3327	.0273	.0039	.0085	1.0763	.1725	.3518	.0273	.0044	.0089
1.1458	.1548	.3322	.0291	.0039	.0084	1.1481	.1723	.3516	.0292	.0044	.0089
1.2174	.1530	.3293	.0309	.0039	.0084	1.2198	.1706	.3489	.0310	.0043	.0089
1.2890	.1499	.3239	.0327	.0038	.0082	1.2916	.1676	.3435	.0328	.0043	.0087
1.3606	.1456	.3160	.0346	.0037	.0080	1.3633	.1631	.3354	.0346	.0041	.0085
1.4322	.1401	.3057	.0364	.0036	.0078	1.4351	.1571	.3248	.0365	.0040	.0082
1.5038	.1333	.2928	.0382	.0034	.0074	1.5068	.1498	.3114	.0383	.0038	.0079
1.5754	.1252	.2773	.0400	.0032	.0070	1.5786	.1410	.2952	.0401	.0036	.0075
1.6470	.1158	.2592	.0418	.0029	.0066	1.6504	.1307	.2762	.0419	.0033	.0070
1.7186	.1052	.2384	.0437	.0027	.0061	1.7221	.1189	.2543	.0437	.0030	.0065
1.7902	.0933	.2147	.0455	.0024	.0055	1.7939	.1057	.2293	.0456	.0027	.0058
1.8619	.0800	.1982	.0473	.0020	.0048	1.8656	.0919	.2012	.0474	.0023	.0051
1.9335	.0655	.1587	.0491	.0017	.0040	1.9374	.0746	.1698	.0492	.0019	.0043
2.0051	.0496	.1253	.0509	.0013	.0032	2.0091	.0568	.1349	.0510	.0014	.0034
2.0767	.0323	.0899	.0527	.0008	.0023	2.0803	.0374	.0964	.0529	.0009	.0024
2.1483	.0137	.0504	.0546	.0002	.0013	2.1526	.0133	.0539	.0547	.0004	.0014
2.2135	-.0043	.0111	.0562	-.0001	.0003	2.2182	-.0042	.0114	.0563	-.0001	.0003
2.2199	-.0061	.0073	.0564	-.0002	.0002	2.2244	-.0061	.0074	.0565	-.0002	.0002
RADIUS (INCHES) = 16.450	RADIUS (METERS) = 0.4176	RADIUS (INCHES) = 16.450	RADIUS (METERS) = 0.4176	RADIUS (INCHES) = 16.450	RADIUS (METERS) = 0.4176	RADIUS (INCHES) = 16.450	RADIUS (METERS) = 0.4176	RADIUS (INCHES) = 16.450	RADIUS (METERS) = 0.4176	RADIUS (INCHES) = 16.450	RADIUS (METERS) = 0.4176
CHORD (INCHES) = 2.220	CHORD (METERS) = 0.0564	CHORD (INCHES) = 2.220	CHORD (METERS) = 0.0564	CHORD (INCHES) = 2.220	CHORD (METERS) = 0.0564	CHORD (INCHES) = 2.220	CHORD (METERS) = 0.0564	CHORD (INCHES) = 2.220	CHORD (METERS) = 0.0564	CHORD (INCHES) = 2.220	CHORD (METERS) = 0.0564
ZC3L (INCHES) = 1.1095	ZC3L (METERS) = 0.0282	ZC3L (INCHES) = 1.1095	ZC3L (METERS) = 0.0282	ZC3L (INCHES) = 1.1095	ZC3L (METERS) = 0.0282	ZC3L (INCHES) = 1.1095	ZC3L (METERS) = 0.0282	ZC3L (INCHES) = 1.1095	ZC3L (METERS) = 0.0282	ZC3L (INCHES) = 1.1095	ZC3L (METERS) = 0.0282
YCSL (INCHES) = 1.1321	YCSL (METERS) = 0.0282	YCSL (INCHES) = 1.1321	YCSL (METERS) = 0.0282	YCSL (INCHES) = 1.1321	YCSL (METERS) = 0.0282	YCSL (INCHES) = 1.1321	YCSL (METERS) = 0.0282	YCSL (INCHES) = 1.1321	YCSL (METERS) = 0.0282	YCSL (INCHES) = 1.1321	YCSL (METERS) = 0.0282
RLE (INCHES) = 0.0073	RLE (METERS) = 0.0018	RLE (INCHES) = 0.0073	RLE (METERS) = 0.0018	RLE (INCHES) = 0.0073	RLE (METERS) = 0.0018	RLE (INCHES) = 0.0073	RLE (METERS) = 0.0018	RLE (INCHES) = 0.0073	RLE (METERS) = 0.0018	RLE (INCHES) = 0.0073	RLE (METERS) = 0.0018
X-AREA (SQ. IN.) = 0.0070	X-AREA (SQ. IN.) = 0.0017	X-AREA (SQ. IN.) = 0.0070	X-AREA (SQ. IN.) = 0.0017	X-AREA (SQ. IN.) = 0.0070	X-AREA (SQ. IN.) = 0.0017	X-AREA (SQ. IN.) = 0.0070	X-AREA (SQ. IN.) = 0.0017	X-AREA (SQ. IN.) = 0.0070	X-AREA (SQ. IN.) = 0.0017	X-AREA (SQ. IN.) = 0.0070	X-AREA (SQ. IN.) = 0.0017
GAMMA-CHORD (INCHES) = 13.57	GAMMA-CHORD (METERS) = 0.3440	GAMMA-CHORD (INCHES) = 13.57	GAMMA-CHORD (METERS) = 0.3440	GAMMA-CHORD (INCHES) = 13.57	GAMMA-CHORD (METERS) = 0.3440	GAMMA-CHORD (INCHES) = 13.57	GAMMA-CHORD (METERS) = 0.3440	GAMMA-CHORD (INCHES) = 13.57	GAMMA-CHORD (METERS) = 0.3440	GAMMA-CHORD (INCHES) = 13.57	GAMMA-CHORD (METERS) = 0.3440

TABLE XXVI

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0111	.0136	.0000	-.0003	.0033	.0000	-.0113	.0132	.0000	-.0003	.0033
.0110	-.0073	.0210	.0003	-.0002	.0035	.0113	-.0077	.0204	.0003	-.0002	.0005
.1042	.0248	.0939	.0026	.0006	.0021	.1086	.0219	.0794	.0027	.0006	.0020
.2083	.0615	.1529	.0053	.0016	.0039	.2092	.0556	.1443	.0053	.0014	.0037
.3125	.0988	.2199	.0079	.0025	.0056	.3137	.0900	.2074	.0080	.0023	.0053
.4167	.1359	.2851	.0106	.0035	.0072	.4183	.1244	.2689	.0106	.0032	.0068
.5209	.1736	.3483	.0132	.0044	.0088	.5229	.1593	.3284	.0133	.0040	.0083
.6251	.2128	.4099	.0159	.0054	.0104	.6275	.1951	.3862	.0159	.0050	.0098
.7292	.2526	.4696	.0185	.0064	.0119	.7320	.2315	.4422	.0186	.0059	.0112
.8334	.2926	.5293	.0212	.0074	.0134	.8366	.2682	.4971	.0213	.0068	.0126
.9376	.3336	.5893	.0238	.0085	.0149	.9412	.3058	.5504	.0239	.0078	.0140
1.0418	.3747	.6378	.0265	.0095	.0162	1.0458	.3435	.6000	.0266	.0087	.0152
1.1459	.4135	.6854	.0291	.0105	.0174	1.1503	.3796	.6452	.0292	.0096	.0164
1.2501	.4503	.7259	.0318	.0114	.0184	1.2549	.4129	.6839	.0319	.0105	.0174
1.3543	.4803	.7599	.0344	.0122	.0193	1.3595	.4419	.7164	.0345	.0112	.0182
1.4585	.5068	.7875	.0370	.0129	.0200	1.4641	.4666	.7428	.0372	.0119	.0189
1.5626	.5282	.8092	.0397	.0134	.0206	1.5687	.4867	.7635	.0398	.0124	.0194
1.6668	.5449	.8246	.0423	.0138	.0209	1.6732	.5023	.7783	.0425	.0128	.0198
1.7710	.5567	.8340	.0450	.0141	.0212	1.7778	.5133	.7872	.0452	.0130	.0200
1.8752	.5633	.8373	.0476	.0143	.0213	1.8824	.5195	.7904	.0478	.0132	.0201
1.9793	.5647	.8342	.0503	.0143	.0212	1.9870	.5208	.7874	.0505	.0132	.0200
2.0835	.5605	.8246	.0529	.0142	.0209	2.0915	.5170	.7782	.0531	.0131	.0198
2.1877	.5507	.8082	.0556	.0140	.0205	2.1961	.5078	.7624	.0558	.0129	.0194
2.2919	.5346	.7844	.0582	.0136	.0199	2.3007	.4929	.7397	.0584	.0125	.0188
2.3960	.5121	.7528	.0609	.0130	.0191	2.4053	.4719	.7094	.0611	.0120	.0180
2.5002	.4824	.7125	.0635	.0123	.0181	2.5099	.4443	.6709	.0638	.0113	.0170
2.6044	.4449	.6623	.0662	.0113	.0169	2.6144	.4094	.6231	.0664	.0104	.0158
2.7086	.3987	.6011	.0688	.0101	.0153	2.7190	.3665	.5649	.0691	.0093	.0143
2.8127	.3427	.5268	.0714	.0087	.0134	2.8236	.3146	.4944	.0717	.0080	.0126
2.9169	.2755	.4368	.0741	.0070	.0111	2.9282	.2525	.4093	.0744	.0064	.0104
3.0211	.1952	.3270	.0767	.0050	.0083	3.0327	.1784	.3060	.0770	.0045	.0078
3.1253	.0994	.1911	.0794	.0025	.0049	3.1373	.0902	.1787	.0797	.0023	.0045
3.2295	-.0069	.0297	.0819	-.0002	.0018	3.2422	-.0068	.0296	.0822	-.0002	.0008
3.3337	-.0134	.0198	.0820	-.0003	.0005	3.3419	-.0134	.0194	.0823	-.0003	.0005
RADIUS (INCHES) = 8.286			RADIUS (METERS) = .2105			RADIUS (INCHES) = 8.431			RADIUS (METERS) = .2141		
CHORD (INCHES) = 3.229			CHORD (METERS) = .0820			CHORD (INCHES) = 3.242			CHORD (METERS) = .0824		
ZCSSL (INCHES) = 1.6552			ZCSSL (METERS) = .0420			ZCSSL (INCHES) = 1.6644			ZCSSL (METERS) = .0423		
YCSSL (INCHES) = .5274			YCSSL (METERS) = .0134			YCSSL (INCHES) = .5231			YCSSL (METERS) = .0125		
LER (INCHES) = .0125			LER (METERS) = .00317			LER (INCHES) = .0126			LER (METERS) = .00320		
TER (INCHES) = .0108			TER (METERS) = .00274			TER (INCHES) = .0113			TER (METERS) = .00287		
X-AREA (SQ. IN.) = .6796			X-AREA (SQ. METERS) = .00438			X-AREA (SQ. IN.) = .6687			X-AREA (SQ. METERS) = .00431		
GAMMA-CHORD(DEC.) = 18.70			GAMMA-CHORD(DEC.) = .3264			GAMMA-CHORD(DEC.) = 15.57			GAMMA-CHORD(DEC.) = .3415		

TABLE XXVI (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-.0000	-.0113	.0127	-.0000	-.0003	.0033	-.0000	-.0111	.0125	-.0000	-.0003	.0003
.0114	-.0079	.0194	.0003	-.0002	.0005	.0113	-.0080	.0189	.0003	-.0002	.0005
.0052	-.0194	.0747	.0027	-.0005	.0019	.1056	-.0180	.0721	.0027	-.0005	.0018
.2105	.0501	.1350	.0053	.0013	.0034	.2111	.0471	.1299	.0054	.0012	.0033
.3157	.0808	.1932	.0090	.0021	.0049	.3167	.0760	.1855	.0080	.0019	.0047
.4209	.1116	.2494	.0107	.0028	.0063	.4222	.1048	.2392	.0107	.0027	.0061
.5262	.1424	.3036	.0134	.0036	.0077	.5278	.1337	.2907	.0134	.0034	.0074
.6314	.1734	.3560	.0160	.0044	.0090	.6334	.1625	.3404	.0161	.0041	.0086
.7366	.2048	.4066	.0187	.0052	.0103	.7389	.1914	.3881	.0188	.0049	.0099
.8418	.2365	.4559	.0214	.0060	.0116	.8445	.2205	.4343	.0215	.0056	.0110
.9471	.2690	.5035	.0241	.0068	.0128	.9501	.2499	.4787	.0241	.0063	.0122
1.0523	.3016	.5487	.0267	.0077	.0139	1.0556	.2733	.5211	.0268	.0071	.0132
1.1575	.3337	.5903	.0294	.0085	.0150	1.1612	.3088	.5603	.0295	.0078	.0142
1.2628	.3634	.6260	.0321	.0092	.0159	1.2667	.3360	.5940	.0322	.0085	.0151
1.3690	.3891	.6561	.0347	.0099	.0167	1.3723	.3598	.6226	.0349	.0091	.0158
1.4732	.4111	.6806	.0374	.0104	.0173	1.4779	.3800	.6458	.0375	.0097	.0164
1.5785	.4291	.6998	.0401	.0109	.0178	1.5834	.3966	.6639	.0402	.0101	.0169
1.6837	.4429	.7134	.0428	.0112	.0181	1.6890	.4094	.6767	.0429	.0104	.0172
1.7889	.4526	.7216	.0454	.0115	.0183	1.7945	.4184	.6843	.0456	.0106	.0174
1.8942	.4580	.7243	.0481	.0116	.0184	1.9001	.4234	.6867	.0483	.0108	.0174
1.9994	.4592	.7212	.0508	.0117	.0183	2.0057	.4242	.6835	.0509	.0108	.0174
2.1046	.4558	.7123	.0535	.0116	.0181	2.1112	.4208	.6747	.0536	.0107	.0171
2.2099	.4472	.6973	.0561	.0114	.0177	2.2168	.4129	.6601	.0563	.0105	.0168
2.3151	.4336	.6757	.0588	.0110	.0172	2.3224	.4002	.6392	.0590	.0102	.0162
2.4203	.4147	.6473	.0615	.0105	.0164	2.4279	.3825	.6117	.0617	.0097	.0155
2.5256	.3901	.6112	.0641	.0099	.0155	2.5335	.3593	.5769	.0644	.0091	.0147
2.6308	.3590	.5665	.0668	.0091	.0144	2.6390	.3302	.5342	.0670	.0084	.0136
2.7360	.3209	.5128	.0695	.0081	.0130	2.7446	.2946	.4825	.0697	.0075	.0123
2.8413	.2749	.4475	.0722	.0070	.0114	2.8502	.2519	.4205	.0724	.0064	.0107
2.9465	.2197	.3691	.0748	.0056	.0094	2.9557	.2009	.3464	.0751	.0051	.0088
3.0517	.1543	.2748	.0775	.0039	.0070	3.0613	.1407	.2576	.0778	.0036	.0065
3.1569	.0769	.1600	.0802	.0020	.0041	3.1668	.0697	.1500	.0804	.0018	.0038
3.2584	-.0067	.0287	.0827	-.0002	.0037	3.2641	-.0065	.0284	.0829	-.0002	.0037
3.2622	-.0133	.0183	.0829	-.0003	.0005	3.2724	-.0131	.0180	.0831	-.0003	.0005
RADIUS (INCHES) = 8.446			RADIUS (METERS) = .2196			RADIUS (INCHES) = 8.773			RADIUS (METERS) = .2224		
CHORD (INCHES) = 3.262			CHORD (METERS) = .0829			CHORD (INCHES) = 3.272			CHORD (METERS) = .0831		
ZC (INCHES) = 1.6778			ZC (METERS) = .0426			ZC (INCHES) = 1.6845			ZC (METERS) = .0428		
YC (INCHES) = .4458			YC (METERS) = .0113			YC (INCHES) = .4490			YC (METERS) = .0106		
LER (INCHES) = .0124			LER (METERS) = .000315			LER (INCHES) = .0123			LER (METERS) = .000312		
TER (INCHES) = .0118			TER (METERS) = .000300			TER (INCHES) = .0122			TER (METERS) = .000310		
X-AREA (SQ. IN.) = .6524			X-AREA (SQ. METERS) = .000421			X-AREA (SQ. IN.) = .6426			X-AREA (SQ. METERS) = .000415		
GAMMA-CHORD( DEG.) = 20.87			GAMMA-CHORD( RAD.) = .3642			GAMMA-CHORD( DEG.) = 21.67			GAMMA-CHORD( RAD.) = .3781		

TABLE XXVI (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES - ROTOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0109	.0120	.0000	-.0003	.0033	-.0000	-.0108	.0118	.0000	-.0003	.0003
.0112	-.0081	.0178	.0003	-.0002	.0005	.0112	-.0082	.0171	.0003	-.0002	.0004
.0165	.0155	.0668	.0027	.0004	.0017	.1071	.0135	.0630	.0027	.0003	.0016
.2130	.0415	.1196	.0054	.0011	.0030	.2142	.0373	.1124	.0054	.0009	.0029
.3195	.0670	.1700	.0081	.0017	.0043	.3213	.0603	.1593	.0082	.0015	.0040
.4260	.0920	.2180	.0108	.0023	.0055	.4285	.0828	.2039	.0109	.0021	.0050
.5326	.1163	.2636	.0135	.0030	.0057	.5356	.1047	.2462	.0136	.0021	.0063
.6391	.1401	.3070	.0162	.0036	.0078	.6427	.1260	.2863	.0163	.0032	.0073
.7456	.1636	.3482	.0189	.0042	.0088	.7498	.1467	.3242	.0190	.0037	.0082
.8521	.1867	.3875	.0216	.0047	.0098	.8569	.1670	.3600	.0218	.0042	.0091
.9586	.2037	.4248	.0243	.0053	.0108	.9640	.1867	.3922	.0245	.0047	.0100
1.0651	.2324	.4607	.0271	.0059	.0117	1.0711	.2059	.4258	.0272	.0052	.0108
1.1716	.2553	.4937	.0298	.0065	.0125	1.1783	.2251	.4552	.0299	.0057	.0116
1.2781	.2763	.5225	.0325	.0070	.0133	1.2854	.2427	.4813	.0326	.0062	.0122
1.3847	.2948	.5469	.0352	.0075	.0133	1.3925	.2582	.5033	.0354	.0066	.0128
1.4912	.3104	.5665	.0379	.0079	.0144	1.4996	.2712	.5207	.0381	.0069	.0132
1.5977	.3230	.5814	.0406	.0082	.0148	1.6067	.2815	.5339	.0408	.0072	.0136
1.7042	.3324	.5917	.0433	.0084	.0150	1.7138	.2891	.5426	.0435	.0073	.0138
1.8107	.3388	.5971	.0460	.0086	.0152	1.8210	.2940	.5469	.0463	.0075	.0139
1.9172	.3418	.5977	.0487	.0087	.0152	1.9281	.2960	.5467	.0490	.0075	.0139
2.0237	.3414	.5934	.0514	.0087	.0151	2.0352	.2952	.5420	.0517	.0075	.0138
2.1302	.3375	.5841	.0541	.0086	.0148	2.1423	.2913	.5326	.0544	.0072	.0132
2.2367	.3299	.5695	.0568	.0084	.0145	2.2494	.2842	.5184	.0571	.0072	.0132
2.3433	.3185	.5494	.0595	.0081	.0140	2.3565	.2738	.4992	.0599	.0070	.0127
2.4498	.3030	.5235	.0622	.0077	.0133	2.4636	.2599	.4746	.0626	.0066	.0121
2.5563	.2833	.4914	.0649	.0072	.0125	2.5708	.2423	.4444	.0653	.0062	.0113
2.6628	.2590	.4526	.0676	.0066	.0115	2.6779	.2208	.4151	.0680	.0056	.0104
2.7693	.2298	.4055	.0703	.0058	.0103	2.7850	.1951	.3651	.0707	.0050	.0093
2.8758	.1953	.3521	.0730	.0050	.0089	2.8921	.1648	.3146	.0735	.0042	.0080
2.9823	.1546	.2882	.0758	.0039	.0073	2.9992	.1294	.2558	.0762	.0033	.0065
3.0889	.1070	.2127	.0785	.0027	.0054	3.1063	.0886	.1875	.0789	.0022	.0048
3.1954	.0516	.1232	.0812	.0013	.0031	3.2135	.0415	.1077	.0816	.0011	.0027
3.2922	-.0066	.0258	.0836	-.0002	.0007	3.3104	-.0067	.0236	.0841	-.0002	.0026
3.3919	-.0124	.0161	.0839	-.0003	.0004	3.3206	-.0118	.0148	.0843	-.0003	.0004
RADIUS (INCHES) = 9.116			RADIUS (METERS) = .2315			RADIUS (INCHES) = 9.354			RADIUS (METERS) = .2376		
CHORD (INCHES) = 3.302			CHORD (METERS) = .0839			CHORD (INCHES) = 3.321			CHORD (METERS) = .0843		
ZC SL (INCHES) = 1.696			ZC SL (METERS) = .0432			ZC SL (INCHES) = 1.7091			ZC SL (METERS) = .0434		
YC SL (INCHES) = .3564			YC SL (METERS) = .0091			YC SL (INCHES) = .3205			YC SL (METERS) = .0081		
LER (INCHES) = .0120			LER (METERS) = .000305			LER (INCHES) = .0119			LER (METERS) = .000302		
TER (INCHES) = .0125			TER (METERS) = .000317			TER (INCHES) = .0124			TER (METERS) = .000315		
X-AREA (SQ. IN.) = .6175			X-AREA (SQ. METERS) = .000398			X-AREA (SQ. IN.) = .6013			X-AREA (SQ. METERS) = .000388		
GAMMA-CHORD( DEG.) = 23.90			GAMMA-CHORD( DEG.) = .4172			GAMMA-CHORD( DEG.) = 25.56			GAMMA-CHORD( DEG.) = .4460		

TABLE XXVI (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES - ROTOR 2

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)			
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS	
.0000	-.0106	.0116		.0000	-.0003	.0033		.0000	-.0105	.0114		.0000	-.0003	.0033	
.0111	-.0093	.0167		.0003	-.0002	.0004		.0111	-.0083	.0162		.0003	-.0002	.0004	
.1074	.0123	.0608		.0027	.0003	.0015		.1079	.0109	.0591		.0027	.0003	.0015	
.2148	.0347	.1082		.0055	.0009	.0027		.2157	.0317	.1029		.0055	.0008	.0026	
.3223	.0564	.1532		.0082	.0014	.0039		.3236	.0517	.1454		.0082	.0013	.0037	
.4237	.0774	.1959		.0109	.0020	.0050		.4314	.0710	.1856		.0110	.0018	.0047	
.5371	.0978	.2362		.0136	.0025	.0050		.5393	.0895	.2234		.0137	.0023	.0057	
.6446	.1175	.2744		.0164	.0030	.0070		.6472	.1072	.2590		.0164	.0027	.0066	
.7520	.1366	.3104		.0191	.0035	.0079		.7550	.1240	.2923		.0192	.0031	.0074	
.8598	.1552	.3442		.0218	.0039	.0087		.8629	.1401	.3234		.0219	.0036	.0082	
.9668	.1731	.3761		.0246	.0044	.0096		.9707	.1556	.3525		.0247	.0040	.0090	
1.0743	.1905	.4061		.0273	.0048	.0103		1.0786	.1705	.3796		.0274	.0043	.0096	
1.1817	.2077	.4336		.0300	.0053	.0110		1.1865	.1849	.4045		.0301	.0047	.0103	
1.2891	.2255	.4592		.0327	.0057	.0116		1.2943	.1982	.4269		.0329	.0050	.0108	
1.3965	.2375	.4788		.0355	.0060	.0122		1.4022	.2093	.4456		.0356	.0053	.0113	
1.5040	.2491	.4931		.0382	.0063	.0126		1.5100	.2196	.4603		.0384	.0056	.0117	
1.6114	.2582	.5073		.0409	.0066	.0129		1.6179	.2271	.4711		.0411	.0058	.0120	
1.7188	.2649	.5152		.0437	.0067	.0131		1.7258	.2324	.4779		.0438	.0059	.0121	
1.8263	.2690	.5189		.0464	.0068	.0132		1.8336	.2354	.4807		.0466	.0060	.0122	
1.9337	.2705	.5183		.0491	.0069	.0132		1.9415	.2361	.4795		.0493	.0060	.0122	
2.0411	.2693	.5134		.0518	.0068	.0130		2.0493	.2345	.4742		.0521	.0060	.0120	
2.1485	.2653	.5039		.0546	.0067	.0128		2.1572	.2304	.4647		.0548	.0059	.0118	
2.2560	.2584	.4899		.0573	.0066	.0124		2.2651	.2237	.4508		.0575	.0057	.0115	
2.3634	.2484	.4710		.0600	.0063	.0120		2.3729	.2145	.4326		.0603	.0054	.0110	
2.4708	.2353	.4470		.0628	.0060	.0114		2.4808	.2025	.4097		.0630	.0051	.0104	
2.5782	.2188	.4177		.0655	.0056	.0106		2.5886	.1877	.3819		.0658	.0048	.0097	
2.6857	.1988	.3827		.0682	.0050	.0097		2.6965	.1698	.3469		.0685	.0043	.0089	
2.7931	.1750	.3415		.0709	.0044	.0087		2.8044	.1488	.3104		.0712	.0038	.0079	
2.9005	.1473	.2935		.0737	.0037	.0075		2.9122	.1245	.2658		.0740	.0032	.0068	
3.0080	.1152	.2380		.0764	.0029	.0060		3.0201	.0966	.2147		.0767	.0025	.0055	
3.1154	.0783	.1738		.0791	.0020	.0044		3.1280	.0693	.1562		.0795	.0016	.0040	
3.2228	.0361	.0997		.0819	.0009	.0025		3.2358	.0020	.0894		.0822	.0007	.0023	
3.3198	-.0068	.0224		.0843	-.0002	.0006		3.3330	-.0071	.0207		.0847	-.0002	.0005	
3.3303	-.0114			.0846	-.0003	.0004		3.3437	-.0110	.0132		.0849	-.0003	.0003	
RADIUS (INCHES) = 9.484				RADIUS (METERS) = .2405				RADIUS (INCHES) = 9.684				RADIUS (METERS) = .2460			
CHORD (INCHES) = 3.330				CHORD (METERS) = .0846				CHORD (INCHES) = 3.344				CHORD (METERS) = .0849			
ZCSSL (INCHES) = 1.7142				ZCSSL (METERS) = .0435				ZCSSL (INCHES) = 1.7216				ZCSSL (METERS) = .0437			
YCSSL (INCHES) = .3001				YCSSL (METERS) = .0076				YCSSL (INCHES) = .2726				YCSSL (METERS) = .0069			
LER (INCHES) = .0118				LER (METERS) = .000300				LER (INCHES) = .0116				LER (METERS) = .000295			
TER (INCHES) = .0123				TER (METERS) = .000312				TER (INCHES) = .0121				TER (METERS) = .000307			
X-AREA (SQ. IN.) = .5927				X-AREA (SQ. METERS) = .000382				X-AREA (SQ. IN.) = .5799				X-AREA (SQ. METERS) = .000374			
GAMMA-CHORD (DEG.) = 26.55				GAMMA-CHORD (RAD.) = .4634				GAMMA-CHORD (DEG.) = 28.10				GAMMA-CHORD (RAD.) = .4904			

TABLE XXVI (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0104	.0112	.0000	-.0003	.0003	.0000	-.0102	.0110	.0000	-.0003	.0003
.0110	-.0083	.0157	.0003	-.0002	.0004	.0109	-.0083	.0153	.0003	-.0002	.0004
.1082	.0037	.0559	.0027	.0002	.0014	.1084	.0086	.0538	.0028	.0002	.0014
.2163	.0231	.0988	.0055	.0007	.0025	.2169	.0263	.0950	.0055	.0007	.0024
.3245	.0478	.1394	.0082	.0012	.0035	.3253	.0442	.1337	.0083	.0011	.0030
.4326	.0657	.1777	.0110	.0017	.0045	.4337	.0604	.1703	.0110	.0015	.0043
.5408	.0828	.2138	.0137	.0021	.0054	.5421	.0767	.2048	.0138	.0019	.0052
.6489	.0992	.2477	.0165	.0025	.0063	.6506	.0918	.2371	.0165	.0023	.0060
.7571	.1146	.2794	.0192	.0029	.0071	.7590	.1062	.2673	.0193	.0027	.0068
.8652	.1297	.3090	.0220	.0033	.0078	.8674	.1199	.2955	.0220	.0030	.0075
.9734	.1438	.3365	.0247	.0037	.0085	.9759	.1328	.3216	.0248	.0034	.0082
1.0816	.1573	.3621	.0275	.0040	.0092	1.0843	.1451	.3458	.0275	.0037	.0088
1.1897	.1701	.3854	.0302	.0043	.0098	1.1927	.1566	.3678	.0303	.0040	.0093
1.2979	.1819	.4064	.0330	.0046	.0103	1.3012	.1673	.3877	.0330	.0042	.0098
1.4060	.1923	.4239	.0357	.0049	.0108	1.4096	.1766	.4042	.0358	.0045	.0103
1.5142	.2006	.4376	.0385	.0051	.0111	1.5180	.1841	.4172	.0386	.0047	.0106
1.6223	.2070	.4473	.0412	.0053	.0114	1.6264	.1897	.4263	.0413	.0048	.0108
1.7305	.2113	.4533	.0440	.0054	.0115	1.7349	.1934	.4318	.0441	.0049	.0110
1.8387	.2136	.4555	.0467	.0054	.0116	1.8433	.1951	.4336	.0468	.0050	.0110
1.9468	.2139	.4538	.0494	.0054	.0115	1.9517	.1949	.4316	.0496	.0049	.0110
2.0550	.2119	.4483	.0522	.0054	.0114	2.0602	.1926	.4259	.0523	.0049	.0108
2.1631	.2078	.4388	.0549	.0053	.0111	2.1686	.1883	.4162	.0551	.0048	.0106
2.2713	.2013	.4252	.0577	.0051	.0108	2.2770	.1820	.4027	.0578	.0046	.0102
2.3794	.1925	.4073	.0604	.0049	.0103	2.3855	.1735	.3852	.0606	.0044	.0098
2.4876	.1813	.3851	.0632	.0046	.0098	2.4939	.1628	.3635	.0633	.0041	.0092
2.5958	.1676	.3584	.0659	.0043	.0091	2.6023	.1500	.3375	.0661	.0038	.0086
2.7039	.1512	.3268	.0687	.0039	.0083	2.7107	.1348	.3071	.0689	.0034	.0078
2.8121	.1320	.2901	.0714	.0034	.0074	2.8192	.1173	.2719	.0716	.0030	.0059
2.9202	.1100	.2478	.0742	.0028	.0063	2.9276	.0973	.2318	.0744	.0025	.0059
3.0284	.0848	.1996	.0769	.0022	.0051	3.0360	.0746	.1864	.0771	.0019	.0047
3.1365	.0564	.1449	.0797	.0014	.0037	3.1445	.0491	.1349	.0799	.0012	.0034
3.2447	.0245	.0828	.0824	.0006	.0021	3.2529	.0207	.0770	.0826	.0005	.0020
3.3529	-.0073	.0197	.0849	-.0002	.0015	3.3605	-.0074	.0187	.0851	-.0002	.0005
			.0852	-.0003	.0003	3.3613	-.0105	.0123	.0854	-.0003	.0003
RADIUS (INCHES) = 9.833			RADIUS (METERS) = .2498			RADIUS (INCHES) = 9.983			RADIUS (METERS) = .2536		
CHORD (INCHES) = 3.353			CHORD (METERS) = .0852			CHORD (INCHES) = 3.361			CHORD (METERS) = .0854		
ZCSSL (INCHES) = 1.7265			ZCSSL (METERS) = .0435			ZCSSL (INCHES) = 1.7310			ZCSSL (METERS) = .0440		
YCSL (INCHES) = .2545			YCSL (METERS) = .0065			YCSL (INCHES) = .2382			YCSL (METERS) = .0061		
LER (INCHES) = .0115			LER (METERS) = .000292			LER (INCHES) = .0113			LER (METERS) = .00287		
TER (INCHES) = .0120			TER (METERS) = .000305			TER (INCHES) = .0119			TER (METERS) = .00302		
X-AREA (SQ. IN.) = .5707			X-AREA (SQ. METERS) = .00368			X-AREA (SQ. IN.) = .5618			X-AREA (SQ. METERS) = .00362		
GAMMA-CHORD (DEG.) = 29.23			GAMMA-CHORD (RAD.) = .5102			GAMMA-CHORD (DEG.) = 30.33			GAMMA-CHORD (RAD.) = .5234		

TABLE XXVI (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-0.000	-0.0100	-0.0106	-0.000	-0.0003	-0.0003	-0.000	-0.0098	-0.0104	-0.000	-0.0002	-0.0003
-0.006	-0.008	-0.0145	-0.0003	-0.0002	-0.0004	-0.005	-0.0084	-0.0139	-0.0003	-0.0002	-0.0004
-0.008	-0.0067	-0.0503	-0.0028	-0.0002	-0.0013	-0.0092	-0.0052	-0.0471	-0.0028	-0.0001	-0.0012
-0.0177	-0.0229	-0.0882	-0.0055	-0.0006	-0.0022	-0.0184	-0.0196	-0.0822	-0.0055	-0.0005	-0.0021
-0.0265	-0.0382	-0.1240	-0.0083	-0.0010	-0.0031	-0.0275	-0.0331	-0.1152	-0.0083	-0.0008	-0.0029
-0.0353	-0.0528	-0.1577	-0.0111	-0.0013	-0.0040	-0.0367	-0.0459	-0.1462	-0.0111	-0.0012	-0.0037
-0.0442	-0.0667	-0.1893	-0.0138	-0.0017	-0.0048	-0.0459	-0.0580	-0.1754	-0.0139	-0.0015	-0.0045
-0.0530	-0.0799	-0.2190	-0.0166	-0.0020	-0.0056	-0.0551	-0.0693	-0.2026	-0.0166	-0.0018	-0.0051
-0.0618	-0.0923	-0.2466	-0.0194	-0.0023	-0.0063	-0.0643	-0.0800	-0.2280	-0.0194	-0.0020	-0.0058
-0.0707	-0.1040	-0.2723	-0.0221	-0.0026	-0.0059	-0.0734	-0.0900	-0.2515	-0.0222	-0.0023	-0.0064
-0.0795	-0.1149	-0.2961	-0.0249	-0.0029	-0.0075	-0.0826	-0.0993	-0.2732	-0.0250	-0.0025	-0.0069
-0.0883	-0.1252	-0.3180	-0.0276	-0.0032	-0.0081	-0.0918	-0.1078	-0.2931	-0.0277	-0.0027	-0.0074
-0.0971	-0.1348	-0.3379	-0.0304	-0.0034	-0.0086	-0.1010	-0.1157	-0.3111	-0.0305	-0.0029	-0.0079
-0.1060	-0.1436	-0.3560	-0.0332	-0.0036	-0.0090	-0.1102	-0.1230	-0.3276	-0.0333	-0.0031	-0.0083
-0.1148	-0.1513	-0.3712	-0.0359	-0.0038	-0.0094	-0.1193	-0.1294	-0.3414	-0.0361	-0.0033	-0.0087
-0.1236	-0.1575	-0.3830	-0.0387	-0.0040	-0.0097	-0.1285	-0.1344	-0.3523	-0.0388	-0.0034	-0.0089
-0.1325	-0.1621	-0.3913	-0.0415	-0.0041	-0.0099	-0.1377	-0.1381	-0.3600	-0.0416	-0.0035	-0.0091
-0.1413	-0.1649	-0.3962	-0.0442	-0.0042	-0.0101	-0.1469	-0.1403	-0.3644	-0.0444	-0.0036	-0.0093
-0.1501	-0.1661	-0.3976	-0.0470	-0.0042	-0.0101	-0.1561	-0.1411	-0.3655	-0.0471	-0.0036	-0.0093
-0.1590	-0.1656	-0.3955	-0.0498	-0.0042	-0.0100	-0.1653	-0.1404	-0.3634	-0.0499	-0.0036	-0.0092
-0.1678	-0.1634	-0.3899	-0.0525	-0.0041	-0.0099	-0.1744	-0.1382	-0.3580	-0.0527	-0.0035	-0.0091
-0.1766	-0.1594	-0.3808	-0.0553	-0.0040	-0.0097	-0.1836	-0.1345	-0.3493	-0.0555	-0.0034	-0.0089
-0.1855	-0.1536	-0.3679	-0.0581	-0.0039	-0.0093	-0.1928	-0.1294	-0.3373	-0.0582	-0.0033	-0.0086
-0.1943	-0.1460	-0.3514	-0.0608	-0.0037	-0.0089	-0.2020	-0.1227	-0.3218	-0.0610	-0.0031	-0.0082
-0.2031	-0.1366	-0.3311	-0.0636	-0.0035	-0.0084	-0.2112	-0.1145	-0.3029	-0.0638	-0.0029	-0.0077
-0.2120	-0.1253	-0.3069	-0.0663	-0.0032	-0.0078	-0.2203	-0.1047	-0.2804	-0.0666	-0.0027	-0.0071
-0.2208	-0.1121	-0.2787	-0.0691	-0.0028	-0.0071	-0.2295	-0.0933	-0.2542	-0.0693	-0.0024	-0.0065
-0.2296	-0.0969	-0.2461	-0.0719	-0.0025	-0.0063	-0.2387	-0.0803	-0.2242	-0.0721	-0.0020	-0.0057
-0.2385	-0.0797	-0.2092	-0.0746	-0.0020	-0.0053	-0.2479	-0.0656	-0.1903	-0.0749	-0.0017	-0.0048
-0.2473	-0.0604	-0.1676	-0.0774	-0.0015	-0.0043	-0.2571	-0.0493	-0.1522	-0.0776	-0.0013	-0.0039
-0.2561	-0.0390	-0.1210	-0.0802	-0.0010	-0.0031	-0.2662	-0.0312	-0.1098	-0.0804	-0.0008	-0.0028
-0.2650	-0.0152	-0.0689	-0.0829	-0.0004	-0.0017	-0.2754	-0.0114	-0.0627	-0.0832	-0.0003	-0.0016
-0.2738	-0.0077	-0.0174	-0.0854	-0.0002	-0.0004	-0.2846	-0.0078	-0.0162	-0.0857	-0.0002	-0.0004
-0.2826	-0.0103	-0.0117	-0.0881	-0.0003	-0.0003	-0.2938	-0.0099	-0.0111	-0.0880	-0.0003	-0.0003
RADIUS (INCHES) = 10.283			RADIUS (METERS) = 0.2612			RADIUS (INCHES) = 10.582			RADIUS (METERS) = 0.2688		
CHORD (INCHES) = 3.374			CHORD (METERS) = 0.0857			CHORD (INCHES) = 3.385			CHORD (METERS) = 0.0860		
ZCSL (INCHES) = 1.7394			ZCSL (METERS) = 0.0442			ZCSL (INCHES) = 1.7468			ZCSL (METERS) = 0.0444		
YCSL (INCHES) = 0.2124			YCSL (METERS) = 0.0054			YCSL (INCHES) = 0.1894			YCSL (METERS) = 0.0048		
LER (INCHES) = 0.110			LER (METERS) = 0.00279			LER (INCHES) = 0.108			LER (METERS) = 0.00274		
TER (INCHES) = 0.117			TER (METERS) = 0.00297			TER (INCHES) = 0.113			TER (METERS) = 0.00287		
X-AREA (SQ. IN.) = 0.5443			X-AREA (SQ. METERS) = 0.00351			X-AREA (SQ. IN.) = 0.5268			X-AREA (SQ. METERS) = 0.00340		
GAMMA-CHORD (DEG.) = 32.36			GAMMA-CHORD (RAD.) = 0.5648			GAMMA-CHORD (DEG.) = 34.35			GAMMA-CHORD (RAD.) = 0.5995		

TABLE XXVI (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES - ROTOR 2

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)			
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS	
.0000	-.0095	.0100		.0000	-.0003	.0097		.0000	-.0093	.0097		.0000	-.0002	.0002	
.0102	-.0083	.0131		.0003	-.0002	.0123		.0100	-.0084	.0123		.0003	-.0002	.0003	
.1096	.0032	.0430		.0028	.0001	.0385		.1099	.0009	.0385		.0028	.0000	.0010	
.2191	.0154	.0747		.0056	.0004	.0661		.2199	.0106	.0661		.0056	.0003	.0017	
.3287	.0268	.1045		.0093	.0007	.0922		.3298	.0197	.0922		.0084	.0005	.0023	
.4382	.0376	.1325		.0111	.0010	.1166		.4398	.0282	.1166		.0112	.0007	.0030	
.5478	.0477	.1587		.0139	.0012	.1393		.5497	.0359	.1393		.0140	.0009	.0035	
.6574	.0572	.1832		.0167	.0015	.1604		.6596	.0430	.1604		.0168	.0011	.0041	
.7669	.0659	.2059		.0195	.0017	.1800		.7696	.0495	.1800		.0195	.0013	.0046	
.8765	.0740	.2269		.0223	.0019	.1981		.8795	.0555	.1981		.0223	.0014	.0050	
.9860	.0814	.2462		.0250	.0021	.2147		.9895	.0609	.2147		.0251	.0015	.0055	
1.0956	.0882	.2638		.0278	.0022	.2297		1.0994	.0657	.2297		.0279	.0017	.0058	
1.2052	.0943	.2797		.0306	.0024	.2433		1.2093	.0699	.2433		.0307	.0018	.0062	
1.3147	.0998	.2941		.0334	.0025	.2554		1.3193	.0736	.2554		.0335	.0019	.0065	
1.4243	.1045	.3064		.0362	.0027	.2661		1.4292	.0768	.2661		.0363	.0020	.0068	
1.5339	.1082	.3162		.0390	.0027	.2747		1.5390	.0793	.2747		.0391	.0020	.0070	
1.6434	.1109	.3230		.0417	.0028	.2807		1.6491	.0809	.2807		.0419	.0021	.0071	
1.7530	.1123	.3268		.0445	.0029	.2848		1.7590	.0817	.2848		.0447	.0021	.0072	
1.8625	.1126	.3277		.0473	.0029	.2888		1.8690	.0815	.2888		.0475	.0021	.0072	
1.9721	.1117	.3256		.0501	.0028	.2929		1.9789	.0806	.2929		.0503	.0020	.0072	
2.0817	.1096	.3205		.0529	.0028	.2970		2.0889	.0787	.2970		.0531	.0020	.0071	
2.1912	.1063	.3125		.0557	.0027	.3011		2.1988	.0760	.3011		.0558	.0019	.0069	
2.3008	.1019	.3014		.0584	.0026	.3052		2.3087	.0725	.3052		.0586	.0018	.0066	
2.4103	.0962	.2872		.0612	.0024	.3093		2.4187	.0680	.3093		.0614	.0017	.0063	
2.5199	.0894	.2700		.0640	.0023	.3134		2.5286	.0628	.3134		.0642	.0016	.0059	
2.6295	.0813	.2496		.0668	.0021	.3175		2.6386	.0567	.3175		.0670	.0014	.0055	
2.7390	.0721	.2259		.0696	.0018	.3216		2.7485	.0497	.3216		.0698	.0013	.0050	
2.8486	.0616	.1990		.0724	.0016	.3257		2.8584	.0419	.3257		.0726	.0011	.0044	
2.9582	.0498	.1686		.0751	.0013	.3298		2.9684	.0333	.3298		.0754	.0008	.0037	
3.0677	.0369	.1347		.0779	.0009	.3339		3.0783	.0239	.3339		.0782	.0006	.0029	
3.1773	.0226	.0971		.0807	.0006	.3380		3.1893	.0137	.3380		.0810	.0003	.0021	
3.2868	.0071	.0555		.0835	.0002	.3421		3.2982	.0026	.3421		.0838	.0001	.0012	
3.3860	-.0079	.0147		.0860	-.0002	.3462		3.3981	-.0080	.3462		.0863	-.0002	.0003	
3.3964	-.0095	.0105		.0883	-.0002	.3503		3.4082	-.0091	.3503		.0886	-.0002	.0002	
RADIUS (INCHES) = 10.381				RADIUS (METERS) = .2789				RADIUS (INCHES) = 11.481				RADIUS (METERS) = .2916			
CHORD (INCHES) = 3.396				CHORD (METERS) = .0863				CHORD (INCHES) = 3.408				CHORD (METERS) = .0866			
ZCSSL (INCHES) = 1.7556				ZCSSL (METERS) = .0446				ZCSSL (INCHES) = 1.7646				ZCSSL (METERS) = .0448			
YCSSL (INCHES) = .1628				YCSSL (METERS) = .0041				YCSSL (INCHES) = .1327				YCSSL (METERS) = .0034			
LER (INCHES) = .0104				LER (METERS) = .000264				LER (INCHES) = .0101				LER (METERS) = .000257			
TER (INCHES) = .0108				TER (METERS) = .000274				TER (INCHES) = .0104				TER (METERS) = .000264			
X-AREA (SQ. IN.) = .5040				X-AREA (SQ. METERS) = .000325				X-AREA (SQ. IN.) = .4757				X-AREA (SQ. METERS) = .000307			
GAMMA-CHORD(180.0) = 37.01				GAMMA-CHORD(180.0) = .6499				GAMMA-CHORD(180.0) = 40.16				GAMMA-CHORD(180.0) = .7009			

TABLE XXVI (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-.0000	-.0089	-.0092	.0000	-.0002	.0002	.0000	-.0085	.0088	.0000	-.0002	.0002
-.0096	-.0083	-.0113	-.0002	-.0002	.0003	.0092	-.0081	.0105	.0002	-.0002	.0003
.1102	-.0019	.0334	.0028	-.0000	.0018	.1105	-.0036	.0295	.0028	-.0001	.0007
.2205	.0048	.0567	.0056	.0001	.0014	.2203	.0010	.0494	.0056	.0000	.0013
.3308	.0111	.0786	.0084	.0003	.0020	.3314	.0053	.0682	.0084	.0001	.0017
.4410	.0169	.0992	.0112	.0004	.0025	.4419	.0092	.0858	.0112	.0002	.0022
.5513	.0224	.1186	.0140	.0006	.0030	.5524	.0128	.1024	.0140	.0003	.0026
.6615	.0274	.1367	.0168	.0007	.0035	.6628	.0161	.1178	.0168	.0004	.0030
.7718	.0320	.1535	.0196	.0008	.0039	.7733	.0190	.1322	.0196	.0005	.0034
.8820	.0363	.1690	.0224	.0009	.0043	.8838	.0217	.1454	.0224	.0006	.0037
.9923	.0401	.1833	.0252	.0010	.0047	.9943	.0241	.1576	.0253	.0006	.0040
1.1025	.0435	.1964	.0280	.0011	.0050	1.1047	.0261	.1687	.0281	.0007	.0043
1.2128	.0465	.2082	.0308	.0012	.0053	1.2152	.0279	.1787	.0309	.0007	.0045
1.3230	.0491	.2187	.0336	.0012	.0056	1.3257	.0294	.1877	.0337	.0007	.0048
1.4333	.0513	.2282	.0364	.0013	.0058	1.4361	.0307	.1958	.0365	.0008	.0050
1.5435	.0533	.2360	.0392	.0013	.0060	1.5466	.0316	.2026	.0393	.0008	.0051
1.6538	.0549	.2417	.0420	.0014	.0061	1.6571	.0322	.2078	.0421	.0008	.0053
1.7640	.0563	.2452	.0448	.0014	.0062	1.7676	.0324	.2110	.0449	.0008	.0054
1.8743	.0578	.2462	.0476	.0014	.0063	1.8780	.0322	.2121	.0477	.0008	.0054
1.9846	.0591	.2449	.0504	.0014	.0062	1.9885	.0317	.2111	.0505	.0008	.0054
2.0948	.0528	.2412	.0532	.0013	.0061	2.0990	.0308	.2081	.0533	.0008	.0053
2.2051	.0508	.2351	.0560	.0013	.0060	2.2095	.0294	.2030	.0561	.0007	.0052
2.3153	.0483	.2267	.0588	.0012	.0058	2.3199	.0278	.1958	.0589	.0007	.0050
2.4256	.0451	.2159	.0616	.0011	.0055	2.4304	.0257	.1866	.0617	.0007	.0047
2.5358	.0413	.2027	.0644	.0010	.0051	2.5409	.0232	.1752	.0645	.0006	.0045
2.6461	.0370	.1871	.0672	.0009	.0048	2.6513	.0204	.1618	.0673	.0005	.0041
2.7563	.0320	.1691	.0700	.0008	.0043	2.7618	.0173	.1463	.0702	.0004	.0037
2.8666	.0266	.1487	.0728	.0007	.0038	2.8723	.0138	.1287	.0730	.0004	.0033
2.9768	.0205	.1258	.0756	.0005	.0032	2.9828	.0100	.1090	.0758	.0003	.0028
3.0871	.0139	.1004	.0784	.0004	.0026	3.0932	.0058	.0872	.0786	.0001	.0022
3.1973	.0069	.0725	.0812	.0002	.0018	3.2037	.0014	.0632	.0814	.0000	.0016
3.3076	-.0008	.0419	.0840	-.0000	.0011	3.3142	-.0033	.0369	.0842	-.0001	.0009
3.4082	-.0079	.0120	.0866	-.0002	.0003	3.4155	-.0079	.0111	.0868	-.0002	.0003
3.4178	-.0086	.0092	.0868	-.0002	.0002	3.4247	-.0083	.0087	.0870	-.0002	.0002
RADIUS (INCHES)	= 11.980		RADIUS (METERS)	= .3043		RADIUS (INCHES)	= 12.479		RADIUS (METERS)	= .3170	
CHORD (INCHES)	= 3.418		CHORD (METERS)	= .0868		CHORD (INCHES)	= 3.425		CHORD (METERS)	= .0870	
ZCSL (INCHES)	= 1.7727		ZCSL (METERS)	= .0450		ZCSL (INCHES)	= 1.7791		ZCSL (METERS)	= .0452	
YCSSL (INCHES)	= .1052		YCSSL (METERS)	= .0027		YCSSL (INCHES)	= .0819		YCSSL (METERS)	= .0021	
LER (INCHES)	= .0097		LER (METERS)	= .000246		LER (INCHES)	= .0092		LER (METERS)	= .000234	
TER (INCHES)	= .0098		TER (METERS)	= .000249		TER (INCHES)	= .0093		TER (METERS)	= .000236	
X-AREA (SQ. IN.)	= .4476		X-AREA (SQ. METERS)	= .000289		X-AREA (SQ. IN.)	= .4511		X-AREA (SQ. METERS)	= .000271	
GAMMA-CHORD (DEG.)	= 43.16		GAMMA-CHORD (RAD.)	= .7532		GAMMA-CHORD (DEG.)	= 45.11		GAMMA-CHORD (RAD.)	= .7873	

TABLE XXVI (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES - ROTOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-0.000	-0.079	-0.080	-0.000	-0.002	-0.002	-0.000	-0.080	-0.081	-0.000	-0.002	-0.002
-0.008	-0.076	-0.093	-0.002	-0.002	-0.002	-0.008	-0.077	-0.093	-0.002	-0.002	-0.002
-1.108	-0.044	-0.260	-0.028	-0.001	-0.007	-1.109	-0.048	-0.267	-0.028	-0.001	-0.006
-2.217	-0.011	-0.431	-0.056	-0.000	-0.014	-2.218	-0.020	-0.407	-0.056	-0.001	-0.010
-3.325	-0.019	-0.592	-0.084	-0.000	-0.015	-3.326	-0.006	-0.559	-0.084	-0.000	-0.014
-4.434	-0.045	-0.743	-0.113	-0.001	-0.019	-4.435	-0.029	-0.701	-0.113	-0.001	-0.018
-5.542	-0.069	-0.885	-0.141	-0.002	-0.022	-5.544	-0.050	-0.834	-0.141	-0.001	-0.021
-6.650	-0.090	-1.016	-0.169	-0.002	-0.026	-6.653	-0.068	-0.959	-0.169	-0.002	-0.024
-7.759	-0.108	-1.137	-0.197	-0.003	-0.029	-7.761	-0.093	-1.074	-0.197	-0.002	-0.027
-8.867	-0.123	-1.248	-0.225	-0.003	-0.032	-8.870	-0.095	-1.180	-0.225	-0.002	-0.030
-9.975	-0.136	-1.350	-0.253	-0.003	-0.034	-9.979	-0.106	-1.277	-0.253	-0.003	-0.032
-1.1084	-0.146	-1.442	-0.282	-0.004	-0.037	-1.1088	-0.114	-1.365	-0.282	-0.003	-0.035
-1.2192	-0.153	-1.525	-0.310	-0.004	-0.039	-1.2197	-0.119	-1.445	-0.310	-0.003	-0.037
-1.3301	-0.157	-1.597	-0.338	-0.004	-0.041	-1.3305	-0.123	-1.515	-0.338	-0.003	-0.038
-1.4409	-0.159	-1.661	-0.366	-0.004	-0.042	-1.4414	-0.124	-1.577	-0.366	-0.003	-0.040
-1.5517	-0.159	-1.716	-0.394	-0.004	-0.045	-1.5523	-0.123	-1.631	-0.394	-0.003	-0.041
-1.6626	-0.156	-1.759	-0.422	-0.004	-0.045	-1.6632	-0.120	-1.675	-0.422	-0.003	-0.043
-1.7734	-0.151	-1.785	-0.450	-0.004	-0.045	-1.7741	-0.116	-1.703	-0.451	-0.003	-0.043
-1.8843	-0.144	-1.796	-0.479	-0.004	-0.046	-1.8849	-0.110	-1.714	-0.479	-0.003	-0.044
-1.9951	-0.136	-1.787	-0.507	-0.003	-0.045	-1.9958	-0.102	-1.707	-0.507	-0.003	-0.043
-2.1059	-0.126	-1.761	-0.535	-0.003	-0.045	-2.1067	-0.093	-1.684	-0.535	-0.002	-0.043
-2.2168	-0.114	-1.717	-0.563	-0.003	-0.044	-2.2176	-0.083	-1.642	-0.563	-0.002	-0.042
-2.3276	-0.101	-1.656	-0.591	-0.003	-0.042	-2.3284	-0.071	-1.584	-0.591	-0.002	-0.040
-2.4385	-0.086	-1.577	-0.619	-0.002	-0.040	-2.4393	-0.059	-1.509	-0.620	-0.001	-0.038
-2.5493	-0.071	-1.481	-0.647	-0.001	-0.038	-2.5502	-0.045	-1.417	-0.648	-0.001	-0.036
-2.6601	-0.054	-1.367	-0.676	-0.001	-0.035	-2.6611	-0.032	-1.308	-0.676	-0.001	-0.033
-2.7710	-0.037	-1.235	-0.704	-0.001	-0.033	-2.7720	-0.017	-1.182	-0.704	-0.000	-0.030
-2.8818	-0.019	-1.086	-0.732	-0.000	-0.028	-2.8828	-0.002	-1.040	-0.732	-0.000	-0.026
-2.9927	-0.000	-0.920	-0.760	-0.000	-0.023	-2.9937	-0.013	-0.881	-0.760	-0.000	-0.022
-3.1035	-0.019	-0.736	-0.788	-0.000	-0.019	-3.1046	-0.029	-0.705	-0.789	-0.001	-0.018
-3.2143	-0.038	-0.534	-0.816	-0.001	-0.014	-3.2155	-0.044	-0.512	-0.817	-0.001	-0.013
-3.3252	-0.057	-0.314	-0.845	-0.001	-0.008	-3.3264	-0.060	-0.303	-0.845	-0.002	-0.008
-3.4360	-0.074	-0.097	-0.871	-0.002	-0.002	-3.4368	-0.075	-0.096	-0.871	-0.002	-0.002
			-0.873	-0.002	-0.002	-3.4372	-0.075	-0.079	-0.873	-0.002	-0.002
RADIUS (INCHES) = 13.172						RADIUS (INCHES) = 13.363					
CHORD (INCHES) = 3.436						CHORD (INCHES) = 3.437					
ZCSSL (INCHES) = 1.7961						ZCSSL (INCHES) = 1.7931					
YCSSL (INCHES) = -0.606						YCSSL (INCHES) = -0.553					
LER (INCHES) = -0.084						LER (INCHES) = -0.085					
TER (INCHES) = -0.085						TER (INCHES) = -0.085					
X-AREA (SQ. IN.) = -0.3872						X-AREA (SQ. IN.) = -0.3755					
GAMMA-CHORD (DEG.) = 47.56						GAMMA-CHORD (DEG.) = 48.49					
RADIUS (METERS) = 0.3346						RADIUS (METERS) = 0.3394					
CHORD (METERS) = 0.0873						CHORD (METERS) = 0.0873					
ZCSSL (METERS) = -0.0455						ZCSSL (METERS) = -0.0455					
YCSSL (METERS) = -0.015						YCSSL (METERS) = -0.014					
LER (METERS) = -0.00213						LER (METERS) = -0.00216					
TER (METERS) = -0.00216						TER (METERS) = -0.00216					
X-AREA (SQ. METERS) = -0.00250						X-AREA (SQ. METERS) = -0.00242					
GAMMA-CHORD (RAD.) = 0.8301						GAMMA-CHORD (RAD.) = 0.8464					

TABLE XXVI (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0081	-.0082	.0000	-.0002	-.0002	.0000	-.0078	.0078	.0000	-.0002	.0002
.0005	-.0078	.0093	.0002	-.0002	.0002	.0081	-.0076	.0087	.0002	-.0002	.0002
.0109	-.0051	.0226	.0028	-.0001	.0006	.1110	-.0056	.0200	.0028	-.0001	.0005
.2218	-.0024	.0364	.0056	-.0001	.0039	.2220	-.0034	.0318	.0056	-.0001	.0008
.3328	.0001	.0497	.0085	.0000	.0013	.3331	-.0014	.0431	.0085	-.0000	.0011
.4437	.0023	.0622	.0113	.0001	.0016	.4441	.0005	.0538	.0113	.0000	.0014
.5546	.0044	.0740	.0141	.0001	.0019	.5551	.0024	.0641	.0141	.0001	.0016
.6656	.0062	.0851	.0169	.0002	.0022	.6661	.0042	.0738	.0169	.0001	.0019
.7765	.0079	.0955	.0197	.0002	.0024	.7771	.0058	.0829	.0197	.0001	.0021
.8874	.0093	.1052	.0225	.0002	.0027	.8882	.0074	.0916	.0225	.0002	.0023
.9983	.0105	.1141	.0254	.0003	.0029	.9992	.0090	.0996	.0254	.0002	.0025
1.1093	.0115	.1223	.0282	.0003	.0031	1.1102	.0104	.1071	.0282	.0003	.0027
1.2202	.0124	.1297	.0310	.0003	.0033	1.2212	.0118	.1141	.0310	.0003	.0029
1.3311	.0131	.1364	.0338	.0003	.0035	1.3323	.0131	.1205	.0338	.0003	.0031
1.4420	.0137	.1424	.0366	.0003	.0036	1.4433	.0145	.1263	.0366	.0004	.0032
1.5530	.0141	.1478	.0394	.0004	.0038	1.5543	.0158	.1319	.0395	.0004	.0033
1.6639	.0145	.1522	.0423	.0004	.0039	1.6653	.0171	.1366	.0423	.0004	.0035
1.7748	.0146	.1553	.0451	.0004	.0039	1.7763	.0182	.1403	.0451	.0005	.0036
1.8857	.0145	.1568	.0479	.0004	.0040	1.8874	.0189	.1424	.0479	.0005	.0036
1.9967	.0140	.1566	.0507	.0004	.0040	1.9984	.0192	.1429	.0508	.0005	.0036
2.1076	.0134	.1547	.0535	.0003	.0039	2.1094	.0191	.1418	.0536	.0005	.0036
2.2185	.0126	.1511	.0564	.0003	.0038	2.2204	.0186	.1391	.0564	.0005	.0035
2.3294	.0115	.1459	.0592	.0003	.0037	2.3315	.0178	.1348	.0592	.0005	.0034
2.4404	.0103	.1391	.0620	.0003	.0035	2.4425	.0167	.1290	.0620	.0004	.0033
2.5513	.0089	.1308	.0648	.0002	.0033	2.5535	.0153	.1216	.0649	.0004	.0031
2.6622	.0073	.1208	.0676	.0002	.0031	2.6645	.0135	.1127	.0677	.0003	.0029
2.7732	.0056	.1093	.0704	.0001	.0028	2.7755	.0114	.1022	.0705	.0003	.0026
2.8841	.0039	.0962	.0733	.0001	.0024	2.8866	.0090	.0902	.0733	.0002	.0023
2.9950	.0017	.0916	.0761	.0000	.0021	2.9976	.0063	.0767	.0761	.0002	.0019
3.1059	-.0004	.0654	.0789	-.0000	.0017	3.1086	.0033	.0617	.0790	.0001	.0016
3.2169	-.0027	.0478	.0817	-.0001	.0012	3.2196	-.0001	.0452	.0818	-.0000	.0011
3.3278	-.0052	.0286	.0845	-.0001	.0007	3.3307	-.0037	.0272	.0846	-.0001	.0007
3.4302	-.0076	.0097	.0871	-.0002	.0002	3.4335	-.0073	.0093	.0872	-.0002	.0002
3.4387	-.0078	.0081	.0873	-.0002	.0002	3.4417	-.0076	.0079	.0874	-.0002	.0002
RADIUS (INCHES) = 13.553			RADIUS (METERS) = 3.442			RADIUS (INCHES) = 13.745			RADIUS (METERS) = 3.491		
CHORD (INCHES) = 3.439			CHORD (METERS) = .0873			CHORD (INCHES) = 3.442			CHORD (METERS) = .0874		
ZCSSL (INCHES) = 1.7947			ZCSSL (METERS) = .0456			ZCSSL (INCHES) = 1.7942			ZCSSL (METERS) = .0456		
YCSSL (INCHES) = .0497			YCSSL (METERS) = .0013			YCSSL (INCHES) = .0444			YCSSL (METERS) = .0011		
LER (INCHES) = .0085			LER (METERS) = .000216			LER (INCHES) = .0082			LER (METERS) = .000208		
TER (INCHES) = .0086			TER (METERS) = .000218			TER (INCHES) = .0082			TER (METERS) = .000208		
X-AREA (SQ. IN.) = .3343			X-AREA (SQ. METERS) = .000216			X-AREA (SQ. IN.) = .2930			X-AREA (SQ. METERS) = .000189		
GAMMA-CHORD( DEG.) = 49.71			GAMMA-CHORD( RAD.) = .8677			GAMMA-CHORD( DEG.) = 50.86			GAMMA-CHORD( RAD.) = .8876		

TABLE XXVI (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES – ROTOR 2

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)							
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS					
-0.000	-0.017	0.078		0.000	-0.002	0.002		0.000	-0.074	0.074		0.000	-0.002	0.074					
-0.080	-0.076	0.095		0.002	-0.002	0.002		0.077	-0.074	0.080		0.002	-0.002	0.080					
-0.111	-0.064	0.183		0.028	-0.002	0.005		0.113	-0.075	0.158		0.028	-0.002	0.158					
-0.222	-0.031	0.286		0.056	-0.001	0.007		0.225	-0.075	0.239		0.057	-0.002	0.239					
-0.333	-0.038	0.364		0.085	-0.001	0.010		0.338	-0.073	0.319		0.085	-0.002	0.319					
-0.445	-0.024	0.479		0.113	-0.001	0.012		0.451	-0.070	0.396		0.113	-0.002	0.396					
-0.556	-0.009	0.571		0.141	-0.000	0.014		0.564	-0.064	0.544		0.141	-0.002	0.544					
-0.667	0.006	0.658		0.169	-0.000	0.017		0.676	-0.057	0.615		0.170	-0.001	0.615					
-0.778	0.021	0.741		0.198	0.001	0.019		0.789	-0.047	0.683		0.198	-0.001	0.683					
-0.889	0.037	0.820		0.226	0.001	0.021		0.890	-0.036	0.759		0.226	-0.001	0.759					
-0.999	0.053	0.896		0.254	0.001	0.023		1.0015	-0.023	0.814		0.254	-0.001	0.814					
-1.111	0.070	0.967		0.282	0.002	0.025		1.1127	-0.003	0.877		0.283	-0.000	0.877					
-1.222	0.088	1.035		0.310	0.002	0.026		1.2240	-0.003	0.937		0.311	-0.000	0.937					
-1.334	0.106	1.099		0.339	0.003	0.028		1.3353	0.027	0.995		0.339	0.001	0.995					
-1.445	0.125	1.159		0.367	0.003	0.029		1.4465	0.048	1.055		0.367	0.001	1.055					
-1.556	0.146	1.217		0.395	0.004	0.031		1.5578	0.072	1.117		0.396	0.002	1.117					
-1.667	0.168	1.270		0.423	0.004	0.032		1.6691	0.099	1.180		0.424	0.003	1.180					
-1.778	0.187	1.314		0.452	0.005	0.033		1.7804	0.125	1.243		0.452	0.003	1.243					
-1.889	0.203	1.344		0.480	0.005	0.034		1.8916	0.148	1.295		0.480	0.004	1.295					
-1.999	0.213	1.357		0.508	0.005	0.034		2.0029	0.165	1.347		0.509	0.004	1.347					
-2.112	0.218	1.353		0.536	0.006	0.034		2.1142	0.177	1.399		0.537	0.004	1.399					
-2.223	0.218	1.344		0.564	0.006	0.034		2.2255	0.183	1.451		0.565	0.005	1.451					
-2.334	0.214	1.299		0.593	0.005	0.033		2.3367	0.184	1.503		0.594	0.005	1.503					
-2.445	0.204	1.247		0.621	0.005	0.032		2.4480	0.180	1.555		0.622	0.005	1.555					
-2.556	0.191	1.190		0.649	0.005	0.030		2.5593	0.171	1.607		0.622	0.004	1.607					
-2.667	0.172	1.097		0.677	0.004	0.028		2.6706	0.157	1.659		0.622	0.004	1.659					
-2.778	0.150	0.998		0.706	0.004	0.025		2.7818	0.138	1.711		0.622	0.003	1.711					
-2.889	0.123	0.884		0.734	0.003	0.022		2.8931	0.114	1.763		0.622	0.003	1.763					
-2.999	0.099	0.778		0.762	0.002	0.019		3.0044	0.085	1.815		0.622	0.002	1.815					
-3.112	0.056	0.608		0.790	0.001	0.015		3.1156	0.053	1.867		0.622	0.001	1.867					
-3.223	0.016	0.445		0.818	0.000	0.011		3.2269	0.015	1.919		0.622	0.000	1.919					
-3.334	-0.028	0.269		0.847	-0.001	0.007		3.3392	-0.026	1.971		0.622	-0.001	1.971					
-3.445	-0.071	0.091		0.873	-0.002	0.002		3.4418	-0.069	2.023		0.622	-0.002	2.023					
-3.556	-0.175	0.077		0.875	-0.002	0.002		3.5495	-0.072	2.075		0.622	-0.002	2.075					
								RADIUS (INCHES) = 14.376								RADIUS (METERS) = 0.3652			
								CHORD (INCHES) = 3.449								CHORD (METERS) = 0.0875			
								ZCSL (INCHES) = 1.7987								ZCSL (METERS) = 0.0457			
								YCSL (INCHES) = 0.0307								YCSL (METERS) = 0.0008			
								LER (INCHES) = 0.0177								LER (METERS) = 0.00196			
								TER (INCHES) = 0.0077								TER (METERS) = 0.00163			
								X-AREA (SQ. IN.) = 2.521								X-AREA (SQ. METERS) = 0.00163			
								GAMMA-CHORD( DEG.) = 53.79								GAMMA-CHORD( RAD.) = 0.9389			

TABLE XXVI (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
.0000	-.0071	.0074	.0000	-.0002	.0002	.0000	-.0069	.0069	.0000	-.0002	.0012
.0075	-.0072	.0078	.0002	-.0002	.0002	.0072	-.0071	.0072	.0002	-.0002	.0002
.1115	-.0088	.0142	.0028	-.0002	.0004	.1117	-.0101	.0121	.0028	-.0003	.0033
.2230	-.0103	.0208	.0057	-.0003	.0005	.2234	-.0130	.0173	.0057	-.0003	.0004
.3345	-.0115	.0271	.0085	-.0003	.0007	.3351	-.0155	.0225	.0085	-.0004	.0036
.4460	-.0124	.0334	.0113	-.0003	.0008	.4468	-.0176	.0277	.0113	-.0004	.0037
.5575	-.0130	.0396	.0142	-.0003	.0010	.5585	-.0192	.0330	.0142	-.0005	.0008
.6690	-.0133	.0459	.0170	-.0003	.0012	.6702	-.0204	.0383	.0170	-.0005	.0010
.7805	-.0133	.0520	.0198	-.0003	.0013	.7819	-.0212	.0436	.0198	-.0005	.0011
.8920	-.0130	.0581	.0227	-.0003	.0015	.8936	-.0215	.0490	.0227	-.0005	.0012
1.0035	-.0124	.0639	.0255	-.0003	.0016	1.0052	-.0215	.0543	.0255	-.0005	.0014
1.1150	-.0115	.0696	.0283	-.0003	.0018	1.1169	-.0210	.0596	.0284	-.0005	.0015
1.2265	-.0103	.0752	.0312	-.0003	.0019	1.2286	-.0200	.0650	.0312	-.0005	.0017
1.3380	-.0088	.0807	.0340	-.0002	.0021	1.3403	-.0187	.0704	.0340	-.0005	.0018
1.4495	-.0069	.0863	.0368	-.0002	.0022	1.4520	-.0169	.0759	.0369	-.0004	.0019
1.5610	-.0047	.0919	.0396	-.0001	.0023	1.5637	-.0146	.0814	.0397	-.0004	.0021
1.6725	-.0021	.0973	.0425	-.0001	.0025	1.6754	-.0118	.0871	.0426	-.0003	.0022
1.7840	-.0008	.1025	.0453	-.0000	.0026	1.7871	-.0085	.0929	.0454	-.0002	.0024
1.8955	.0036	.1067	.0481	.0001	.0027	1.8988	-.0051	.0980	.0482	-.0001	.0025
2.0070	.0059	.1096	.0510	.0001	.0028	2.0105	-.0020	.1019	.0511	-.0001	.0026
2.1185	.0077	.1110	.0538	.0002	.0028	2.1222	.0005	.1042	.0539	.0000	.0026
2.2300	.0090	.1108	.0566	.0002	.0028	2.2339	.0026	.1049	.0567	.0001	.0027
2.3415	.0098	.1091	.0595	.0002	.0028	2.3456	.0041	.1040	.0596	.0001	.0026
2.4530	.0102	.1058	.0623	.0003	.0027	2.4573	.0052	.1015	.0624	.0001	.0026
2.5645	.0100	.1010	.0651	.0003	.0026	2.5690	.0058	.0974	.0653	.0001	.0025
2.6760	.0094	.0946	.0680	.0002	.0024	2.6807	.0059	.0917	.0681	.0001	.0023
2.7875	.0084	.0867	.0708	.0002	.0022	2.7924	.0055	.0844	.0709	.0001	.0021
2.8990	.0069	.0772	.0736	.0002	.0020	2.9041	.0047	.0755	.0738	.0001	.0019
3.0105	.0050	.0662	.0765	.0001	.0017	3.0158	.0034	.0649	.0766	.0001	.0016
3.1220	.0027	.0537	.0793	.0001	.0014	3.1274	.0016	.0528	.0794	.0000	.0013
3.2335	-.0000	.0396	.0821	-.0000	.0010	3.2391	-.0007	.0390	.0823	-.0000	.0010
3.3450	-.0032	.0240	.0850	-.0001	.0006	3.3508	-.0034	.0236	.0851	-.0001	.0006
3.4565	-.0064	.0080	.0876	-.0002	.0002	3.4596	-.0063	.0077	.0878	-.0002	.0002
3.5680	-.0067	.0069	.0878	-.0002	.0002	3.5625	-.0065	.0067	.0879	-.0002	.0002
RADIUS (INCHES) = 14.976			RADIUS (METERS) = .3804			RADIUS (INCHES) = 15.475			RADIUS (METERS) = .3931		
CHORD (INCHES) = 3.456			CHORD (METERS) = .0878			CHORD (INCHES) = 3.463			CHORD (METERS) = .0880		
ZCGL (INCHES) = 1.8030			ZCGL (METERS) = .0458			ZCGL (INCHES) = 1.8107			ZCGL (METERS) = .0460		
YCGL (INCHES) = .0199			YCGL (METERS) = .0005			YCGL (INCHES) = .0120			YCGL (METERS) = .0003		
LER (INCHES) = .0075			LER (METERS) = .000190			LER (INCHES) = .0072			LER (METERS) = .000183		
TER (INCHES) = .0072			TER (METERS) = .000183			TER (INCHES) = .0070			TER (METERS) = .000178		
X-AREA (SQ. IN.) = .2495			X-AREA (SQ. METERS) = .000161			X-AREA (SQ. IN.) = .2495			X-AREA (SQ. METERS) = .000161		
GAMMA-CHORD( DEG.) = 55.87			GAMMA-CHORD(RAD.) = .9750			GAMMA-CHORD( DEG.) = 57.57			GAMMA-CHORD(RAD.) = 1.0048		

TABLE XXVI (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES -- ROTOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-.0000	-.0067	.0067	.0000	-.0068	.0067	.0000	-.0068	.0067	.0000	-.0068	.0067
.0070	-.0070	.0069	.0070	-.0070	.0070	.0070	-.0070	.0070	.0070	-.0070	.0070
.1120	-.0110	.0111	.1120	-.0103	.0117	.1120	-.0103	.0117	.0028	-.0003	.0003
.2239	-.0146	.0155	.2241	-.0132	.0169	.2241	-.0132	.0169	.0057	-.0003	.0004
.3359	-.0177	.0202	.3361	-.0136	.0222	.3361	-.0136	.0222	.0095	-.0004	.0006
.4478	-.0201	.0249	.4482	-.0174	.0277	.4482	-.0174	.0277	.0114	-.0004	.0007
.5598	-.0221	.0298	.5602	-.0196	.0334	.5602	-.0196	.0334	.0142	-.0005	.0008
.6718	-.0235	.0349	.6722	-.0132	.0393	.6722	-.0132	.0393	.0171	-.0005	.0010
.7837	-.0243	.0401	.7843	-.0192	.0453	.7843	-.0192	.0453	.0199	-.0005	.0012
.8957	-.0246	.0456	.8963	-.0186	.0516	.8963	-.0186	.0516	.0228	-.0005	.0013
1.0076	-.0242	.0512	1.0083	-.0174	.0580	1.0083	-.0174	.0580	.0256	-.0004	.0015
1.1196	-.0233	.0570	1.1204	-.0156	.0647	1.1204	-.0156	.0647	.0285	-.0004	.0016
1.2315	-.0218	.0629	1.2324	-.0132	.0715	1.2324	-.0132	.0715	.0313	-.0003	.0018
1.3435	-.0196	.0691	1.3445	-.0101	.0786	1.3445	-.0101	.0786	.0341	-.0003	.0020
1.4555	-.0169	.0754	1.4565	-.0064	.0860	1.4565	-.0064	.0860	.0370	-.0002	.0022
1.5674	-.0137	.0820	1.5685	-.0021	.0935	1.5685	-.0021	.0935	.0398	-.0001	.0024
1.6794	-.0096	.0889	1.6906	.0029	.1014	1.6906	.0029	.1014	.0427	.0001	.0026
1.7913	-.0049	.0962	1.7926	.0087	.1098	1.7926	.0087	.1098	.0455	.0002	.0028
1.9033	.0002	.1032	1.9047	.0149	.1180	1.9047	.0149	.1180	.0484	.0004	.0030
2.0153	.0052	.1092	2.0167	.0210	.1251	2.0167	.0210	.1251	.0512	.0005	.0032
2.1272	.0094	.1135	2.1287	.0260	.1303	2.1287	.0260	.1303	.0541	.0007	.0033
2.2392	.0128	.1157	2.2408	.0300	.1331	2.2408	.0300	.1331	.0569	.0008	.0034
2.3511	.0154	.1160	2.3528	.0328	.1337	2.3528	.0328	.1337	.0598	.0008	.0034
2.4631	.0171	.1143	2.4649	.0344	.1319	2.4649	.0344	.1319	.0626	.0009	.0034
2.5751	.0180	.1107	2.5769	.0349	.1278	2.5769	.0349	.1278	.0655	.0009	.0032
2.6870	.0187	.1049	2.6889	.0341	.1213	2.6889	.0341	.1213	.0683	.0009	.0031
2.7990	.0174	.0972	2.8010	.0322	.1125	2.8010	.0322	.1125	.0711	.0008	.0029
2.9109	.0157	.0875	2.9130	.0290	.1012	2.9130	.0290	.1012	.0740	.0007	.0026
3.0229	.0132	.0757	3.0251	.0245	.0874	3.0251	.0245	.0874	.0768	.0006	.0022
3.1349	.0098	.0617	3.1371	.0188	.0712	3.1371	.0188	.0712	.0797	.0005	.0019
3.2468	.0053	.0456	3.2491	.0117	.0523	3.2491	.0117	.0523	.0825	.0003	.0013
3.3588	-.0001	.0271	3.3612	.0033	.0308	3.3612	.0033	.0308	.0854	.0001	.0008
3.4707	-.0065	.0068	3.4663	-.0059	.0083	3.4663	-.0059	.0083	.0880	-.0001	.0002
			3.4732	-.0065	.0068	3.4732	-.0065	.0068	.0882	-.0002	.0002
						RADIUS (INCHES) = 16.425					
						CHORD (INCHES) = 3.473					
						ZCSSL (INCHES) = 1.8221					
						YCSSL (INCHES) = .0252					
						LER (INCHES) = .0070					
						TER (INCHES) = .0070					
						X-AREA (SQ. IN.) = .2513					
						GAMMA-CHORD(1/2) = 59.55					
						RADIUS (METERS) = .4172					
						CHORD (METERS) = .0882					
						ZCSSL (METERS) = .0463					
						YCSSL (METERS) = .0006					
						LER (METERS) = .000178					
						TER (METERS) = .000178					
						X-AREA (SQ. METERS) = .000162					
						GAMMA-CHORD(1/2) = 1.0351					

TABLE XXVI (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES — ROTOR 2

English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS
.0000	-.0069	.0067	.0000	-.0002	.0022
.0071	-.0071	.0071	.0002	-.0002	.0002
.1121	-.0100	.0121	.0029	-.0003	.0033
.2241	-.0126	.0176	.0057	-.0003	.0004
.3362	-.0147	.0232	.0085	-.0004	.0006
.4483	-.0161	.0291	.0114	-.0004	.0007
.5604	-.0169	.0352	.0142	-.0004	.0009
.6724	-.0171	.0414	.0171	-.0004	.0011
.7845	-.0166	.0479	.0199	-.0004	.0012
.8966	-.0156	.0545	.0228	-.0004	.0014
1.0086	-.0140	.0615	.0256	-.0004	.0016
1.1207	-.0117	.0686	.0285	-.0003	.0017
1.2328	-.0088	.0759	.0313	-.0002	.0019
1.3449	-.0053	.0835	.0342	-.0001	.0021
1.4569	-.0011	.0913	.0370	-.0000	.0023
1.5690	.0037	.0993	.0399	.0001	.0025
1.6811	.0092	.1078	.0427	.0002	.0027
1.7932	.0156	.1168	.0455	.0004	.0030
1.9052	.0225	.1256	.0484	.0006	.0032
2.0173	.0291	.1333	.0512	.0007	.0034
2.1294	.0347	.1390	.0541	.0009	.0035
2.2414	.0390	.1422	.0569	.0010	.0036
2.3535	.0419	.1430	.0598	.0011	.0036
2.4656	.0435	.1412	.0626	.0011	.0036
2.5777	.0437	.1369	.0655	.0011	.0035
2.6997	.0426	.1300	.0683	.0011	.0033
2.8018	.0401	.1206	.0712	.0010	.0031
2.9139	.0361	.1085	.0740	.0009	.0028
3.0260	.0306	.0938	.0769	.0008	.0024
3.1380	.0237	.0763	.0797	.0006	.0019
3.2501	.0152	.0560	.0826	.0004	.0014
3.3622	.0051	.0328	.0854	.0001	.0008
3.4674	-.0058	.0084	.0881	-.0001	.0002
3.5742	-.0065	.0069	.0882	-.0002	.0002
RADIUS (INCHES) = 16.575			RADIUS (METERS) = .4210		
CHORD (INCHES) = 3.474			CHORD (METERS) = .0882		
ZCSL (INCHES) = 1.8231			ZCSL (METERS) = .0463		
YCSL (INCHES) = .0308			YCSL (METERS) = .0008		
LER (INCHES) = .0071			LER (METERS) = .000180		
TER (INCHES) = .0070			TER (METERS) = .000179		
X-AREA (SQ. IN.) = .2517			X-AREA (SQ. METERS) = .000162		
GAMMA-CHORD (DEG.) = 59.71			GAMMA-CHORD (RAD.) = 1.0422		

TABLE XXVII

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES - STATOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-.0014	.0041	.0041	-.0000	.0001	.0001	-.0012	.0039	.0039	-.0000	.0001	.0001	-.0012	.0039	.0039	-.0000	.0001	.0001
.0011	-.0011	.0118	.0000	-.0000	.0003	.0012	-.0014	.0113	.0000	-.0000	.0003	.0012	-.0014	.0113	.0000	-.0000	.0003
.0035	.0025	.0162	.0001	-.0001	.0004	.0036	-.0001	.0156	.0001	-.0001	.0004	.0036	-.0001	.0156	.0001	-.0001	.0004
.0059	-.0029	.0198	.0001	-.0001	.0005	.0061	-.0031	.0189	.0002	-.0002	.0005	.0061	-.0031	.0189	.0002	-.0002	.0005
.0083	.0028	.0230	.0002	-.0001	.0006	.0085	-.0032	.0220	.0002	-.0002	.0006	.0085	-.0032	.0220	.0002	-.0002	.0006
.0296	.0026	.0461	.0008	.0001	.0012	.0297	.0011	.0436	.0008	.0008	.0011	.0297	.0011	.0436	.0008	.0008	.0011
.0509	.0118	.0656	.0013	.0003	.0017	.0510	.0032	.0616	.0013	.0002	.0016	.0510	.0032	.0616	.0013	.0002	.0016
.0722	.0219	.0835	.0018	.0006	.0021	.0722	.0181	.0788	.0018	.0005	.0020	.0722	.0181	.0788	.0018	.0005	.0020
.0935	.0320	.1011	.0024	.0008	.0026	.0935	.0271	.0949	.0024	.0007	.0024	.0935	.0271	.0949	.0024	.0007	.0024
.1148	.0421	.1174	.0029	.0011	.0030	.1147	.0361	.1101	.0029	.0009	.0028	.1147	.0361	.1101	.0029	.0009	.0028
.1608	.1063	.2107	.0066	.0027	.0054	.1605	.0341	.1974	.0066	.0024	.0050	.1605	.0341	.1974	.0066	.0024	.0050
.4068	.1591	.2797	.0103	.0040	.0071	.4062	.1425	.2624	.0103	.0036	.0067	.4062	.1425	.2624	.0103	.0036	.0067
.5529	.1994	.3299	.0140	.0051	.0084	.5519	.1795	.3097	.0140	.0046	.0079	.5519	.1795	.3097	.0140	.0046	.0079
.6989	.2283	.3629	.0178	.0058	.0092	.6976	.2062	.3409	.0177	.0052	.0087	.6976	.2062	.3409	.0177	.0052	.0087
.8449	.2460	.3800	.0215	.0062	.0097	.8434	.2296	.3571	.0214	.0057	.0091	.8434	.2296	.3571	.0214	.0057	.0091
.9909	.2531	.3817	.0252	.0064	.0097	.9891	.2270	.3452	.0251	.0058	.0088	.9891	.2270	.3452	.0251	.0058	.0088
1.1370	.2499	.3680	.0289	.0063	.0093	1.1348	.2270	.3452	.0288	.0058	.0088	1.1348	.2270	.3452	.0288	.0058	.0088
1.2830	.2358	.3386	.0326	.0060	.0086	1.2805	.2143	.3171	.0325	.0054	.0081	1.2805	.2143	.3171	.0325	.0054	.0081
1.4290	.2087	.2940	.0363	.0053	.0075	1.4262	.1897	.2747	.0362	.0048	.0070	1.4262	.1897	.2747	.0362	.0048	.0070
1.5750	.1673	.2338	.0400	.0043	.0059	1.5720	.1518	.2179	.0399	.0039	.0055	1.5720	.1518	.2179	.0399	.0039	.0055
1.7210	.1099	.1563	.0437	.0028	.0040	1.7177	.0994	.1452	.0436	.0037	.0057	1.7177	.0994	.1452	.0436	.0037	.0057
1.8255	.0573	.0895	.0464	.0015	.0023	1.8219	.0515	.0831	.0463	.0033	.0051	1.8219	.0515	.0831	.0463	.0033	.0051
1.8468	.0454	.0745	.0469	.0012	.0019	1.8432	.0406	.0692	.0468	.0030	.0051	1.8432	.0406	.0692	.0468	.0030	.0051
1.8681	.0329	.0591	.0474	.0008	.0015	1.8657	.0377	.0602	.0474	.0027	.0051	1.8657	.0377	.0602	.0474	.0027	.0051
1.8894	.0201	.0431	.0480	.0005	.0011	1.8857	.0340	.0549	.0484	.0024	.0051	1.8857	.0340	.0549	.0484	.0024	.0051
1.9107	.0067	.0266	.0485	.0002	.0007	1.9069	.0056	.0250	.0488	.0021	.0051	1.9069	.0056	.0250	.0488	.0021	.0051
1.9257	-.0026	.0147	.0489	-.0001	.0004	1.9219	-.0028	.0140	.0489	-.0001	.0051	1.9219	-.0028	.0140	.0489	-.0001	.0051
1.9281	-.0028	.0127	.0490	-.0001	.0003	1.9243	-.0031	.0122	.0489	-.0001	.0051	1.9243	-.0031	.0122	.0489	-.0001	.0051
1.9305	-.0022	.0108	.0490	-.0001	.0003	1.9267	-.0025	.0104	.0490	-.0001	.0051	1.9267	-.0025	.0104	.0490	-.0001	.0051
1.9329	-.0004	.0086	.0491	-.0000	.0002	1.9291	-.0006	.0084	.0490	-.0000	.0051	1.9291	-.0006	.0084	.0490	-.0000	.0051
1.9345	.0041	.0041	.0491	.0001	.0001	1.9308	.0039	.0039	.0490	.0001	.0051	1.9308	.0039	.0039	.0490	.0001	.0051
RADIUS (INCHES) = 9.042			RADIUS (METERS) = .2397			RADIUS (INCHES) = 9.275			RADIUS (METERS) = .2356			RADIUS (INCHES) = 9.275			RADIUS (METERS) = .2356		
CHORD (INCHES) = 1.933			CHORD (METERS) = .0491			CHORD (INCHES) = 1.930			CHORD (METERS) = .0490			CHORD (INCHES) = 1.930			CHORD (METERS) = .0490		
ZCSL (INCHES) = .8678			ZCSL (METERS) = .0220			ZCSL (INCHES) = .8668			ZCSL (METERS) = .0220			ZCSL (INCHES) = .8668			ZCSL (METERS) = .0220		
YCSL (INCHES) = .2454			YCSL (METERS) = .0062			YCSL (INCHES) = .2274			YCSL (METERS) = .0058			YCSL (INCHES) = .2274			YCSL (METERS) = .0058		
RLE (INCHES) = .0070			RLE (METERS) = .00018			RLE (INCHES) = .0070			RLE (METERS) = .00018			RLE (INCHES) = .0070			RLE (METERS) = .00018		
RTE (INCHES) = .0070			RTE (METERS) = .000178			RTE (INCHES) = .0070			RTE (METERS) = .000178			RTE (INCHES) = .0070			RTE (METERS) = .000178		
X-AREA (SQ. IN.) = .1867			X-AREA (SQ. METERS) = .000120			X-AREA (SQ. IN.) = .1857			X-AREA (SQ. METERS) = .000120			X-AREA (SQ. IN.) = .1857			X-AREA (SQ. METERS) = .000120		
GAMMA-CHORD( DEG.) = 23.18			GAMMA-CHORD(RAD.) = .4047			GAMMA-CHORD( DEG.) = 22.04			GAMMA-CHORD(RAD.) = .3846			GAMMA-CHORD( DEG.) = 22.04			GAMMA-CHORD(RAD.) = .3846		

TABLE XXVII (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES - STATOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-.0011	.0037	.0037	-.0000	.0001	.0001	-.0009	.0035	.0035	-.0000	.0001	.0001
.0013	-.0016	.0109	.0000	-.0000	.0003	.0015	-.0018	.0106	.0000	-.0000	.0003
.0038	-.0029	.0150	.0001	-.0001	.0004	.0039	-.0031	.0146	.0001	-.0001	.0004
.0062	-.0034	.0183	.0002	-.0001	.0005	.0063	-.0036	.0178	.0002	-.0001	.0005
.0086	-.0035	.0212	.0002	-.0001	.0005	.0087	-.0039	.0205	.0002	-.0001	.0005
.0298	.0000	.0418	.0008	.0006	.0011	.0299	-.0010	.0402	.0008	-.0000	.0010
.0510	.0072	.0590	.0013	.0002	.0015	.0511	.0054	.0565	.0013	.0001	.0014
.0722	.0153	.0751	.0018	.0004	.0019	.0722	.0128	.0719	.0018	.0003	.0018
.0935	.0235	.0903	.0024	.0006	.0023	.0934	.0202	.0863	.0024	.0005	.0022
.1147	.0317	.1047	.0029	.0008	.0027	.1146	.0277	.1000	.0029	.0007	.0025
.2602	.0850	.1876	.0066	.0022	.0048	.2599	.0768	.1789	.0066	.0020	.0045
.4057	.1298	.2494	.0103	.0033	.0063	.4052	.1185	.2379	.0103	.0030	.0060
.5512	.1643	.2946	.0140	.0042	.0075	.5505	.1507	.2810	.0140	.0038	.0071
.6967	.1893	.3243	.0177	.0048	.0082	.6957	.1742	.3094	.0177	.0044	.0079
.8421	.2049	.3397	.0214	.0052	.0086	.8410	.1890	.3240	.0214	.0048	.0082
.9876	.2116	.3409	.0251	.0054	.0087	.9863	.1934	.3251	.0251	.0050	.0083
1.1331	.2094	.3280	.0288	.0053	.0083	1.1316	.1937	.3125	.0287	.0049	.0079
1.2786	.1979	.3008	.0325	.0050	.0076	1.2769	.1832	.2863	.0324	.0047	.0073
1.4241	.1752	.2602	.0362	.0045	.0066	1.4221	.1623	.2472	.0361	.0041	.0063
1.5696	.1402	.2059	.0399	.0036	.0052	1.5674	.1297	.1953	.0398	.0033	.0050
1.7151	.0915	.1365	.0436	.0023	.0035	1.7127	.0846	.1296	.0435	.0021	.0033
1.8192	.0472	.0783	.0462	.0012	.0020	1.8166	.0433	.0741	.0461	.0011	.0019
1.8404	.0371	.0653	.0467	.0009	.0017	1.8378	.0340	.0618	.0467	.0009	.0016
1.8616	.0267	.0518	.0473	.0007	.0013	1.8590	.0244	.0492	.0472	.0006	.0012
1.8828	.0159	.0380	.0478	.0004	.0010	1.8802	.0144	.0361	.0478	.0004	.0009
1.9041	.0048	.0238	.0484	.0001	.0006	1.9014	.0041	.0228	.0483	.0001	.0006
1.9190	-.0030	.0135	.0487	-.0001	.0003	1.9163	-.0032	.0131	.0487	-.0001	.0003
1.9214	-.0033	.0118	.0488	-.0001	.0003	1.9187	-.0035	.0115	.0487	-.0001	.0003
1.9238	-.0026	.0102	.0489	-.0001	.0003	1.9211	-.0028	.0099	.0488	-.0001	.0003
1.9262	-.0008	.0082	.0489	-.0000	.0002	1.9235	-.0010	.0080	.0489	-.0000	.0002
1.9279	.0037	.0037	.0490	.0001	.0001	1.9251	.0035	.0035	.0489	.0001	.0001
RADIUS (INCHES) = 9.462						RADIUS (INCHES) = 9.650					
CHORD (INCHES) = 1.927						CHORD (INCHES) = 1.924					
ZCSL (INCHES) = .8659						ZCSL (INCHES) = .8651					
YCSL (INCHES) = .2136						YCSL (INCHES) = .2013					
RLE (INCHES) = .0070						RLE (INCHES) = .0070					
RTE (INCHES) = .0070						RTE (INCHES) = .0070					
X-AREA (SQ. IN.) = .1851						X-AREA (SQ. IN.) = .1847					
GAMMA-CHORD IDEG. = 21.20						GAMMA-CHORD IDEG. = 20.54					
RADIUS (METERS) = .2403						RADIUS (METERS) = .2451					
CHORD (METERS) = .0489						CHORD (METERS) = .0489					
ZCSL (METERS) = .0220						ZCSL (METERS) = .0220					
YCSL (METERS) = .0054						YCSL (METERS) = .0051					
RLE (METERS) = .000178						RLE (METERS) = .000178					
RTE (METERS) = .000178						RTE (METERS) = .000178					
X-AREA (SQ. IN.) = .000119						X-AREA (SQ. IN.) = .000119					
GAMMA-CHORD (RAD.) = .3700						GAMMA-CHORD (RAD.) = .3584					

TABLE XXVII (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES - STATOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-.0008	.0033	.0033	-.0000	.0001	.0001	-.0007	.0031	.0031	-.0000	.0001	.0001
.0016	-.0020	.0101	.0000	-.0001	.0003	.0017	-.0022	.0098	.0000	-.0001	.0003
.0040	-.0034	.0140	.0001	-.0001	.0004	.0041	-.0035	.0136	.0001	-.0001	.0003
.0064	-.0039	.0170	.0002	-.0001	.0004	.0065	-.0042	.0166	.0002	-.0001	.0004
.0088	-.0043	.0196	.0002	-.0001	.0005	.0089	-.0046	.0191	.0002	-.0001	.0005
.0299	-.0024	.0380	.0008	-.0001	.0010	.0300	-.0032	.0369	.0008	-.0001	.0009
.0511	.0030	.0532	.0013	.0001	.0014	.0511	.0016	.0515	.0013	.0000	.0013
.0722	.0093	.0674	.0018	.0002	.0017	.0722	.0074	.0651	.0018	.0002	.0017
.0934	.0158	.0809	.0024	.0004	.0021	.0933	.0133	.0780	.0024	.0003	.0020
.1145	.0223	.0936	.0029	.0006	.0024	.1144	.0193	.0901	.0029	.0005	.0023
.1356	.0288	.1069	.0034	.0007	.0024	.1352	.0254	.1064	.0034	.0006	.0024
.1567	.0353	.1201	.0039	.0008	.0026	.1563	.0313	.1213	.0039	.0007	.0024
.1778	.0418	.1334	.0044	.0009	.0027	.1777	.0372	.1318	.0044	.0008	.0024
.1989	.0483	.1467	.0049	.0010	.0028	.1988	.0431	.1415	.0049	.0009	.0024
.2199	.0548	.1599	.0054	.0011	.0029	.2198	.0489	.1463	.0054	.0010	.0024
.2409	.0613	.1731	.0059	.0012	.0030	.2408	.0547	.1511	.0059	.0011	.0024
.2619	.0678	.1863	.0064	.0013	.0031	.2618	.0605	.1559	.0064	.0012	.0024
.2829	.0743	.1995	.0069	.0014	.0032	.2828	.0663	.1607	.0069	.0013	.0024
.3039	.0808	.2127	.0074	.0015	.0033	.3038	.0721	.1655	.0074	.0014	.0024
.3249	.0873	.2259	.0079	.0016	.0034	.3248	.0779	.1703	.0079	.0015	.0024
.3459	.0938	.2391	.0084	.0017	.0035	.3458	.0837	.1751	.0084	.0016	.0024
.3669	.1003	.2523	.0089	.0018	.0036	.3668	.0895	.1799	.0089	.0017	.0024
.3879	.1068	.2655	.0094	.0019	.0037	.3878	.0953	.1847	.0094	.0018	.0024
.4089	.1133	.2787	.0099	.0020	.0038	.4088	.1011	.1895	.0099	.0019	.0024
.4299	.1198	.2919	.0104	.0021	.0039	.4298	.1069	.1943	.0104	.0020	.0024
.4509	.1263	.3051	.0109	.0022	.0040	.4508	.1127	.1991	.0109	.0021	.0024
.4719	.1328	.3183	.0114	.0023	.0041	.4718	.1185	.2039	.0114	.0022	.0024
.4929	.1393	.3315	.0119	.0024	.0042	.4928	.1243	.2087	.0119	.0023	.0024
.5139	.1458	.3447	.0124	.0025	.0043	.5138	.1301	.2135	.0124	.0024	.0024
.5349	.1523	.3579	.0129	.0026	.0044	.5348	.1359	.2183	.0129	.0025	.0024
.5559	.1588	.3711	.0134	.0027	.0045	.5558	.1417	.2231	.0134	.0026	.0024
.5769	.1653	.3843	.0139	.0028	.0046	.5768	.1475	.2279	.0139	.0027	.0024
.5979	.1718	.3975	.0144	.0029	.0047	.5978	.1533	.2327	.0144	.0028	.0024
.6189	.1783	.4107	.0149	.0030	.0048	.6188	.1591	.2375	.0149	.0029	.0024
.6399	.1848	.4239	.0154	.0031	.0049	.6398	.1649	.2423	.0154	.0030	.0024
.6609	.1913	.4371	.0159	.0032	.0050	.6608	.1707	.2471	.0159	.0031	.0024
.6819	.1978	.4503	.0164	.0033	.0051	.6818	.1765	.2519	.0164	.0032	.0024
.7029	.2043	.4635	.0169	.0034	.0052	.7028	.1823	.2567	.0169	.0033	.0024
.7239	.2108	.4767	.0174	.0035	.0053	.7238	.1881	.2615	.0174	.0034	.0024
.7449	.2173	.4899	.0179	.0036	.0054	.7448	.1939	.2663	.0179	.0035	.0024
.7659	.2238	.5031	.0184	.0037	.0055	.7658	.2007	.2711	.0184	.0036	.0024
.7869	.2303	.5163	.0189	.0038	.0056	.7868	.2065	.2759	.0189	.0037	.0024
.8079	.2368	.5295	.0194	.0039	.0057	.8078	.2123	.2807	.0194	.0038	.0024
.8289	.2433	.5427	.0199	.0040	.0058	.8288	.2181	.2855	.0199	.0039	.0024
.8499	.2498	.5559	.0204	.0041	.0059	.8498	.2239	.2903	.0204	.0040	.0024
.8709	.2563	.5691	.0209	.0042	.0060	.8708	.2297	.2951	.0209	.0041	.0024
.8919	.2628	.5823	.0214	.0043	.0061	.8918	.2355	.3009	.0214	.0042	.0024
.9129	.2693	.5955	.0219	.0044	.0062	.9128	.2413	.3057	.0219	.0043	.0024
.9339	.2758	.6087	.0224	.0045	.0063	.9338	.2471	.3105	.0224	.0044	.0024
.9549	.2823	.6219	.0229	.0046	.0064	.9548	.2529	.3153	.0229	.0045	.0024
.9759	.2888	.6351	.0234	.0047	.0065	.9758	.2587	.3201	.0234	.0046	.0024
.9969	.2953	.6483	.0239	.0048	.0066	.9968	.2645	.3249	.0239	.0047	.0024
.1.0179	.3018	.6615	.0244	.0049	.0067	.1.0178	.2703	.3297	.0244	.0048	.0024
.1.0389	.3083	.6747	.0249	.0050	.0068	.1.0388	.2761	.3345	.0249	.0049	.0024
.1.0599	.3148	.6879	.0254	.0051	.0069	.1.0598	.2819	.3393	.0254	.0050	.0024
.1.0809	.3213	.7011	.0259	.0052	.0070	.1.0808	.2877	.3441	.0259	.0051	.0024
.1.1019	.3278	.7143	.0264	.0053	.0071	.1.1018	.2935	.3489	.0264	.0052	.0024
.1.1229	.3343	.7275	.0269	.0054	.0072	.1.1228	.3003	.3537	.0269	.0053	.0024
.1.1439	.3408	.7407	.0274	.0055	.0073	.1.1438	.3061	.3585	.0274	.0054	.0024
.1.1649	.3473	.7539	.0279	.0056	.0074	.1.1648	.3119	.3633	.0279	.0055	.0024
.1.1859	.3538	.7671	.0284	.0057	.0075	.1.1858	.3177	.3681	.0284	.0056	.0024
.1.2069	.3603	.7803	.0289	.0058	.0076	.1.2068	.3235	.3729	.0289	.0057	.0024
.1.2279	.3668	.7935	.0294	.0059	.0077	.1.2278	.3293	.3777	.0294	.0058	.0024
.1.2489	.3733	.8067	.0299	.0060	.0078	.1.2488	.3351	.3825	.0299	.0059	.0024
.1.2699	.3798	.8199	.0304	.0061	.0079	.1.2698	.3409	.3873	.0304	.0060	.0024
.1.2909	.3863	.8331	.0309	.0062	.0080	.1.2908	.3467	.3921	.0309	.0061	.0024
.1.3119	.3928	.8463	.0314	.0063	.0081	.1.3118	.3525	.3969	.0314	.0062	.0024
.1.3329	.3993	.8595	.0319	.0064	.0082	.1.3328	.3583	.4017	.0319	.0063	.0024
.1.3539	.4058	.8727	.0324	.0065	.0083	.1.3538	.3641	.4065	.0324	.0064	.0024
.1.3749	.4123	.8859	.0329	.0066	.0084	.1.3748	.3699	.4113	.0329	.0065	.0024
.1.3959	.4188	.8991	.0334	.0067	.0085	.1.3958	.3757	.4161	.0334	.0066	.0024
.1.4169	.4253	.9123	.0339	.0068	.0086	.1.4168	.3815	.4209	.0339	.0067	.0024
.1.4379	.4318	.9255	.0344	.0069	.0087	.1.4378	.3873	.4257	.0344	.0068	.0024
.1.4589	.4383	.9387	.0349	.0070	.0088	.1.4588	.3931	.4305	.0349	.0069	.0024
.1.4799	.4448	.9519	.0354	.0071	.0089	.1.4798	.3989	.4353	.0354	.0070	.0024
.1.5009	.4513	.9651	.0359	.0072	.0090	.1.5008	.4047	.4401	.0359	.0071	.0024
.1.5219	.4578	.9783	.0364	.0073	.0091	.1.5218	.4105	.4449	.0364	.0072	.0024
.1.5429	.4643	.9915	.0369	.0074	.0092	.1.5428	.4163	.4497	.0369	.0073	.0024
.1.5639	.4708	.1.0047	.0374	.0075	.0093	.1.5638	.4221	.4545	.0374	.0074	.0024
.1.5849	.4773	.1.0179	.0379	.0076	.0094	.1.5848	.4279	.4593	.0379	.0075	.0024
.1.6059	.4838	.1.0311	.0384	.0077	.0095	.1.6058	.4337	.4641	.0384	.0076	.0024
.1.6269	.4903	.1.0443	.0389	.0078	.0096	.1.6268	.4395	.4689	.0389	.0077	.0024
.1.6479	.4968	.1.0575	.0394	.0079	.0097	.1.6478	.4453	.4737	.0394	.0078	.0024
.1.6689	.5033	.1.0707	.0399	.0080	.0098	.1.6688	.4511	.4785	.0399	.0079	.0024
.1.6899	.5098	.1.0839	.0404	.0081	.0099	.1.6898	.4569	.4833	.0404	.0080	.0024
.1.7109	.5163	.1.0971	.0409	.0082	.0100	.1.7108	.4627	.4881	.0409	.0081	.0024
.1.7319	.5228	.1.1103	.0414	.0083	.0101	.1.7318	.4685	.4929	.0414	.0082	.0024
.1.7529	.5293	.1.1235	.0419	.0084	.0102	.1.7528	.4743	.4977	.0419	.0083	.0024
.1.7739	.5358	.1.1367	.0424	.0085	.0103	.1.7738	.4801	.5025	.0424	.0084	.0024
.1.7949	.5423	.1.1499	.0429	.0086	.0104	.1.7948	.4859	.5073	.0429	.0085	.0024
.1.8159	.5488	.1.1631	.0434	.0087	.0105	.1.8158	.4917	.5121	.0434	.0086	.0024
.1.8369	.5553	.1.1763	.0439	.0088	.0106	.1.8368	.4975	.5169	.0439	.0087	.0024
.1.8579	.5618	.1.1895	.0444	.0089	.0107	.1.8578	.5033	.5217	.0444	.0088	.0024
.1.8789	.5683	.1.2027	.0449	.0090	.0108	.1.8788	.5091	.5265	.0449	.0089	.0024
.1.8999	.5748	.1.2159	.0454	.0091	.0109	.1.8998	.5149	.5313	.0454	.0090	.0024
.1.9209	.5813	.1.2291	.0459	.0092	.0110	.1.9208	.5207	.5361	.0459	.0091	.0024
.1.9419	.5878	.1.2423	.0464	.0093	.0111	.1.9418	.5265	.5409	.0464	.0092	.0024
.1.9629	.5943	.1.2555	.0469	.0094	.0112	.1.9628	.5323	.5457	.0469	.0093	.0024
.1.9839	.6008	.1.2687	.0474	.0095	.0113	.1.9838	.5381	.5505	.0474	.0094	.0024
.2.0049	.6073	.1.2819	.0479	.0096	.0114	.2.0048	.5439	.5553	.0479	.0095	.0024
.2.0259	.6138	.1.2951	.0484	.0097	.0115	.2.0258	.5497	.5601	.0484	.0096	.0024
.2.0469	.6203	.1.3083	.0489	.0098	.0116	.2.0468	.5555	.5649	.0489	.0097	.0024
.2.0679	.6268	.1.3215	.0494	.0099	.0117	.2.0678	.5613	.5697	.0494	.0098	

TABLE XXVII (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES - STATOR 2

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)			
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS	
-.0006	.0029	.0029		-.0000	.0001	.0001		-.0006	.0029	.0029		-.0000	.0001	.0001	
.0017	-.0023	.0096		.0000	-.0001	.0002		.0017	-.0023	.0096		.0000	-.0001	.0002	
.0041	-.0037	.0133		.0001	-.0001	.0003		.0041	-.0037	.0133		.0001	-.0001	.0003	
.0065	-.0044	.0161		.0002	-.0001	.0004		.0065	-.0044	.0162		.0002	-.0001	.0004	
.0089	-.0049	.0186		.0002	-.0001	.0005		.0089	-.0049	.0187		.0002	-.0001	.0005	
.0299	-.0042	.0356		.0008	-.0001	.0009		.0299	-.0043	.0358		.0008	-.0001	.0009	
.0509	-.0000	.0495		.0013	-.0000	.0013		.0509	-.0002	.0498		.0013	-.0000	.0013	
.0720	.0050	.0625		.0018	-.0001	.0016		.0720	.0048	.0628		.0018	-.0001	.0016	
.0930	.0102	.0747		.0024	.0003	.0019		.0930	.0100	.0751		.0024	.0003	.0019	
.1140	.0156	.0863		.0029	.0004	.0022		.1140	.0136	.0867		.0029	.0004	.0022	
.1581	.0518	.1531		.0066	.0013	.0039		.1581	.0513	.1536		.0066	.0013	.0039	
.2022	.0835	.2032		.0102	.0021	.0052		.2022	.0829	.2038		.0102	.0021	.0052	
.2463	.1084	.2399		.0139	.0028	.0061		.2463	.1077	.2405		.0139	.0027	.0061	
.2904	.1271	.2841		.0175	.0032	.0067		.2904	.1267	.2841		.0175	.0027	.0067	
.3345	.1391	.3276		.0212	.0035	.0070		.3345	.1383	.2769		.0212	.0035	.0070	
.3787	.1450	.3767		.0249	.0037	.0070		.3787	.1442	.2772		.0249	.0037	.0070	
.4228	.1446	.4262		.0285	.0037	.0067		.4228	.1439	.2657		.0285	.0037	.0067	
.4669	.1377	.4719		.0322	.0035	.0061		.4669	.1371	.2423		.0322	.0035	.0062	
.5110	.1224	.5077		.0358	.0031	.0053		.5110	.1301	.2081		.0358	.0031	.0053	
.5551	.0979	.5532		.0395	.0025	.0041		.5551	.1246	.1834		.0395	.0025	.0042	
.5992	.0634	.5978		.0432	.0016	.0027		.5992	.1189	.1634		.0432	.0016	.0027	
.6433	.0318	.6417		.0468	.0008	.0016		.6433	.1189	.1634		.0468	.0016	.0027	
.6874	.0246	.6856		.0463	.0006	.0013		.6874	.1189	.1634		.0463	.0016	.0027	
.7315	.0173	.7297		.0468	.0004	.0010		.7315	.1189	.1634		.0468	.0016	.0027	
.7756	.0097	.7738		.0474	.0002	.0008		.7756	.1189	.1634		.0474	.0016	.0027	
.8197	.0018	.8179		.0479	.0000	.0005		.8197	.1189	.1634		.0479	.0016	.0027	
.8638	.0038	.8620		.0483	-.0001	.0003		.8638	.1189	.1634		.0483	-.0001	.0003	
.9079	-.0040	.9061		.0484	-.0001	.0003		.9079	.1189	.1634		.0484	-.0001	.0003	
.9520	-.0034	.9502		.0484	-.0001	.0002		.9520	.1189	.1634		.0484	-.0001	.0002	
.9961	-.0015	.9943		.0485	-.0000	.0002		.9961	.1189	.1634		.0485	-.0000	.0002	
1.0402	.0029	1.0384		.0485	.0001	.0001		1.0402	.1189	.1634		.0485	.0001	.0001	
RADIUS (INCHES) = 10.860				RADIUS (METERS) = 2.758				RADIUS (INCHES) = 11.559				RADIUS (METERS) = 2.936			
CHORD (INCHES) = 1.909				CHORD (METERS) = 0.0495				CHORD (INCHES) = 1.903				CHORD (METERS) = 0.0483			
ZC SL (INCHES) = .8592				ZC SL (METERS) = .0218				ZC SL (INCHES) = .8560				ZC SL (METERS) = .0217			
YC SL (INCHES) = .1631				YC SL (METERS) = .0041				YC SL (INCHES) = .1631				YC SL (METERS) = .0041			
RLE (INCHES) = .0070				RLE (METERS) = .00178				RLE (INCHES) = .0070				RLE (METERS) = .00178			
RTE (INCHES) = .0070				RTE (METERS) = .00178				RTE (INCHES) = .0070				RTE (METERS) = .00178			
X-AREA (SQ. IN.) = .1841				X-AREA (SQ. METERS) = .00119				X-AREA (SQ. IN.) = .1853				X-AREA (SQ. METERS) = .00120			
GAMMA-CHORD (DEG.) = 16.78				GAMMA-CHORD (DEG.) = 29.28				GAMMA-CHORD (DEG.) = 16.48				GAMMA-CHORD (DEG.) = 29.76			

TABLE XXVII (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-.0007	-.0030	.0030	-.0000	-.0001	.0001	.0007	.0030	.0030	-.0000	-.0001	.0001
.0017	-.0023	.0097	.0000	-.0001	.0002	.0017	-.0023	.0097	.0000	-.0001	.0002
.0091	-.0037	.0134	.0001	-.0001	.0003	.0041	-.0036	.0135	.0001	-.0001	.0003
.0065	-.0044	.0163	.0002	-.0001	.0004	.0064	-.0044	.0164	.0002	-.0001	.0004
.0088	-.0049	.0188	.0002	-.0001	.0005	.0088	-.0049	.0189	.0002	-.0001	.0005
.0297	-.0043	.0361	.0008	-.0001	.0009	.0296	-.0044	.0363	.0008	-.0001	.0009
.0506	-.0002	.0502	.0013	-.0000	.0013	.0504	-.0004	.0504	.0013	-.0000	.0013
.0714	.0047	.0633	.0018	.0001	.0016	.0712	.0045	.0636	.0018	.0001	.0016
.0923	.0099	.0756	.0023	.0003	.0019	.0920	.0097	.0760	.0023	.0002	.0019
.1132	.0152	.0873	.0029	.0004	.0022	.1129	.0149	.0877	.0029	.0004	.0022
.1363	.0312	.1546	.0065	.0013	.0039	.1356	.0307	.1551	.0065	.0013	.0039
.3995	.0828	.2050	.0101	.0021	.0052	.3983	.0821	.2056	.0101	.0021	.0052
.5426	.0777	.2420	.0138	.0027	.0061	.5410	.0769	.2426	.0137	.0027	.0062
.6858	.2633	.2662	.0174	.0032	.0068	.6837	.2555	.2668	.0174	.0032	.0068
.8289	.1384	.2785	.0211	.0035	.0071	.8265	.1376	.2790	.0210	.0035	.0071
.9720	.1444	.2787	.0247	.0037	.0071	.9692	.1436	.2793	.0246	.0036	.0071
1.1152	.1442	.2671	.0283	.0037	.0068	1.1119	.1434	.2676	.0282	.0036	.0068
1.2583	.1374	.2436	.0320	.0035	.0062	1.2546	.1367	.2440	.0319	.0035	.0062
1.4015	.1223	.2092	.0356	.0031	.0053	1.3973	.1218	.2095	.0355	.0031	.0053
1.5446	.0978	.1643	.0392	.0025	.0042	1.5401	.0975	.1645	.0391	.0025	.0042
1.6877	.0634	.1085	.0429	.0016	.0028	1.6828	.0632	.1087	.0427	.0016	.0028
1.7901	.0318	.0622	.0455	.0008	.0016	1.7849	.0317	.0622	.0453	.0008	.0016
1.8110	.0247	.0520	.0460	.0006	.0013	1.8057	.0246	.0520	.0459	.0006	.0013
1.8319	.0173	.0415	.0465	.0004	.0011	1.8265	.0172	.0416	.0464	.0004	.0011
1.8528	.0097	.0308	.0471	.0002	.0008	1.8473	.0096	.0308	.0469	.0002	.0008
1.8736	.0018	.0198	.0476	.0000	.0005	1.8681	.0018	.0198	.0474	.0000	.0005
1.8883	-.0038	.0119	.0480	-.0001	.0003	1.8828	-.0038	.0119	.0478	-.0001	.0003
1.8907	-.0040	.0106	.0480	-.0001	.0003	1.8851	-.0040	.0106	.0479	-.0001	.0003
1.8931	-.0033	.0093	.0481	-.0001	.0002	1.8875	-.0033	.0093	.0479	-.0001	.0002
1.8955	-.0015	.0074	.0481	-.0000	.0002	1.8899	-.0015	.0074	.0480	-.0000	.0002
1.8971	.0030	.0030	.0482	.0001	.0001	1.8915	.0030	.0030	.0480	.0001	.0001
RADIUS (INCHES) = 12.257						RADIUS (INCHES) = 12.956					
CHORD (INCHES) = 1.896						CHORD (INCHES) = 1.891					
ZCSL (INCHES) = .8530						ZCSL (INCHES) = .8502					
YCSL (INCHES) = .1638						YCSL (INCHES) = .1637					
RLE (INCHES) = .0070						RLE (INCHES) = .0072					
RTE (INCHES) = .0070						RTE (INCHES) = .0070					
X-AREA (SQ. IN.) = .1865						X-AREA (SQ. IN.) = .1878					
GAMMA-CHORD (DEG.) = 16.43						GAMMA-CHORD (DEG.) = 16.25					
RADIUS (METERS) = .3113						RADIUS (METERS) = .3291					
CHORD (METERS) = .0482						CHORD (METERS) = .0480					
ZCSL (METERS) = .0217						ZCSL (METERS) = .0216					
YCSL (METERS) = .0042						YCSL (METERS) = .0042					
RLE (METERS) = .000178						RLE (METERS) = .000183					
RTE (METERS) = .000178						RTE (METERS) = .000178					
X-AREA (SQ. METERS) = .000120						X-AREA (SQ. METERS) = .000121					
GAMMA-CHORD (RAD.) = .2867						GAMMA-CHORD (RAD.) = .2836					

TABLE XXVII (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES - STATOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-.0007	.0030	.0030	-.0000	.0001	.0001	-.0007	.0030	.0030	-.0000	.0001	.0001
.0017	-.0023	.0097	.0000	-.0001	.0002	.0017	-.0022	.0098	.0000	-.0001	.0002
.0000	.0036	.0135	.0001	.0001	.0003	.0040	.0036	.0136	.0001	-.0001	.0003
.0064	-.0044	.0165	.0002	-.0001	.0004	.0064	.0043	.0166	.0002	-.0001	.0004
.0088	-.0049	.0190	.0002	-.0001	.0005	.0087	.0049	.0192	.0002	-.0001	.0005
.0295	-.0045	.0365	.0008	-.0001	.0009	.0294	.0045	.0368	.0007	-.0001	.0009
.0503	-.0005	.0507	.0013	-.0000	.0013	.0502	-.0006	.0511	.0013	-.0000	.0013
.0710	.0043	.0639	.0018	.0001	.0016	.0709	.0043	.0645	.0018	.0001	.0016
.0918	.0094	.0764	.0023	.0002	.0019	.0916	.0094	.0770	.0023	.0002	.0020
.1126	.0147	.0881	.0029	.0004	.0022	.1123	.0146	.0889	.0029	.0004	.0023
.2549	.0503	.1558	.0065	.0013	.0040	.2543	.0503	.1570	.0065	.0013	.0040
.3972	.0816	.2054	.0101	.0021	.0052	.3963	.0817	.2079	.0101	.0021	.0053
.5396	.1064	.2434	.0137	.0027	.0062	.5384	.1066	.2451	.0137	.0027	.0062
.6819	.1249	.2677	.0173	.0032	.0068	.6804	.1251	.2695	.0173	.0032	.0068
.8243	.1370	.2800	.0209	.0035	.0071	.8224	.1373	.2818	.0209	.0035	.0072
.9666	.1430	.2801	.0246	.0036	.0071	.9644	.1434	.2820	.0245	.0036	.0072
1.1090	.1429	.2684	.0282	.0036	.0068	1.1064	.1434	.2701	.0281	.0036	.0069
1.2513	.1364	.2447	.0318	.0035	.0062	1.2484	.1368	.2463	.0317	.0035	.0063
1.3936	.1215	.2101	.0354	.0031	.0053	1.3905	.1220	.2114	.0353	.0031	.0054
1.5360	.0973	.1650	.0390	.0025	.0042	1.5325	.0977	.1660	.0389	.0025	.0042
1.6783	.0631	.1089	.0426	.0016	.0028	1.6745	.0634	.1096	.0425	.0016	.0028
1.7801	.0317	.0624	.0452	.0008	.0016	1.7761	.0318	.0628	.0451	.0008	.0016
1.8009	.0245	.0522	.0457	.0006	.0013	1.7968	.0247	.0525	.0456	.0006	.0013
1.8217	.0172	.0417	.0463	.0004	.0011	1.8175	.0173	.0419	.0462	.0004	.0011
1.8424	.0096	.0309	.0468	.0002	.0008	1.8382	.0097	.0311	.0467	.0002	.0008
1.8632	.0018	.0198	.0473	.0000	.0005	1.8589	.0018	.0199	.0472	.0000	.0005
1.8778	-.0038	.0119	.0477	-.0001	.0003	1.8735	-.0038	.0119	.0476	-.0001	.0003
1.8801	-.0040	.0106	.0478	-.0001	.0003	1.8759	-.0040	.0106	.0476	-.0001	.0003
1.8825	-.0033	.0093	.0478	-.0001	.0002	1.8782	-.0033	.0093	.0477	-.0001	.0002
1.8849	-.0015	.0074	.0479	-.0000	.0002	1.8806	-.0014	.0074	.0478	-.0000	.0002
1.8865	.0030	.0030	.0479	.0001	.0001	1.8822	.0030	.0030	.0478	.0001	.0001
RADIUS (INCHES) = 13.655			RADIUS (METERS) = .3468			RADIUS (INCHES) = 14.354			RADIUS (METERS) = .3546		
CHORD (INCHES) = 1.886			CHORD (METERS) = .0479			CHORD (INCHES) = 1.881			CHORD (METERS) = .0478		
ZC SL (INCHES) = .8478			ZC SL (METERS) = .0215			ZC SL (INCHES) = .8456			ZC SL (METERS) = .0215		
YC SL (INCHES) = .1639			YC SL (METERS) = .0042			YC SL (INCHES) = .1648			YC SL (METERS) = .0042		
RLE (INCHES) = .0074			RLE (METERS) = .000108			RLE (INCHES) = .0074			RLE (METERS) = .000108		
RTE (INCHES) = .0070			RTE (METERS) = .000178			RTE (INCHES) = .0070			RTE (METERS) = .000178		
X-AREA (SQ. IN.) = .1892			X-AREA (SQ. METERS) = .000122			X-AREA (SQ. IN.) = .1907			X-AREA (SQ. METERS) = .000123		
GAMMA-CHORD (DEG.) = 16.05			GAMMA-CHORD (RAD.) = .2802			GAMMA-CHORD (DEG.) = 15.90			GAMMA-CHORD (RAD.) = .2775		

TABLE XXVII (Cont'd)

AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 2

English Units (Inches)				SI Units (Meters)				English Units (Inches)				SI Units (Meters)			
ZC	YP	YS		ZC	YP	YS		ZC	YP	YS		ZC	YP	YS	
-.0007	.0031	.0031		-.0000	.0001	.0001		-.0008	.0032	.0032		-.0000	.0001	.0001	
.0016	-.0022	.0099		.0000	-.0001	.0003		.0016	-.0020	.0102		.0000	-.0001	.0003	
.0040	.0035	.0138		.0001	-.0001	.0004		.0039	-.0034	.0142		.0001	-.0001	.0004	
.0063	-.0042	.0169		.0002	-.0001	.0004		.0063	-.0041	.0172		.0002	-.0001	.0004	
.0087	-.0048	.0195		.0002	-.0001	.0005		.0086	-.0046	.0199		.0002	-.0001	.0005	
.0294	-.0043	.0374		.0007	-.0001	.0010		.0293	-.0038	.0384		.0007	-.0001	.0010	
.0500	-.0002	.0521		.0013	-.0000	.0013		.0499	.0006	.0536		.0013	.0000	.0014	
.0707	.0048	.0657		.0018	.0001	.0017		.0706	.0060	.0677		.0018	.0002	.0017	
.0914	.0100	.0785		.0023	.0003	.0020		.0912	.0117	.0809		.0023	.0003	.0021	
.1120	.0154	.0906		.0028	.0004	.0023		.1119	.0174	.0935		.0028	.0004	.0024	
.1328	.0200	.1061		.0034	.0006	.0031		.1335	.0232	.1053		.0034	.0004	.0024	
.1535	.0242	.1219		.0040	.0007	.0037		.1531	.0292	.1189		.0040	.0004	.0023	
.1742	.0284	.1378		.0046	.0008	.0043		.1739	.0352	.1253		.0046	.0004	.0023	
.1949	.0326	.1536		.0052	.0009	.0049		.1946	.0412	.1319		.0052	.0004	.0023	
.2156	.0368	.1694		.0058	.0010	.0054		.2153	.0472	.1384		.0058	.0004	.0023	
.2363	.0410	.1852		.0064	.0011	.0060		.2360	.0532	.1449		.0064	.0004	.0023	
.2570	.0452	.2010		.0070	.0012	.0066		.2567	.0592	.1514		.0070	.0004	.0023	
.2777	.0494	.2168		.0076	.0013	.0071		.2774	.0652	.1579		.0076	.0004	.0023	
.2984	.0536	.2326		.0082	.0014	.0077		.2981	.0712	.1644		.0082	.0004	.0023	
.3191	.0578	.2484		.0088	.0015	.0083		.3188	.0772	.1709		.0088	.0004	.0023	
.3398	.0620	.2642		.0094	.0016	.0089		.3395	.0832	.1774		.0094	.0004	.0023	
.3605	.0662	.2800		.0100	.0017	.0095		.3602	.0892	.1839		.0100	.0004	.0023	
.3812	.0704	.2958		.0106	.0018	.0100		.3809	.0952	.1904		.0106	.0004	.0023	
.4019	.0746	.3116		.0112	.0019	.0106		.4016	.1012	.1969		.0112	.0004	.0023	
.4226	.0788	.3274		.0118	.0020	.0111		.4223	.1072	.2034		.0118	.0004	.0023	
.4433	.0830	.3432		.0124	.0021	.0117		.4430	.1132	.2099		.0124	.0004	.0023	
.4640	.0872	.3590		.0130	.0022	.0123		.4637	.1192	.2164		.0130	.0004	.0023	
.4847	.0914	.3748		.0136	.0023	.0129		.4844	.1252	.2229		.0136	.0004	.0023	
.5054	.0956	.3906		.0142	.0024	.0135		.5051	.1312	.2294		.0142	.0004	.0023	
.5261	.1000	.4064		.0148	.0025	.0141		.5258	.1372	.2359		.0148	.0004	.0023	
.5468	.1042	.4222		.0154	.0026	.0147		.5465	.1432	.2424		.0154	.0004	.0023	
.5675	.1084	.4380		.0160	.0027	.0153		.5672	.1492	.2489		.0160	.0004	.0023	
.5882	.1126	.4538		.0166	.0028	.0159		.5879	.1552	.2554		.0166	.0004	.0023	
.6089	.1168	.4696		.0172	.0029	.0165		.6086	.1612	.2619		.0172	.0004	.0023	
.6296	.1210	.4854		.0178	.0030	.0171		.6293	.1672	.2684		.0178	.0004	.0023	
.6503	.1252	.5012		.0184	.0031	.0177		.6500	.1732	.2749		.0184	.0004	.0023	
.6710	.1294	.5170		.0190	.0032	.0183		.6707	.1792	.2814		.0190	.0004	.0023	
.6917	.1336	.5328		.0196	.0033	.0189		.6914	.1852	.2879		.0196	.0004	.0023	
.7124	.1378	.5486		.0202	.0034	.0195		.7121	.1912	.2944		.0202	.0004	.0023	
.7331	.1420	.5644		.0208	.0035	.0201		.7328	.1972	.3009		.0208	.0004	.0023	
.7538	.1462	.5802		.0214	.0036	.0207		.7535	.2032	.3074		.0214	.0004	.0023	
.7745	.1504	.5960		.0220	.0037	.0213		.7742	.2092	.3139		.0220	.0004	.0023	
.7952	.1546	.6118		.0226	.0038	.0219		.7949	.2152	.3204		.0226	.0004	.0023	
.8159	.1588	.6276		.0232	.0039	.0225		.8156	.2212	.3269		.0232	.0004	.0023	
.8366	.1630	.6434		.0238	.0040	.0231		.8363	.2272	.3334		.0238	.0004	.0023	
.8573	.1672	.6592		.0244	.0041	.0237		.8570	.2332	.3399		.0244	.0004	.0023	
.8780	.1714	.6750		.0250	.0042	.0243		.8777	.2392	.3464		.0250	.0004	.0023	
.8987	.1756	.6908		.0256	.0043	.0249		.8984	.2452	.3529		.0256	.0004	.0023	
.9194	.1798	.7066		.0262	.0044	.0255		.9191	.2512	.3594		.0262	.0004	.0023	
.9401	.1840	.7224		.0268	.0045	.0261		.9398	.2572	.3659		.0268	.0004	.0023	
.9608	.1882	.7382		.0274	.0046	.0267		.9605	.2632	.3724		.0274	.0004	.0023	
.9815	.1924	.7540		.0280	.0047	.0273		.9812	.2692	.3789		.0280	.0004	.0023	
.1.0022	.1966	.7698		.0286	.0048	.0279		.1.0019	.2752	.3854		.0286	.0004	.0023	
.1.0229	.2008	.7856		.0292	.0049	.0285		.1.0226	.2812	.3919		.0292	.0004	.0023	
.1.0436	.2050	.8014		.0298	.0050	.0291		.1.0433	.2872	.3984		.0298	.0004	.0023	
.1.0643	.2092	.8172		.0304	.0051	.0297		.1.0640	.2932	.4049		.0304	.0004	.0023	
.1.0850	.2134	.8330		.0310	.0052	.0303		.1.0847	.2992	.4114		.0310	.0004	.0023	
.1.1057	.2176	.8488		.0316	.0053	.0309		.1.1054	.3052	.4179		.0316	.0004	.0023	
.1.1264	.2218	.8646		.0322	.0054	.0315		.1.1261	.3112	.4244		.0322	.0004	.0023	
.1.1471	.2260	.8804		.0328	.0055	.0321		.1.1468	.3172	.4309		.0328	.0004	.0023	
.1.1678	.2302	.8962		.0334	.0056	.0327		.1.1675	.3232	.4374		.0334	.0004	.0023	
.1.1885	.2344	.9120		.0340	.0057	.0333		.1.1882	.3292	.4439		.0340	.0004	.0023	
.1.2092	.2386	.9278		.0346	.0058	.0339		.1.2089	.3352	.4504		.0346	.0004	.0023	
.1.2299	.2428	.9436		.0352	.0059	.0345		.1.2296	.3412	.4569		.0352	.0004	.0023	
.1.2506	.2470	.9594		.0358	.0060	.0351		.1.2503	.3472	.4634		.0358	.0004	.0023	
.1.2713	.2512	.9752		.0364	.0061	.0357		.1.2710	.3532	.4699		.0364	.0004	.0023	
.1.2920	.2554	.9910		.0370	.0062	.0363		.1.2917	.3592	.4764		.0370	.0004	.0023	
.1.3127	.2596	.1.0068		.0376	.0063	.0369		.1.3124	.3652	.4829		.0376	.0004	.0023	
.1.3334	.2638	.1.0226		.0382	.0064	.0375		.1.3331	.3712	.4894		.0382	.0004	.0023	
.1.3541	.2680	.1.0384		.0388	.0065	.0381		.1.3538	.3772	.4959		.0388	.0004	.0023	
.1.3748	.2722	.1.0542		.0394	.0066	.0387		.1.3745	.3832	.5024		.0394	.0004	.0023	
.1.3955	.2764	.1.0700		.0400	.0067	.0393		.1.3952	.3892	.5089		.0400	.0004	.0023	
.1.4162	.2806	.1.0858		.0406	.0068	.0399		.1.4159	.3952	.5154		.0406	.0004	.0023	
.1.4369	.2848	.1.1016		.0412	.0069	.0405		.1.4366	.4012	.5219		.0412	.0004	.0023	
.1.4576	.2890	.1.1174		.0418	.0070	.0411		.1.4573	.4072	.5284		.0418	.0004	.0023	
.1.4783	.2932	.1.1332		.0424	.0071	.0417		.1.4780	.4132	.5349		.0424	.0004	.0023	
.1.4990	.2974	.1.1490		.0430	.0072	.0423		.1.4987	.4192	.5414		.0430	.0004	.0023	
.1.5197	.3016	.1.1648		.0436	.0073	.0429		.1.5194	.4252	.5479		.0436	.0004	.0023	
.1.5404	.3058	.1.1806		.0442	.0074	.0435		.1.5401	.4312	.5544		.0442	.0004	.0023	
.1.5611	.3100	.1.1964		.0448	.0075	.0441		.1.5608	.4372	.5609		.0448	.0004	.0023	
.1.5818	.3142	.1.2122		.0454	.0076	.0447		.1.5815	.4432	.5674		.0454	.0004	.0023	
.1.6025	.3184	.1.2280		.0460	.0077	.0453		.1.6022	.4492	.5739		.0460	.0004	.0023	
.1.6232	.3226	.1.2438		.0466	.0078	.0459		.1.6229	.4552	.5804		.0466	.0004	.0023	
.1.6439	.3268	.1.2596		.0472	.0079	.0465		.1.6436	.4612	.5869		.0472	.0004	.0023	
.1.6646	.3310	.1.2754		.0478	.0080	.0471		.1.6643	.4672	.5934		.0478	.0004	.0023	
.1.6853	.3352	.1.2912		.0484	.0081	.0477		.1.6850	.4732	.6000		.0484	.0004	.0023	
.1.7060	.3394	.1.3070		.0490	.0082	.0483		.1.7057	.4792	.6065		.0490	.0004	.0023	
.1.7267	.3436	.1.3228		.0496	.0083	.0489		.1.7264	.4852	.6130		.0496	.0004	.0023	
.1.7474	.3478	.1.3386		.0502	.0084	.0495		.1.7471	.4912	.6195		.0502	.0004	.0023	
.1.7681	.3520	.1.3544		.0508	.0085	.0501		.1.7678	.4972	.6260		.0508	.0004	.0023	
.1.7888	.3562	.1.3702		.0514	.0086										

TABLE XXVII (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES — STATOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-.0009	.0034	.0034	-.0000	.0001	.0001	-.0010	.0036	.0036	-.0000	.0001	.0001
.0014	.0018	.0107	.0000	.0000	.0003	.0014	.0016	.0110	.0000	.0000	.0003
.0038	.0032	.0148	.0001	.0001	.0004	.0037	.0030	.0152	.0001	.0001	.0004
.0061	.0037	.0181	.0002	.0001	.0005	.0060	.0035	.0186	.0002	.0001	.0005
.0085	.0041	.0209	.0002	.0001	.0005	.0084	.0039	.0215	.0002	.0001	.0005
.0291	.0026	.0406	.0007	.0001	.0010	.0290	.0019	.0419	.0007	.0000	.0011
.0497	.0027	.0569	.0013	.0001	.0014	.0496	.0038	.0589	.0013	.0001	.0015
.0703	.0089	.0720	.0018	.0002	.0018	.0702	.0106	.0746	.0018	.0003	.0019
.0910	.0134	.0862	.0023	.0004	.0022	.0908	.0175	.0894	.0023	.0004	.0023
.1116	.0219	.0997	.0028	.0006	.0025	.1115	.0245	.1033	.0028	.0006	.0026
.2330	.0657	.1767	.0064	.0017	.0045	.2328	.0712	.1833	.0064	.0018	.0047
.3945	.1035	.2339	.0100	.0026	.0059	.3942	.1111	.2826	.0100	.0028	.0062
.5359	.1330	.2756	.0136	.0034	.0070	.5355	.1422	.2858	.0136	.0036	.0073
.6773	.1547	.3030	.0172	.0039	.0077	.6769	.1651	.3141	.0172	.0042	.0080
.8188	.1687	.3168	.0208	.0043	.0080	.8182	.1797	.3284	.0208	.0046	.0083
.9602	.1754	.3173	.0244	.0045	.0081	.9596	.1866	.3290	.0244	.0047	.0084
1.1017	.1747	.3045	.0280	.0044	.0077	1.1009	.1856	.3160	.0280	.0047	.0080
1.2431	.1662	.2784	.0316	.0042	.0071	1.2422	.1763	.2891	.0316	.0045	.0073
1.3845	.1478	.2398	.0352	.0038	.0061	1.3836	.1568	.2494	.0351	.0040	.0063
1.5260	.1185	.1890	.0388	.0030	.0048	1.5249	.1258	.1969	.0387	.0032	.0050
1.6674	.0773	.1253	.0424	.0020	.0032	1.6663	.0821	.1306	.0423	.0021	.0033
1.7686	.0394	.0716	.0449	.0010	.0018	1.7674	.0421	.0747	.0449	.0011	.0019
1.7892	.0308	.0598	.0454	.0008	.0015	1.7880	.0330	.0623	.0454	.0008	.0016
1.8098	.0219	.0476	.0460	.0006	.0012	1.8086	.0236	.0495	.0459	.0006	.0013
1.8304	.0128	.0350	.0465	.0003	.0009	1.8292	.0139	.0364	.0465	.0004	.0009
1.8511	.0033	.0221	.0470	.0001	.0006	1.8498	.0038	.0229	.0470	.0001	.0006
1.8656	-.0034	.0128	.0474	-.0001	.0003	1.8644	-.0032	.0131	.0474	-.0001	.0003
1.8679	-.0035	.0113	.0474	-.0001	.0003	1.8667	-.0034	.0115	.0474	-.0001	.0003
1.8703	-.0028	.0098	.0475	-.0001	.0002	1.8690	-.0027	.0100	.0475	-.0001	.0003
1.8726	-.0010	.0079	.0476	-.0000	.0002	1.8714	-.0009	.0080	.0475	-.0000	.0002
1.8742	.0034	.0034	.0476	.0001	.0001	1.8730	.0036	.0036	.0476	.0001	.0001
RADIUS (INCHES) = 15.891						RADIUS (INCHES) = 16.170					
CHORD (INCHES) = 1.873						CHORD (INCHES) = 1.872					
ZCSSL (INCHES) = .8406						ZCSSL (INCHES) = .8397					
YCSL (INCHES) = .1910						YCSL (INCHES) = .2000					
RLE (INCHES) = .0080						RLE (INCHES) = .0080					
RTE (INCHES) = .0070						RTE (INCHES) = .0070					
X-AREA (SQ. IN.) = .1956						X-AREA (SQ. IN.) = .1968					
GAMMA-CHORD (DEG.) = 17.37						GAMMA-CHORD (DEG.) = 17.94					
RADIUS (METERS) = .4036						RADIUS (METERS) = .4107					
CHORD (METERS) = .0476						CHORD (METERS) = .0475					
ZCSSL (METERS) = .0214						ZCSSL (METERS) = .0213					
YCSL (METERS) = .0049						YCSL (METERS) = .0051					
RLE (METERS) = .000203						RLE (METERS) = .000204					
RTE (METERS) = .000178						RTE (METERS) = .000178					
X-AREA (SQ. M.) = .000126						X-AREA (SQ. M.) = .000127					
GAMMA-CHORD (RAD.) = .3032						GAMMA-CHORD (RAD.) = .3131					

TABLE XXVII (Cont'd)

## AIRFOIL COORDINATES ON MANUFACTURING SURFACES -- STATOR 2

English Units (Inches)			SI Units (Meters)			English Units (Inches)			SI Units (Meters)		
ZC	YP	YS	ZC	YP	YS	ZC	YP	YS	ZC	YP	YS
-.0011	.0037	.0037	-.0000	.0001	.0001	-.0012	.0039	.0039	-.0000	.0001	.0001
.0013	-.0015	.0113	.0000	-.0000	.0003	.0011	-.0013	.0119	.0000	-.0000	.0003
.0036	-.0029	.0157	.0001	-.0001	.0004	.0035	-.0027	.0184	.0001	-.0001	.0004
.0059	-.0034	.0191	.0002	-.0001	.0005	.0058	-.0031	.0200	.0001	-.0001	.0005
.0083	-.0036	.0222	.0002	-.0001	.0006	.0081	-.0032	.0232	.0002	-.0001	.0006
.0289	-.0012	.0434	.0007	-.0000	.0011	.0287	-.0000	.0457	.0007	-.0000	.0012
.0495	.0051	.0610	.0013	.0001	.0015	.0493	.0071	.0645	.0013	.0002	.0016
.0701	.0124	.0774	.0018	.0003	.0020	.0699	.0152	.0819	.0018	.0004	.0021
.0907	.0198	.0928	.0023	.0005	.0024	.0905	.0236	.0983	.0023	.0008	.0025
.1113	.0274	.1073	.0028	.0007	.0027	.1110	.0320	.1137	.0028	.0008	.0029
.2526	.0771	.1904	.0064	.0020	.0048	.2522	.0866	.2018	.0064	.0022	.0051
.3938	.1194	.2520	.0100	.0030	.0064	.3933	.1326	.2669	.0100	.0034	.0068
.5351	.1523	.2967	.0136	.0039	.0075	.5344	.1631	.3139	.0136	.0043	.0080
.6764	.1763	.3260	.0172	.0045	.0083	.6756	.1939	.3448	.0172	.0049	.0088
.8176	.1915	.3409	.0208	.0049	.0087	.8157	.2101	.3605	.0207	.0053	.0092
.9589	.1986	.3416	.0244	.0050	.0087	.9578	.2174	.3614	.0243	.0055	.0092
1.1001	.1973	.3283	.0279	.0050	.0083	1.0989	.2158	.3476	.0279	.0055	.0088
1.2414	.1873	.3007	.0315	.0048	.0076	1.2401	.2046	.3189	.0315	.0052	.0081
1.3827	.1666	.2597	.0351	.0042	.0066	1.3812	.1819	.2759	.0351	.0046	.0070
1.5239	.1336	.2053	.0387	.0034	.0052	1.5223	.1451	.2187	.0387	.0037	.0056
1.6652	.0875	.1364	.0423	.0022	.0035	1.6635	.0959	.1457	.0423	.0024	.0037
1.7662	.0450	.0779	.0449	.0011	.0020	1.7644	.0496	.0833	.0448	.0013	.0021
1.7868	.0354	.0650	.0454	.0009	.0017	1.7850	.0391	.0694	.0453	.0010	.0018
1.8074	.0254	.0516	.0459	.0006	.0013	1.8056	.0282	.0551	.0459	.0007	.0014
1.8280	.0151	.0378	.0464	.0004	.0010	1.8261	.0169	.0403	.0464	.0004	.0010
1.8486	.0044	.0237	.0470	.0001	.0006	1.8467	.0053	.0250	.0469	.0001	.0006
1.8631	-.0030	.0134	.0473	-.0001	.0003	1.8612	-.0028	.0140	.0473	-.0001	.0004
1.8655	-.0032	.0117	.0474	-.0001	.0003	1.8636	-.0030	.0122	.0474	-.0001	.0003
1.8678	-.0026	.0101	.0474	-.0001	.0003	1.8659	-.0023	.0104	.0474	-.0001	.0003
1.8702	-.0007	.0081	.0475	-.0000	.0002	1.8682	-.0005	.0083	.0475	-.0000	.0002
1.8718	.0037	.0037	.0475	.0001	.0001	1.8698	.0039	.0039	.0475	.0001	.0001
RADIUS (INCHES) = 16.450						RADIUS (INCHES) = 16.869					
CHORD (INCHES) = 1.871						CHORD (INCHES) = 1.869					
ZC SL (INCHES) = .8384						ZC SL (INCHES) = .8370					
YCSL (INCHES) = .2095						YCSL (INCHES) = .2246					
RLE (INCHES) = .0081						RLE (INCHES) = .0083					
RTE (INCHES) = .0070						RTE (INCHES) = .0070					
X-AREA (SQ. IN.) = .1980						X-AREA (SQ. IN.) = .2000					
GAMMA-CHORD (RAD.) = 18.14						GAMMA-CHORD (RAD.) = 18.13					
RADIUS (METERS) = .4178						RADIUS (METERS) = .4285					
CHORD (METERS) = .0475						CHORD (METERS) = .0475					
ZC SL (METERS) = .0213						ZC SL (METERS) = .0213					
YCSL (METERS) = .0053						YCSL (METERS) = .0057					
RLE (METERS) = .000206						RLE (METERS) = .000213					
RTE (METERS) = .000178						RTE (METERS) = .000178					
X-AREA (SQ. M.) = .000128						X-AREA (SQ. M.) = .000125					
GAMMA-CHORD (RAD.) = .3167						GAMMA-CHORD (RAD.) = .3164					

## APPENDIX E

## TWO-RING ACOUSTIC INLET AERODYNAMIC AND ACOUSTIC DESIGN

An acoustic inlet design was studied in addition to the translating center-body finally chosen. A schematic of this additional design, a two-ring configuration, is shown in Figure 71. Mach number distributions are included on the O.D. wall and splitter surfaces. Although the inlet flow is not choked, the blockage of the rings was estimated to be about 3 percent of the area. Boundary layer shape factors on all surfaces were well below the separation criterion of 2.2 to 2.5.

For acoustic purposes, the rings, the extended centerbody, and the inner and outer walls were all treated with various combinations of honeycomb and facing sheet. These acoustic treatment parameters are listed in Table XXVIII. An effective-treatment-length to passage-height of about six was achieved for the two outer passages and about four for the inner passage. Treatment was tuned to the predicted inlet fan noise spectrum to maximize the PNL reduction at approach. The inlet attenuation target and predicted treatment attenuation are shown in Figure 72. The attenuation target represents a PNL reduction of 15 PNdB at the peak inlet noise angle.

TABLE XXVIII

## TWO-RING ACOUSTIC INLET TREATMENT PARAMETERS

	TREATMENT LENGTH METERS (INCHES)	BACKING DEPTH METERS (INCHES)	FACING SHEET % OPEN AREA	HONEYCOMB CELL SIZE METERS (INCHES)
Outer Wall	0.61 (24)	0.013 (0.5)	12	0.0095 (3/8)
Outer Ring	0.43 (17)	0.006/0.006 (0.25/0.25)	12/9	0.0095 (3/8)
Inner Ring	0.38 (15)	0.006/0.006 (0.25/0.25)	9/6	0.0095 (3/8)
Centerbody	0.30 (12)	0.013 (0.5)	6	0.0095 (3/8)

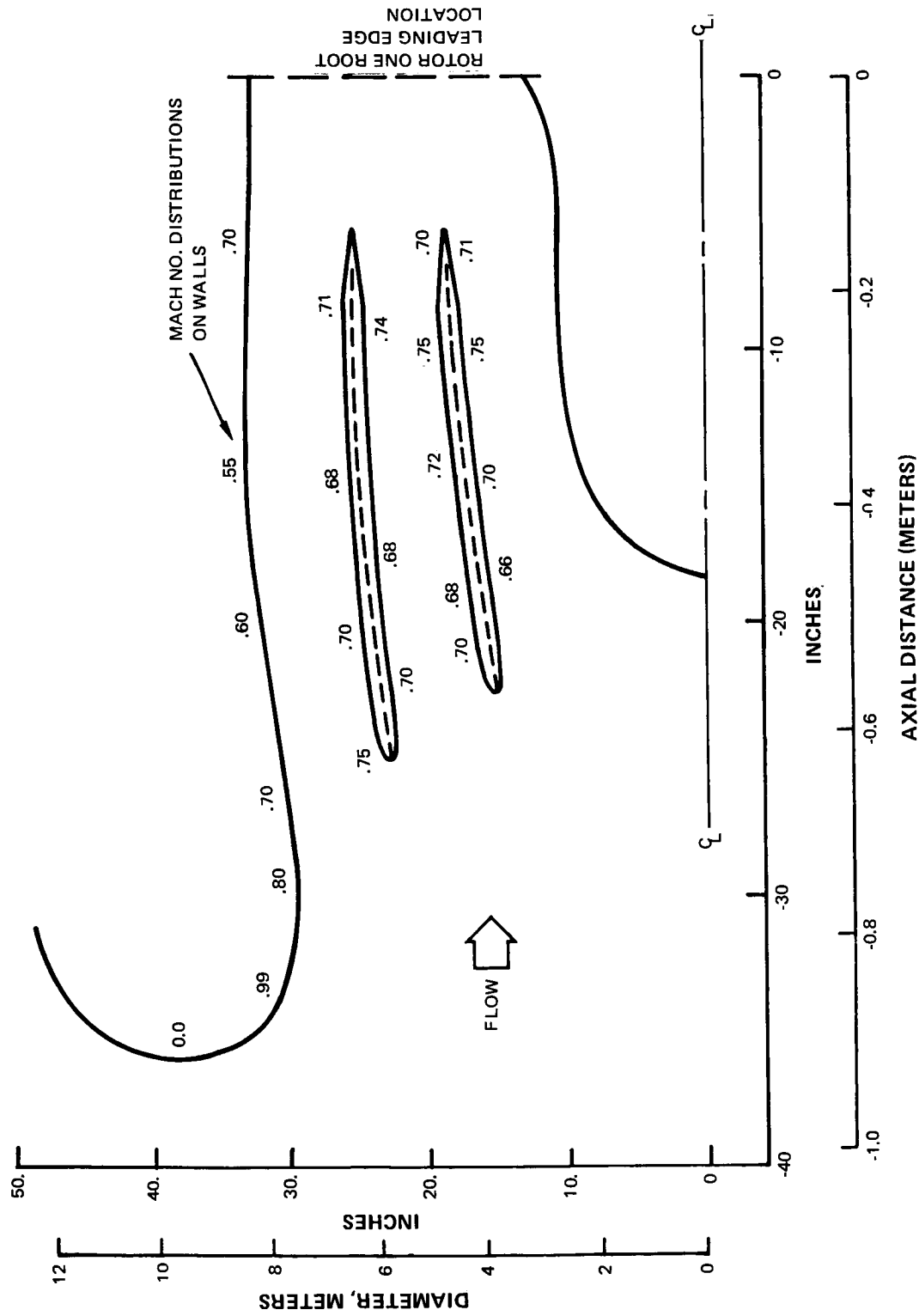


Figure 71 Two-Ring Acoustic Inlet Design Schematic

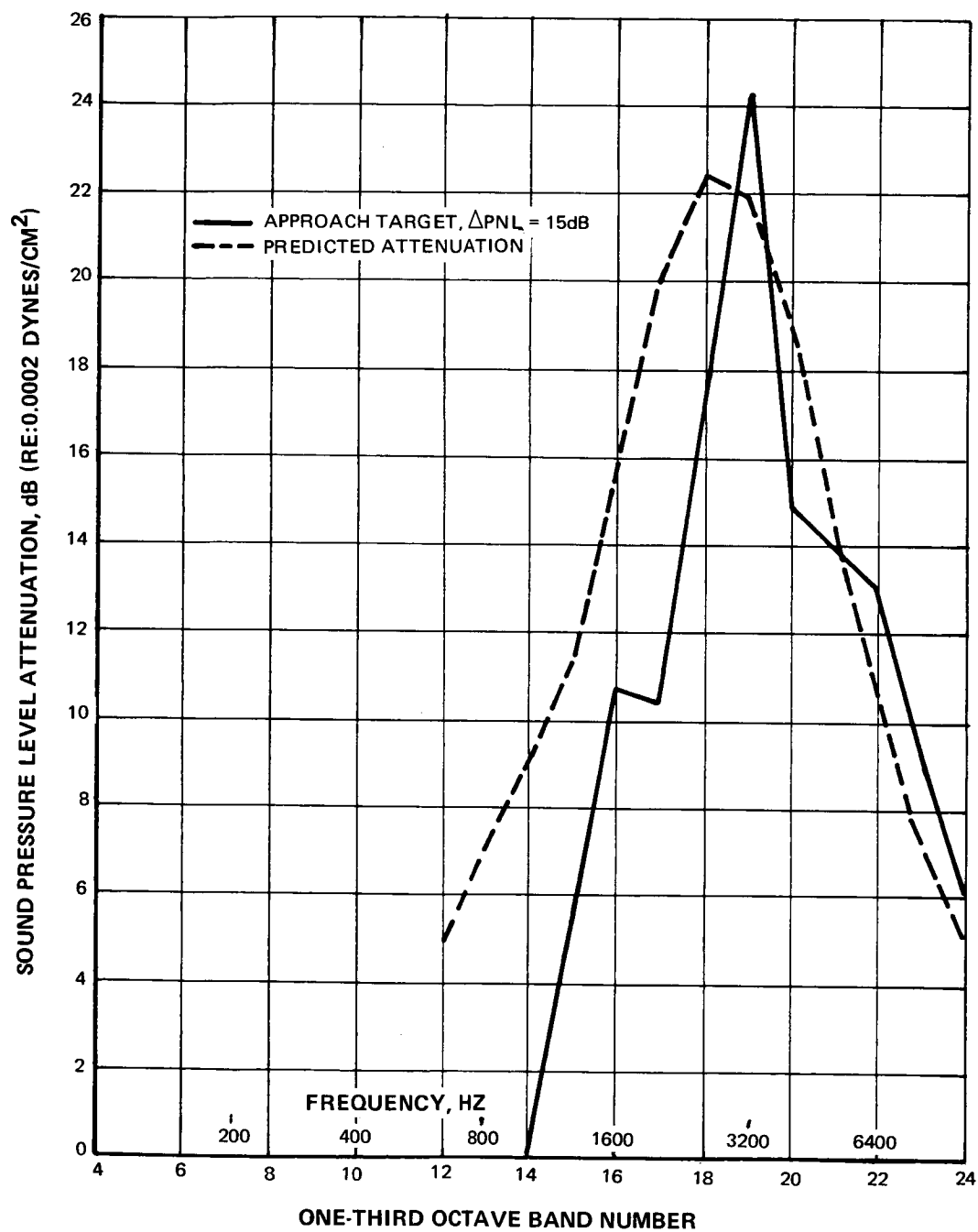


Figure 72 Two-Ring Acoustic Inlet Predicted Attenuation

## REFERENCES

1. Brines, G. L.: "Studies for Determining the Optimum Propulsion System Characteristics for Use in a Long Range Transport Aircraft," NASA CR-120950, PWA-4449, July 1972
2. Keenan, M. J. and Burdsall, E. A.: "High-Loading Low-Speed Fan Study – V Final Report," NASA CR-121148, PWA-4517, April 1973
3. Ruggeri, R. S. and Benser, W. A.: "Performance of a Highly Loaded Two-Stage Axial Flow Fan," NASA Technical Note (to be published)
4. Messenger, H. E. and Kennedy, E. E.: "Two-Stage Fan – I Aerodynamic and Mechanical Design," NASA CR-120859, PWA-4148, January 1972
5. Harley, K. G.; Odegard, P.A.; and Burdsall, E. A.: "High-Loading Low-Speed Fan Study – IV Data and Performance with Redesign Stator and Including a Rotor Tip Casing Treatment," NASA CR-120866, PWA-4326, July 1972
6. Monsarrat, N. T., Keenan, M. J.; and Tramm, P. C.: "High-Loading Low-Speed Fan Study – I Design," NASA CR-72536, PWA-3535, July 1969
7. Keenan, M. H. and Bartok, J. A.: "Experimental Evaluation of Transonic Stators – Final Report," NASA CR-72298, PWA-3470, 1969
8. Tyler, J. M. and Sofrin, T.G.: "Axial Flow Compressor Noise Studies," SAE Trans. Vol. 70, pp. 309 - 322, 1962
9. Rice, E. J.: "Performance of Suppressors for a Full Scale Fan for Turbofan Engines," NASA TMX-52941, 1971



## DISTRIBUTION LIST

1. NASA-Lewis Research Center  
21000 Brookpark Road  
Cleveland, Ohio 44135

Attention:

Report Control Office	MS 5-5	1
Technical Utilization Office	MS 3-19	1
Library	MS 60-3	2
Fluid System Components Div.	MS 5-3	1
Compressor Branch	MS 5-9	5
Director of Aeronautics	MS 3-5	1
R. S. Ruggeri	MS 5-9	1
M. J. Hartmann	MS 5-9	1
W. A. Benser	MS 5-9	1
D. M. Sandercock	MS 5-9	1
L. J. Herrig	MS 501-4	1
T. F. Gelder	MS 5-9	1
C. L. Ball	MS 5-9	1
L. Reid	MS 5-9	1
L. W. Schopen	MS 500-206	1
C. L. Meyer	MS 60-4	1
W. L. Beede	MS 5-3	1
D. W. Drier	MS 21-4	1
E. E. Bailey	MS 5-9	1
N. T. Musial	MS 500-311	1

2. NASA Scientific and Technical Information Facility  
P. O. Box 33  
College Park, Maryland 20740

Attention: Acquisitions Branch 10

3. NASA Headquarters  
Washington, D. C. 20546  
Attention: N. F. Rekos (RLC)

1

### DISTRIBUTION LIST (Cont'd)

- |    |  |             |
|----|--|-------------|
| 4. | U. S. Army Aviation Material Laboratory<br>Fort Eustis, Virginia 23604<br>Attention: John White  | 1           |
| 5. | Headquarters<br>Wright-Patterson AFB, Ohio 45433<br>Attention: A. J. Wennerstrom ARL/LF<br>S. Kobelak, AFAPL/TBP<br>R. P. Carmichael, ASD/XRHP | 1<br>1<br>1 |
| 6. | Department of the Navy<br>Naval Air Systems Command<br>Propulsion Division, AIR 536<br>Washington, D. C. 20360                                 | 1           |
| 7. | Department of Navy<br>Bureau of Ships<br>Washington, D. C. 20360<br>Attention: G. L. Graves  | 1           |
| 8. | NASA-Langley Research Center<br>Technical Library<br>Hampton, Virginia 23365<br>Attention: Mark R. Nichols<br>John V. Becker                   | 1<br>1      |
| 9. | The Boeing Company<br>Commercial Airplane Group<br>P. O. Box 3707<br>Seattle, Washington 98124<br>Attention: G. J. Schott, G-8410, MS 73-24    | 1           |

# DISTRIBUTION LIST (Cont'd)

10. Douglas Aircraft Company  
3855 Lakewood Boulevard  
Long Beach, California 90801  
Attention: J. E. Merriman 1  
Technical Information Ctr. CI-250
  
11. Pratt & Whitney Aircraft  
Florida Research & Development Center  
P. O. Box 2691  
West Palm Beach, Florida 33402  
Attention: J. Brent 1  
H. D. Stetson 1  
W. R. Alley 1  
R. E. Davis 1  
R. W. Rockenbach 1  
B. A. Jones 1  
J. A. Fligg 1
  
12. Pratt & Whitney Aircraft  
400 Main Street  
East Hartford, Connecticut 06108  
Attention: R. E. Palatine 1  
T. G. Slaiby 1  
H. V. Marman 1  
M. J. Keenan 1  
B. B. Smyth 1  
A. A. Mikolajczak 1  
Library (UARL) 1  
W. M. Foley (UARL) 1
  
13. Allison Division, GMC  
Department 8894, Plant 8  
P. O. Box 894  
Indianapolis, Indiana 46206  
Attention: J. N. Barney U-26 1  
G. E. Holbrook T-22 1  
J. A. Korn T-26 1  
R. F. Alverson U-28 1  
Library S-5 1  
A. Medlock U-28 1  
P. Tramm U-23 1

# DISTRIBUTION LIST (Cont'd)

14. Northern Research and Engineering  
219 Vassar Street  
Cambridge, Massachusetts 02139  
Attention: K. Ginwala 1
  
15. General Electric Company  
Flight Propulsion Division  
Cincinnati, Ohio 45215  
Attention: D. Prince H-79 1  
J. F. Klapproth H-42 1  
J. W. McBride H-44 1  
L. H. Smith H-50 1  
J. B. Taylor J-168 1  
Technical Information CTR. N-32 1  
Marlen Miller H-50 1  
C. C. Koch H-79 1  
1  
1  
1  
1
  
16. General Electric Company  
1000 Western Avenue  
Lynn, Massachusetts 01910  
Attention: D. P. Edkins - Bldg. 2-40 1  
F. F. Ehrich - Bldg. 2-40 1  
L. H. King - Bldg. 2-40 1  
R. E. Neitzel- Bldg. 2-40 1  
Dr. C. W. Smith - Library  
Bldg. 2-40M 1
  
17. Curtiss-Wright Corporation  
Wright Aeronautical  
Wood-Ridge, New Jersey 07075  
Attention: S. Lombardo 1  
G. Provenzale 1

### DISTRIBUTION LIST (Cont'd)

18. AiResearch Manufacturing Company  
402 South 36th Street  
Phoenix, Arizona 85034  
Attention: Robert O. Bullock 1  
W. F. Waterman 1  
Jack Erwin 1  
Don Seyler 1  
Jack Switzer 1  
G. L. Perrone 1
19. AiResearch Manufacturing Company  
2525 West 190th Street  
Torrance, California 90509  
Attention: R. Kobayashi 1  
Bob Carmody 1  
Library 1  
R. Jackson 1
20. Union Carbide Corporation  
Nuclear Division  
Oak Ridge Gaseous Diffusion Plant  
P. O. Box "P"  
Oak Ridge, Tennessee 37830  
Attention: R. G. Jordan 1  
D. W. Burton, K-1001, K-25 1
21. Avco Corporation  
Lycoming Division  
550 South Main Street  
Stratford, Connecticut 06497  
Attention: Clause W. Bolton 1
22. Teledyne CAE  
1330 Laskey Road  
Toledo, Ohio 43601  
Attention: Eli H. Benstein 1  
Howard C. Walch 1

### DISTRIBUTION LIST (Cont'd)

23. Solar  
San Diego, California 92112  
Attention: P. A. Pitt 1  
J. Watkins 1
24. Goodyear Atomic Corporation  
Box 628  
Piketon, Ohio 45661  
Attention: C. O. Langebrake 2
25. Iowa State University of Science & Tech.  
Ames, Iowa 50010  
Attention: Professor George K. Serovy  
Dept. of Mechanical Engineering 1
26. Hamilton Standard Division of United  
Aircraft Corporation  
Windsor Locks, Connecticut 06096  
Attention: Mr. Carl Rohrbach  
Head of Aerodynamics and  
Hydrodynamics 1
27. Westinghouse Electric Corporation  
Small Steam and Gas Turbine Engineering B-4  
Lester Branch  
P. O. Box 9175  
Philadelphia, Pennsylvania 19113  
Attention: Mr. S. M. DeCorso 1
28. Williams Research Corporation  
P. O. Box 95  
Walled Lake, Michigan 48088  
Attention: J. Richard Joy  
Supervisor, Analytical Section 1

### DISTRIBUTION LIST (Cont'd)

29. Lockheed Missile and Space Company  
P. O. Box 879  
Mountain View, California 94040  
Attention: Technical Library 1
30. Eaton Research Center  
26201 Northwestern Highway  
Southfield, Michigan 48076  
ATTN: Librarian 1
31. Chrysler Corporation  
Research Office  
Dept. 9000  
P. O. Box 1118  
Detroit, Michigan 48231  
Attention: James Furlong (418-19-40) 1  
Ronald Pampreen (418-38-31) 1
32. Elliott Company  
Jeannette, Pennsylvania 15644  
Attention: J. Rodger Schields  
Director-Engineering 1
33. California Institute of Technology  
Pasadena, California 91109  
ATTN: Prof. Duncan Rannie 1

### DISTRIBUTION LIST (Cont'd)

- 34. Massachusetts Institute of Technology  
Cambridge, Massachusetts 02139  
Attention: Dr. J. L. Kerrebrock 1
  
- 35. Caterpillar Tractor Company  
Peoria, Illinois 61601  
Attention: J. Wiggins 1
  
- 36. Penn State University  
Department of Aerospace Engineering  
233 Hammond Building  
University Park, Pennsylvania 16802  
Attention: Prof. B. Lakshminarayana 1
  
- 37. Texas A&M University  
Department of Mechanical Engineering  
College Station, Texas 77843  
Attention: Dr. Meherwan P. Boyce P.E. 1